# TECHNICAL REPORT ON THE TELEGRAPH MINE GOLD PROJECT SAN BERNARDINO COUNTY, CALIFORNIA

## Prepared for

## MOJAVE GOLD MINING CORPORATION


**Prepared by**
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## Date and Signature Page

I, David A. Hedderly-Smith, a professional geologist and proprietor of D.A. Hedderly-Smith and Associates whose business address is P.O. Box 981224, 7533 Pinebrook Road, Park City, Utah 84098, USA, HEREBY CERTIFY THAT:

This Certificate applies to the Technical report on the Telegraph mine Project, San Bernardino County, California;

I am a graduate of the Western Washington State College (now University) with a B.Sc. in Geology in 1971; I am a graduate of the University of Washington with a M.Sc. in Geological Sciences in 1975; and I am a graduate of the University of Utah with a Ph.D. in Geology in 1997;

I am a member in good standing of several technical associations or societies including the Alaska Miners Association, the Utah Geological Society, the Geological Society of Nevada, the Society of Economic Geologists (SEG, Fellow) and the Society for Geology Applied to Mineral Deposits (SAG, Full Member);

I am a licensed Professional Geologist in the State of Utah, and my registration number is 5328528-2250;

From 1971 until the present I have been actively employed in various capacities in the mineral industry for over 40 years;

I visited the Telegraph Mine Project in San Bernardino County, California, on May 18, 2013 and examined the property;

I do not own any interest in the properties involved in the Telegraph Mine Project, and I am independent and hold no interest in Mojave Gold Mining Corporation or any other entity involved in the Telegraph Mine Project;

I have read Canadian National Instrument 43-101 (N.I. 43-101), Standards of Disclosure for Mineral Projects, dated June 24, 2011, and am a "Qualified Person" per the terms of N.I. 43-101. While Mojave Gold Mining Corporation is not a Canadian Corporation subject to Canadian securities regulations and this report will not reviewed and approved by Canadian securities officials and filed with SEDAR, to the best of my knowledge this technical report has been prepared in compliance with that instrument; I am responsible for all sections of this report;

As of the date of this certificate to the best of my knowledge, information and belief, the technical report contains pertinent historical, scientific and technical information so that it is not misleading.

Dated this 23rd day of December, 2013.

David A. Hedderly-Smith, Ph.D., P.G.

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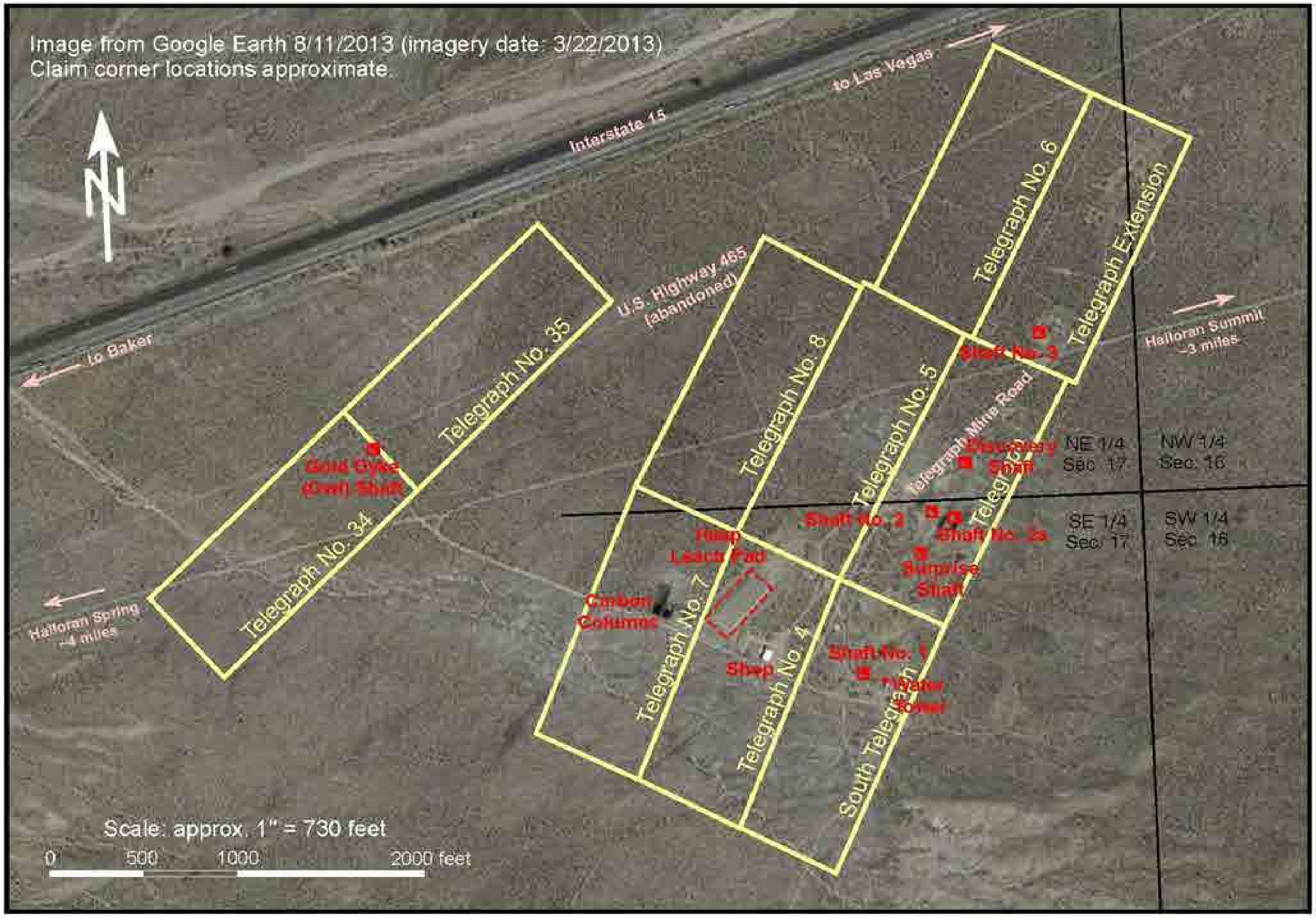


Figure 1. Google Earth image of the Telegraph Mine area with claims located and shafts and surface workings labeled (DHS, 2013).

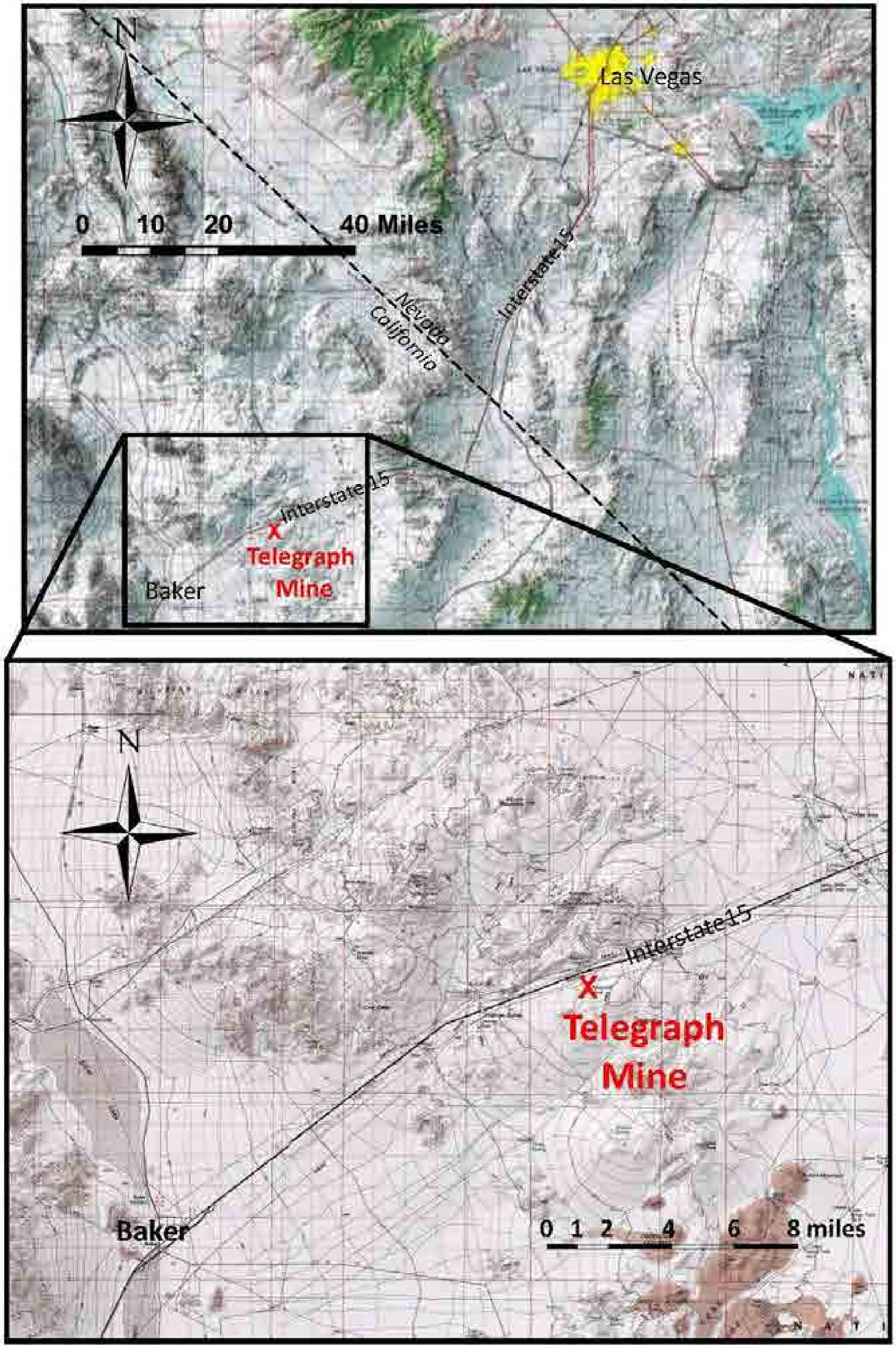


Figure 2. Index map showing the location of the Telegraph Mine property.

# 1. Summary

The Telegraph Mine property is located in the Halloran Hills of the central Mojave Desert in San Bernardino County, California, approximately 18 miles northeast of Baker, California, and 70 miles southwest of Las Vegas, Nevada. The property is within the Mojave National Preserve which is administered by the National Park Service.

The property currently consists of three mining claims patented in 1982 and seven contested unpatented federal mining claims. Shaft No. 2 near the center of the three patented mining claims is located at approximately 3916200N, 606320E, UTM Zone 11, NAD83. The three patented mining claims were patented to Cascade Energy and Metals Corporation ("Cascade"), a Utah corporation, and are currently owned by HMI Lenders LLC ("HMI"), a Utah limited liability company. All federal requirements for patenting under the 1872 Mining Law *et seq.* have been met, and HMI has obtained title to the surface and subsurface estates. The seven unpatented claims are also owned by HMI and are currently subject to litigation involving their validity.

While gold mining in the Halloran Hills may date back to the Spanish occupation of California, the Telegraph mining claims were first located in 1930. The main Telegraph vein was mined from 1932 through 1948 in five separate locations with three developed shafts and associated underground workings. The recorded production from the Telegraph Mine prior to 1948 identifies 2749 tons that were shipped for gold recovery containing 2559 tr. oz. gold, 5423 tr. oz. silver and 500 pounds of copper (an average grade of 0.93 oz. gold/ton and 1.97 oz. silver/ton). Some intermittent work apparently continued into the 1950's.

The Halloran Hills contain rocks ranging in age from the Proterozoic to the latest Holocene. Precambrian rocks exposed north of the Telegraph Mine area include older, mid-Proterozoic (1800 to 1600 Ma) amphibolite facies biotite gneisses and mafic meta-volcanics and younger foliated gneissic granite to granodiorite rocks overlain by Upper Proterozoic (1100 to 1300 Ma) metamorphic carbonates and quartzites of the Pahrump Group and the Johnnie formation. Paleozoic rocks in the central Halloran Hills include Cambrian limestone, shale and quartzite.

Much of the exposed rock in the Halloran Hills is composed of Cretaceous igneous intrusions including the Teutonia quartz monzonite, which is a composite pluton with as many as eight distinct calc-alkalic to alkalic bodies.

The Telegraph Mine hosts a series of low-sulfidation, quartz-adularia, epithermal gold- and silver-bearing quartz breccia-veins (the Telegraph vein) hosted in a Miocene fault in the informally named Cretaceous Teutonia adamellite (quartz monzonite or monzo-granite). The quartz-sericite-adularia-pyrite and quartz-carbonate veins have been shown to displays some 3500 feet-plus of strike and averages about 5 feet in width; however, the structure that contains the vein has boiling-type epithermal deposit. Although the breccia-veins are hosted in a fault in the Cretaceous intrusive rocks, the age of the mineralization is presumably 10.3±0.4 Ma, and likely related to volcanic activity.

The breccia-veins are composed of brecciated and rebrecciated wall rock (adamellite) cemented by products of the mineralizing hydrothermal fluids: dominantly quartz, adularia, illite, sericite, calcite, other carbonates, and minor pyrite. Central zones of the breccia-vein contain a larger percentage of rebrecciated clasts, smaller clast sizes and a higher percentage of open-space hydrothermal mineral matrix.

The breccia-vein ranges from 1 to 11 feet (0.3 to 3.4 meters) in width and is bounded by altered and more weakly mineralized wall rocks extending 1.5 to 80 feet (0.5 to 24 meters) from the main zone. The main outcrop zone of the Telegraph vein stretches 2000 feet (600 meters) from Hill No. 1 on the south-southwest to Hill No. 3 to the north-northeast. However, the breccia-vein system also extends to the north well beyond Hill No. 3 to the northern end of the Telegraph Extension claim and to the south beyond Hill No. 1.

Modern exploration of the Telegraph property began in 1968-1969 with a sampling and core drilling program by geologist Tomo Ito. Ito drilled 14 holes totaling 2079 feet, including 549 feet of core, during the program partially funded by a federal Office of Mineral Exploration grant. Ito estimated a resource within the drilling zone of 72,750 tons averaging 0.51 tr. oz. of gold and 1.16 tr. oz. of silver per ton. His tonnage calculations were based upon a vein structure averaging 4 ft. in width, a height of 150 ft. (down-dip) and a total strike length of 2000 feet, with the tonnage reduced by 28% (mined out, displaced, non-commercial, etc.).

In 1974 Cascade Energy and Metals Corporation acquired the Telegraph Mine. In May of 1976, Telegraph Mine Ltd. (a Utah limited liability company) acquired the Telegraph Mine Prime Lease from Cascade. In January, 1979, Gold Technics Ltd. ("Gold Techniques"), a California corporation, acquired a 40% interest in the prime lease from Telegraph Mine Ltd. In May of 1980 Gold Technics and Telegraph Mine Ltd. entered into a joint venture entitled the Telegraph Mine Joint Venture. In 1980 Gold Technics sold 30% of its prime lease interest to Rex Montis Silver Company ("Rex Montis"), a Utah corporation. In 1980 the Gold Technics parties promoted a Telegraph Mine Joint Venture offer to lease 35 units of sublease and working interests in the Telegraph Mine. The sublease working interest holders formed a private general partnership called Telegraph Mine Associates ("the Associates"). Telegraph Mine Associates hired Cascade as their operator. From September 1981 through December 1982 the Associates Management Committee provided significant and substantial management and oversight direction to their operation manager Cascade.

In late 1981 and 1982 Cascade drilled 1,984 feet in 55 percussion exploration holes on the main Telegraph vein on the three patented Telegraph claims and another 712 feet in 13 percussion exploration holes on the Gold Dyke vein on the unpatented Telegraph Nos. 34 & 35 claims.

During 1981 and 1982 approximately 28,500 tons of ore was mined from an open pit developed at Hill No. 2 (Shaft No. 2) with mining confined to the vein breccia and the fractured, silicified footwall. The waste to ore ratio was 4 to 1. The pit had a mining width of 58 feet and a height from the normal ground surface, extending to the crest of the hill, of 45 feet along a strike of 325 feet. Extraordinary amounts of rain during the spring of 1982 delayed operations.

The ore was mined, run through a jaw, cone and roll crusher and crushed to -¼"; then loaded into cement trucks where each load was sampled (see Appendix H) , and agglomerated with water, Portland cement flue dust, cyanide and hydrogen peroxide while being transported to the leach pad; then dumped onto the leach pad where it was sprinkled with a cyanide-water mixture. The pregnant solution was drained to a pregnant pond; pumped to a Merrill Crowe system for recovery through de-aeration and a zinc feed where the gold dropped out of solution onto diatomaceous earth filters. The filter medium was backwashed into a pressurized container where it was dewatered and the concentrate sent to an in-house refinery in Salt Lake City to be poured into dore bars for distribution to investors and or sale to gold refiners.

Cascade's crushing and haulage records from the summer and fall of 1982 indicate 24,285 tons of ore were crushed to -¼" and agglomerated and stockpiled on the leach pad for gold extraction. This ore reportedly had an average grade of 0.21 tr. oz. gold/ton. During this time and until 1994 the Associates controlled the Telegraph mine property and the recovery process at the mine plant, and it is undetermined how much gold may have been directly distributed to the Associates. It is also undetermined how much gold may have been removed thereafter. Records from Cascade's in-house refinery in Salt Lake City indicate 91 ounces in the form of dore bars was distributed to the Associates and 504.67 ounces of gold was sold by the Associates. An undetermined amount of gold was also apparently misappropriated by an employee of the Salt Lake City in-house refinery. Due to these factors it is unknown how much gold remained in the leach pile when the Associates operations were terminated in early 1983.

In October of 1982, largely due to apparent poor gold production from the open-pit mining operation which resulted from a slow start-up due to a very wet spring in 1982 and other factors, a dispute arose among some of the investors in the Telegraph Mine Associates and the Telegraph Mine Joint Venture which led to the mine's closure and prolonged litigation. Crushing and haulage of ore was discontinued on October 7, 1982, although the plant at the mine site continued to process solution from the pregnant pond until the end of January of 1983, at which time the entire operation was shut down.

Various legal manipulations (more thoroughly described in the **1982-2005 "Legal Limbo"** subsection of section **6. History**, below) continued until 2005 and precluded any development of the property until then. In 1983 about half of the Telegraph Mine Associates investors became disgruntled and filed a *lis pendens* against the Telegraph Mine property and obtained an injunction enjoining the "taking possession of, or otherwise disposing of or impairing the rights of the

(Telegraph Mine) Associates in the mine project." In October of 1985 and again in 1986 the disgruntled Associates filed judgment liens on the Telegraph Mine property in San Bernardino County, California. The inability to secure financing, in part due to the judgment lien filings, caused Cascade to file for reorganization under Chapter 11 of the Bankruptcy Code, and while in 1989 the Bankruptcy Court adjudged that the non-paying Associates judgment recordings were improperly made and did not create a valid lien, the Cascade bankruptcy was not finally dismissed until 2005.

Hence from 1982 until 2005 the property was in a legal "limbo" which precluded any mining operations.

In 2005 HMI Lenders LLC ("HMI"), a Utah limited liability company acquired the Telegraph Mine property from Cascade following the termination of its federal bankruptcy court proceedings in Utah. HMI subsequently formed a joint-venture on the property (the Telegraph Mine Joint Venture) with Investigold Ventures II LLC ("Investigold"), a Utah limited liability company, and in 2010 the Telegraph Mine Joint Venture has leased the Telegraph property to Mojave Gold Mining Corporation ("Mojave Gold"), a Wyoming corporation, for mine development and gold and silver recovery. Mojave Gold Mining Corporation has retained Stone Resources LLC ("Stone Resources"), a Utah limited liability company, as operator.

Several resource estimates (often called "reserve estimates" or "ore reserves" at the time) have been done at the Telegraph Mine since Ito's initial 1969 drill program.

The most current resource estimate is an in-house estimate prepared by and approved in 2010 by Mojave Gold's Directors (see Directors' qualifications Appendix A). These "Ore Reserve Estimates" are included in a 2012 Private Placement Memorandum (Mojave Gold Mining Corporation, 2012) and categorized the resources as "Measured Mineral Reserve," "Probable Mineral Reserve," Inferred Mineral Reserve," and Potential Mineral Reserve" as follows in Table 1:

**Table 1. Mojave Gold In-House Classified Mineral Resources**

| Mojave Gold Mineral Reserves Classification | Quantity (tons) | Gold Grade (g/T) | Gold Total (tr. oz.) | Silver Grade (g/T) | Silver Total (tr. oz.) |
|---|---|---|---|---|---|
| Measured | 510,440 | 7.20 | 107,192 | 12.24 | 182,227 |
| Probable | 525,728 | 7.20 | 110,403 | 12.24 | 187,685 |
| Inferred | 2,102,912 | 7.20 | 441,612 | 12.24 | 750,740 |
| Potential | 1,350,000 | 7.20 | 283,500 | 12.24 | 481,950 |

The "Measured Mineral Reserve" includes the vein/ore contours identified at Hill No. 1 & Hill No. 2, the Surprise Stope, the Discovery Shaft contour and the Shaft No. 3 contour to the 250-foot depth (330 feet down dip). These resources are estimated to contain 510,440 tons (680,587 tons less 25% for non-commercial/mined out) of material containing 107,192 ounces of gold and 182,227 ounces of silver (average grade 0.21 opt [7.20 g/T] Au and 0.36 opt [12.24 g/T] Ag). The "Probable Mineral Reserve" includes these same zones to the 500-foot depth with the assumption that the vein zone between the 250-foot depth and the 500-foot depth will include 50% of the 2000-foot strike length from Hill No. 1 to Hill No. 3 for a mineralized resource of 525,728 tons. The "Inferred Mineral Reserve" of 2,102,912 tons extends the "measured" and "probable" zones to a depth of 1500 feet. The "Potential Mineral Reserve" includes the potential ore zone of the Telegraph vein within the Telegraph Extension claim north of Shaft No. 2 and traceable for another 1200 feet to the north between the 150-foot and 1500-foot elevations.

These resource estimates, while done after implementation of N.I. 43-101, were dependent on the historic work of Ito done in 1969 (Ito, 1969), Cascade Energy and Metals in 1981-1982 (Owesn, 1980; Jensen, 1981) and Rocanville Corporation in 2006 (Ryzak, 2007). This historic work was not done per N.I. 43-101 guidelines, and under N.I. 43-101 guidelines Mojave Gold's resource estimates would not be considered N.I. 43-101-compliant. However, while this work should not be considered N.I. 43-101-compliant, Mojave's work was done by persons qualified by professional degrees and experience. The in-house resource estimates have been authorized and approved by Mojave Gold's Directors (Appendix A).

Prior evaluation of the Telegraph mine's resources commenced in 1969 with Tomo Ito (1969) initial resource estimate (he referred to it as an "ore reserve") within his drilling zone between Shaft No. 1 and Shaft No. 3 at 72,000 tons averaging 0.51 tr. oz. of gold and 1.16 tr. oz. of silver per ton in two blocks to a depth of 150 feet down-vein (an actual depth of about 107 feet on the $45^0$-dipping vein). He felt that the results of the drilling indicated good vein structure to at least a depth of 200 feet on the dip from Shaft No 3 southward to Shaft No 1. At Ito's average grades of 0.51 opt Au and 1.16 opt Ag, his 72,000 tons of resources would contain 36,720 ounces of gold and 83,520 ounces of silver. It is worth noting that Ito's 72,000 tons of resources were only to a depth of slightly over 100 feet below the current ground surface.

In 1979 and again in 1980 the mine was evaluated by geologist Joseph Owens, who had been retained by Gold Technics, a California firm that was a joint-venture partner in the Telegraph Mine property, to confirm the findings of Ito and assess the mineralized resource. Owens examined the deposit, took numerous channel samples to verify Ito's findings, and calculated an average grade of 0.425 tr. oz. of gold and 1.31 tr. oz. of silver. Owens noted that he believed that Ito's tonnage estimates were "extremely conservative." He calculated "Tonnage Estimates – Inferred Ore" of 540,000 tons within the area of the 1968-1969 drilling (mostly between Shafts No 1 and No. 3) by extending the ore zone to a depth of 450 feet. Owens assumed grades of 0.50 opt gold and 1.16 opt silver for an estimated resource of 270,000 ounces of gold and 626,400 ounces of silver. Using an overall strike length of 9,000 feet, extending to the north and south of the three patented claims, and an average vein width of 4 feet, he projected a target resource of 1,350,000 tons to a depth of 450 feet. With a dilution factor of 25% his geologically inferred resource estimate was 1,012,500 tons.

In 1981 the Telegraph Mine Associates hired Meade LeRoy Jensen, Ph.D., a noted university professor, consulting economic geologist and co-author of the college text *Economic Mineral Deposits*, to evaluate the work of Ito and Owens. He affirmed acceptance of the resource estimates of both Ito and Owens. In testimony in court Jensen stated that he felt that Ito's resource estimate of 72,000 tons to be "proven reserves." In December of 1981 Cascade Energy and Metals drilled a vertical 528-foot well for water on the Telegraph No. 4 unpatented mining claim approximately 400 feet west of the Telegraph Mine Shaft No. 1 on the Telegraph South patented claim and intercepted the projected mineralized shear zone at depths of 305 to 314 feet and 364 to 370 feet. Jensen then estimated the resource in the vein between Shafts No. 1 and No. 3 at 300,000 tons based on the drill-hole results and persistence of the vein with depth. Jensen assumed an average grade of 0.354 tr. oz. of gold per ton for a total resource of 106,200 ounces of gold.

In 1982 Zions First National Bank of Salt Lake City, Utah, which was making a loan to Cascade Energy & Metals Corp. to purchase a crushing and screening plant, hired mining engineer C.M. Daily to examine the Telegraph Mine operation and submit a report of his findings to the Bank. Daily had the benefit of having seen the results of much of the 1981-1982 drilling which showed the footwall of the Telegraph vein to be fractured, highly silicified and mineralized, creating a mineralized zone much wider than previously anticipated. Pursuant to that drilling Daily affirmed an estimated reserve of 108,000 tons (30 ft. depth down-dip) averaging 0.189 oz. of gold and 1.16 oz. of silver per ton (containing an estimated 20,412 ounces of gold and 125,280 ounces of silver) which would be amenable to open-pit excavation in the area of Shaft No. 2.

The Ito (1969), Owens (1980), Jensen (1981) and Daily (1982) resource estimates were all contracted by third-party interests prior to the implementation of N.I. 43-101 and would be considered historic resource estimates under the guidelines of N.I. 43-101. Again per N.I. 43-101 guidelines, prospective investors would be advised not to rely upon these historic resource estimates.

In 2006 geologist David Ryzak, a development and mine production geologist with 30 years' experience with several mines in the Western U.S., examined the Telegraph Mine property on behalf of Rocanville Corporation, a Texas corporation interested in becoming a partner in the property. Ryzak also supervised the drilling of a 380-foot vertical drill hole 500 feet west-southwest of Shaft No. 2 on the Telegraph No. 8 claim. In 2007 and 2008 HMI Lenders contracted Ryzak to compile a resource estimate and conduct an economic assessment of the Telegraph Mine as an expert witness in the legal dispute with the Department of the Interior involving the validity of the unpatented claims. Ryzak, in consultation with Peter Lange, calculated an open-pit mineable resource along the vein with a strike length of 2,400 feet extending from the area of Shaft No. 1 at the northern end of the Telegraph South claim across the Telegraph claim to the area of Shaft No. 3 at the southern end of the Telegraph Extension claim to depth of 130 feet down-dip. He determined a resource of 89,700 ounces of gold in 345,000 tons of ore averaging 0.26 opt Au with a 4:1 strip ratio. Ryzak also calculated an underground mineable resource of 204,000 tons from the bottom of his proposed pit to the 500-foot depth in the vein with an average width of 4 feet and a strike length of 2400 feet. With an average grade of 0.48 opt Au, this resource to be mined underground would contain 97,920 ounces. Hence Ryzak identified a total estimated resource of 187,620 tr. oz. of gold in the Telegraph vein to the 500-foot depth.

Ryzak's resource estimates, while done after implementation of N.I. 43-101, were somewhat dependent on the historic work of Ito (1969), Owens (1980) and Jensen (1981). This historic work was not done per N.I. 43-101 guidelines and would not be considered N.I. 43-101 compliant.

The author believes that the potential for a large-volume, low-grade gold deposit at the Telegraph Mine is particularly noteworthy. Historic exploration and development efforts at the Telegraph Mine were always directed towards production from the main Telegraph vein itself and immediately adjacent hanging wall and footwall. However, review of the results of the Cascade Energy and Metals 1981-1982 percussion drilling program at the Telegraph Mine and at the adjacent Gold Dyke property suggest there may be excellent potential for a substantially larger, albeit lower-grade deposit on the property. Numerous drill holes well away from the main Telegraph vein display 40-foot to 80-foot intercepts of about 1.0 g/T Au or greater. Additionally many of the holes into and through the vein itself bottomed with their last sample greater than 1.0 g/T Au and should be considered "open at depth."

The author believes that a very good possibility exists for the development of a surface-mineable, heap- or vat-leachable, resource of up to ten or more million tons of material grading +1.0 g/T Au in the immediate area of the main Telegraph vein on the three patented claims. Additional resources of similar grade may exist on the adjacent Gold Dyke claims.

## 2. Introduction

In May of 2013 the author, David A. Hedderly-Smith, Ph.D., P.G., was commissioned by Mojave Gold Mining Corporation ("Mojave Gold") to prepare a technical report in the form of a Canadian National Instrument 43-101 (NI 43-101) independent technical report on Mojave's Telegraph Mine property in San Bernardino County, California. The purpose of the report was to compile, evaluate and assess a 40-plus year mass of historical data on the property.

Of special note this report has been prepared in accordance with the guidelines provided in Canadian National Instrument 43-101 (N.I. 43-101), Standards of Disclosure for Mineral Projects, dated June 24, 2011. The author, David A. Hedderly-Smith, Ph.D., P.G., is a "Qualified Person" under the guidelines of N.I. 43-101 and has written N.I. 43-101 reports for Canadian clients. This report is written to the standards of that instrument; however, as Mojave Gold Mining Corporation is not a Canadian Corporation regulated by Canadian securities officials, this report has not been reviewed and approved by such officials and is not being submitted to SEDAR. This report is written in the form of a N.I. 43-101 technical report, but lacking official review and publication through SEDAR, it is not a true N.I. 43-101 report.

A substantial amount of historical data in the form of public sector reports, private sector reports, private correspondence and letter-reports, and court testimony and exhibits given or prepared by expert professionals and used in litigation involving the Telegraph Mine property was provided to the author by Mojave Gold Mining Corporation. The vast majority of that material and any of it that is cited herein is listed in section **27. References**, below.

On May 8, 2013, the author made a one-day site visit to the Telegraph Mine in the company of W. David Weston, President and Director of Mojave Gold Mining Corporation, and Jesse Clark, an Australian geologist. The property was inspected and much of the main Telegraph vein was walked from the Shaft No. 1 area on the Telegraph South claim to the north end of the Telegraph Extension claim (Figure 1, Appendix I). The Shaft No. 1 area, the Shaft No. 2 area and the area of the 1982 mining were examined in detail, and the area from Shaft No. 3 through the Northern Extension area to the northern end of Telegraph Extension claim was walked, tracing the vein through the area. The Gold Dyke area on the unpatented Telegraph Nos. 34 & 35 claims was also examined as were the areas of the unpatented Telegraph Nos. 4, 5 & 7 claims that were involved in the production during 1981-1982.

The author has not independently conducted any title or other searches, but has relied upon Mojave Gold Mining Corporation for information on land ownership, tenure and permit status. This report does not provide any legal title opinion as this is beyond the professional scope of the author.

Units historically used in reports on the Telegraph properties are almost exclusively imperial (feet, inches, miles, etc.). As the property is situated in a U.S. jurisdiction, measurement data is usually presented using both U.S. (imperial -- feet, inches, miles, etc.) and metric (meters, kilometers, etc.) measurements. Most of the historic precious metal analytical and assay data was originally presented ounces per ton (opt) of gold or silver, but these analyses have been converted to grams per metric ton (g/T) gold or silver by the author for this report. Often both opt and g/T figures are included in this report. All currencies are in United States dollar denominations unless otherwise stated.

The author wishes to thank the staff of Mojave Gold Mining Corporation for their assistance in providing historical data on the project and Mr. W. David Weston in particular for his assistance in identifying key materials from that data and his participation in helpful discussions of the Telegraph

Mine property. While the author has not met Peter S. Lange, the author feels the Mr. Lange's geologic work on the Telegraph property as documented in his excellent Master's degree thesis at the Colorado State University (Lange, 1988) and his testimony in *United States of America v. HMI Lenders, LLC,* (Lange 2008) should be acknowledged herein.

## 3. Reliance of Other Experts

In the preparation of this report the author has relied very heavily on a series of historical reports on the Telegraph Mine as well as on sworn court testimony in legal proceedings by expert witnesses regarding the property. Throughout this report the author has attempted to cite sources for any technical data gleaned from the historical reports or court testimony, and all of the sources are citied in section **27. References** at the end of this report.

While some of the geologists and other technical experts who compiled the historical reports are known to the author either professionally or by reputation, many of them are not. However, the facts, interpretations and conclusions of these historical reports are very consistent, and in many cases a latter report will cite an earlier report and specifically support and expand upon the conclusions of the earlier report.

The author made a one-day site visit to the Telegraph Mine in May of 2013, and his observations made during that visit were fully consistent with descriptions of the property included in each of the historic reports cited herein.

## 4. Property Description and Location

The Telegraph Mine property is located in the Halloran Hills of the central Mojave Desert in the Halloran Summit Mining District in sections 16 & 17, T. 15 N., R. 11 E., San Bernardino Baseline & Meridian, in San Bernardino County, California, approximately 18 miles northeast of Baker, California, and 70 miles southwest of Las Vegas, Nevada, on the immediate south side of Interstate 15 (Figures 1 & 2, Appendix I). The property is within the Mojave National Preserve which is administered by the National Park Service.

The property currently consists of three patented mining claims and seven contested unpatented federal mining claims (Figure 1, Appendix I). Shaft No. 2 near the center of the three patented mining claims is located at approximately 3916200N, 606320E, UTM Zone 11, NAD83. The property is located in the southwest quarter of the U.S.G.S. Solomons Knob, Calif., 7½-minute (1:24,000 scale) quadrangle one mile due south of Negro Head.

The three patented claims are listed in Table 2:

**Table 2. Patented Claims at the Telegraph Mine Property**

| Claim Name | Min. Survey No. | U.S. Patent No. | Date Patented |
|---|---|---|---|
| Telegraph | MS 6792 | 04-82-030 | March 23, 1982 |
| Telegraph Extension | MS 6792 | 04-82-058 | March 23, 1982 |
| South Telegraph | MS 6792 | 04-82-030 | March 23, 1982 |

The patented claims comprise 58.25 acres.

The three patented mining claims were patented to Cascade Energy and Metals Corp. and are now owned by HMI Lenders LLC ("HMI"). All federal requirements for patenting of the three claims under the 1872 Mining Law *et seq.* have been met, and. HMI now has title to the surface and subsurface estates (Cascade Energy and Metals Corporation, 2001). The seven contested unpatented claims are listed in table 3:

**Table 3. Unpatented Claims at the Telegraph Mine Property**

| Claim Name | Location Date | BLM Number |
|---|---|---|
| Telegraph No. 4 | August 1, 1983 | CAMC 135154 |
| Telegraph No. 5 | August 1, 1983 | CAMC 135155 |
| Telegraph No. 6 | August 1, 1983 | CAMC 135156 |
| Telegraph No. 7 | August 1, 1983 | CAMC 135157 |
| Telegraph No. 8 | August 1, 1983 | CAMC 135158 |
| Telegraph No. 34 | August 1, 1983 | CAMC 135185 |
| Telegraph No. 35 | August 1, 1983 | CAMC 135186 |

The five unpatented claims (Telegraph Nos. 4 through 8) contiguous to the three patented he claims (Figure 1) comprise approximately 110 acres. The two additional claims were located on the Gold Dyke vein and comprise approximately 44 acres. The seven unpatented claims were located by Cascade Energy and Metals Corporation (Cascade Energy and Metals Corporation, 2001) and are now owned by HMI Lenders LLC.

The Mojave National Preserve, consisting of approximately 1,419,800 acres (2,218.4 sq. mi.), was created by Congress as part of the California Desert Protection Act of 1994 (Pub. L. 103-433). The act created or expanded several federal conservation units in southern California.

While the Telegraph Mine property is located within an area described as Class III Desert Tortoise Habitat, it is not included in the Mojave Desert's "Critical Tortoise Habitat" as identified by the U.S. Department of Fish and Wildlife biologists and is only marginal tortoise habitat at elevations of 3800 to 4000 feet (Cascade Energy and Metals Corporation, 2001).

In March of 2004, the Department of the Interior challenged the validity of the twelve Telegraph unpatented claims located within the Mojave National Preserve. Mining on NPS land is governed by 36 CFR Part 9. Pursuant to the California Desert Protection Act, before any mining can commence a claimant must have an approved Plan of Operation, a determination of valid existing rights and an approved environmental report.

The Interior complaint charged that: (a) minerals have not been found within the limits of the unpatented claims in sufficient quantities and/or qualities to constitute a valid discovery of a valuable mineral deposit in 1994, the date of withdrawal pursuant to the California Desert Protection Act of October 31, 1994, (Public Law 103-433; CDPA); and (b) the lands are non-mineral in character. The complaint asked that the mining claims be declared null and void.

In 2005 the three Telegraph Mine patented and twelve unpatented claims (Telegraph No. 4, No. 5, No. 6, No. 7, No. 8, No. 19, No. 20, No. 32, No. 33, No. 34, No. 35, and No. 80) were obtained by HMI Lenders LLC, and subsequently HMI entered into the Telegraph Mine Joint Venture with Investigold Ventures II LLC.

HMI Lenders defended the challenge of the validity of the twelve unpatented Telegraph claims by the Department of the Interior contending that: (a) minerals have been found within the limits of the claim or by virtue of the down dip extension of the mineralized vein pursuant to extra lateral rights to Apex rights with respect to the mineralized veins in sufficient quantities and/or qualities to constitute a valid discovery of a valuable mineral deposit on the unpatented claims; and (b) the land comprising the unpatented claims both separately and collectively are mineral in character. A hearing (trial) was held on January 8 through 11, 2008 (United States of America v. HMI Lenders, LLC, IBLA Docket No. CACA 45975). During the hearing, HMI Lenders defended only Telegraph No. 4 through No. 8, inclusive, and No. 34 and No. 35 (Figure 1). Department of the Interior Administrative Law Judge Harvey Sweitzer rendered a decision on March 23, 2009, finding that values from the main Telegraph vein could not be inferred for the unpatented claims. HMI Lenders appealed Judge Sweitzer's decision which was upheld by the Interior Board of Land Appeals. This matter is now (November, 2013) before the United States District Court for the District of Utah (HMI Lenders v. Ken Salazar, Civ. No. 2:11-cv-504-DB).

The decisions in this matter should have little effect on the ability of HMI to exploit the Telegraph vein as the main Telegraph vein crops out on the three Telegraph patented claims and the side lines of the patented claims are essentially parallel to the vein. Under Apex Law the vein can be followed and mined extra-laterally wherever the vein exists, including under Telegraph No. 4-8, if the vein continues down-dip beneath those claims. (A copy of HMI's brief filed with the U.S. District Court for Utah, Case No. 2:11-cv-00504-DB is available from Mojave Gold upon request.)

It should also be noted that all of the patented and contested unpatented claims at the Telegraph Mine property are located within approximately 4000 feet of Interstate 15, the northern boundary of the Mojave National Preserve in the area. If Congress were to adjust the preserve's boundary in this area, the mining property could be removed from the preserve and these claim validity issues would become moot.

HMI Lenders LLC currently owns 77.45%, and Investigold Ventures II LLC owns 22.55% of the mining claims. These parties have formed the Telegraph Mine Joint Venture with Stone Resources LLC as its manager to develop the claims. The Joint Venture has leased the mining claims to Mojave Gold Mining Corporation for mine development and gold and silver recovery. The lease requires minimum annual payments of $25,000 for the first year established as the date a mining permit is issued by the relevant government agencies, $50,000 for the second year and $100,000 for each year thereafter reduced by any production royalty payments. The production royalty is 6¼% of the net smelter returns when the price of gold is less than $900.00 per ounce or 7¼% of the net smelter returns when the price of gold is greater than $900.00 per ounce.

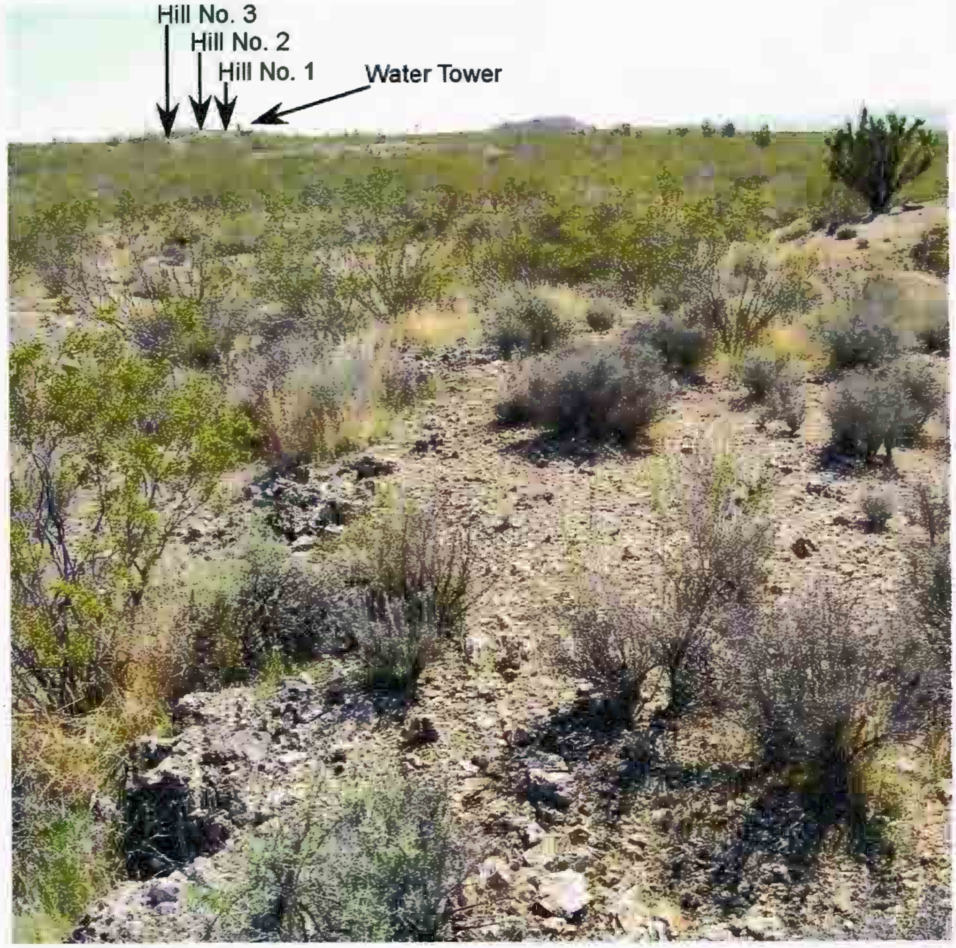


Figure 3. View to the south-southwest towards Hill No. 1 from standing on rubble of the Telegraph Vein in the north-central portion of the Telegraph Extension claim (approx. 155S & 350W on the Telegraph grid). (photo from Mojave Gold Mining Corporation, taken 2010.)

# 5. Accessibility, Climate, Local Resources, Infrastructure and Physiography

Access to the Telegraph Mine property is simple and straight-forward with the property accessed on an existing gravel road along a right-of-way extending from the Halloran Summit (Yucca Grove) overpass (Exit 265) on Interstate 15, approximately 3 miles east-northeast of the property. This access road parallels Interstate 15 along the telephone and telegraph right-of-way from the

Figure 4. View to the north-northwest from standing on rubble of the Telegraph Vein at the northern end of the Telegraph Extension claim (approx. 300N & 400W on the Telegraph grid). (photo from Mojave Gold Mining Corporation, taken 2010.)

Halloran Summit Overpass exits to the Halloran Springs on- and off-ramps (at Exit 259), and the property can also be accessed from the Halloran Springs interchange, approximately 4 miles to the west-southwest. The Telegraph Mine property itself is laced with numerous dirt roads. (See Figures 1 & 2 and Appendix I.)

The nearest community is Baker, California, with a population of 735, 18 miles to the west-southwest at the junction of Interstate 15 and SR 127 (Death Valley Road). Baker is a touristoriented town and bills itself as the "Gateway to Death Valley."

Barstow, California, (pop. 22,500) with most commercial facilities is 83 miles to the west-southwest on the interstate. Las Vegas, Nevada, (pop. 580,000; 1.95 million in Las Vegas metropolitan area) with full commercial facilities is about 70 miles to the east-northeast on Interstate 15.

Elevations on the Telegraph Mine property range from about 3,750 feet to 3,900 feet. Topography is of relatively low relief with three small hills aligned along the main Telegraph vein (Figures 1 & 3). The dominant plant assemblage is that of the Mojave Creosote Bush Scrub Community with creosote bushes, desert mallow, brittlebush, hedgehog cactus, several types of cholla and the occasional Joshua tree (Figures 3, 4 & 5). Vegetation cover is less than 15%.

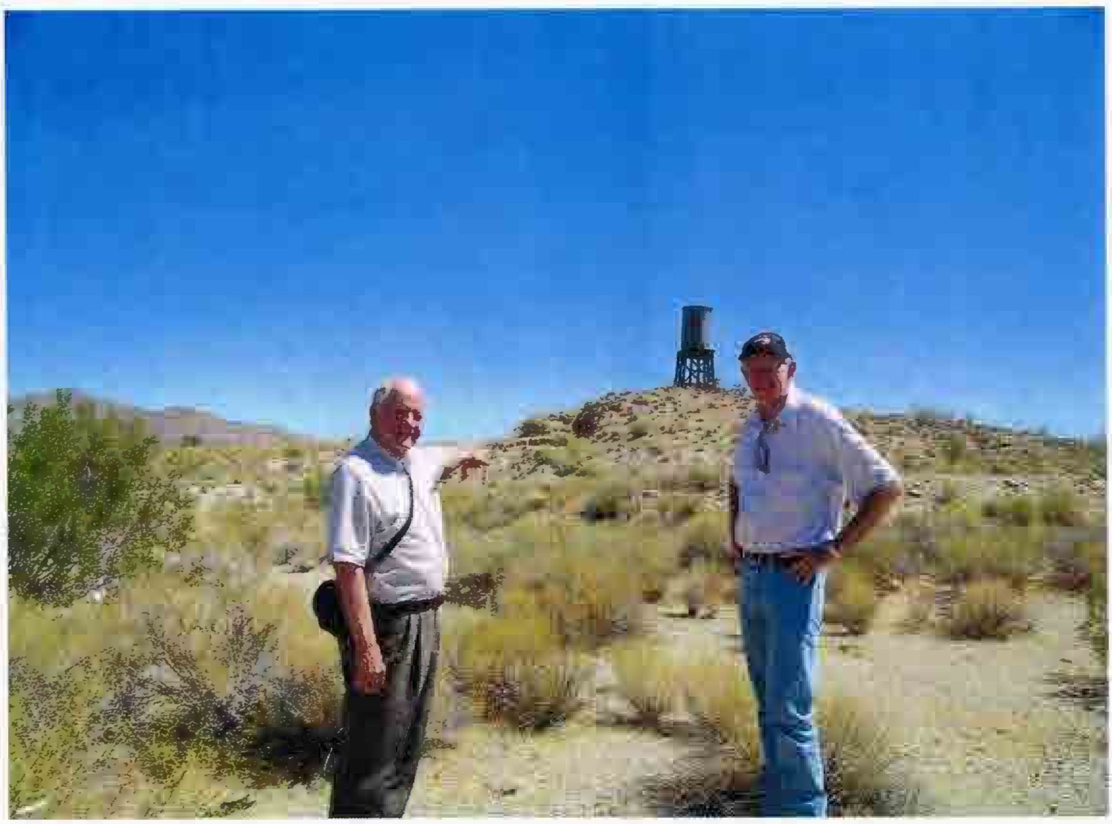

Figure 5. Mojave Gold Directors W. David Weston (left) and Ken Clifford, Ph.D, (right) standing south of the Water Tower and Hill No. 1. (photo from Mojave Gold Mining Corporation, taken 2010.)

Annual precipitation is low (4.19 inches or 106.4 mm at Baker). Temperatures are warm, ranging from an annual average high of 110°F (43°C) in July (record: 124°F; 51°C) to an average low of 34°F (1°C) in December (record: 14°F; -10°C) at Baker. Exploration, development and mining operations could certainly continue year-round.

An existing power transmission line is located on the north side of Interstate 15, and power may be obtained from this line through arrangements with California Power and requisite permitting. Alternatively power may be provided through an on-site diesel generator.

Pursuant to permit No. 05158101 issued by the Environmental Health Services of San Bernardino County, in late 1981 Cascade Energy and Metals drilled a 528-foot deep well (on the Telegraph No. 4 unpatented claim) approximately 400 feet west of the Telegraph Mine Shaft No. 1 (on the Telegraph South patented claim). Water from this source was used for mining and heap leaching operations and for culinary use in 1982 and 1983. It has also been intermittently used for culinary use since. Water necessary for anticipated operations on the Telegraph Mine property should not exceed 1000 gallons per day and will be obtained from water accumulated in the mine and from the well. (Cascade Energy and Metals Corporation, 2001.)

# 6. History

### Telegraph Mine: Pre-History to 1969

The Telegraph Mine is located in the historic Halloran Spring Mining District. Turquoise in the area was mined in pre-historic times by indigenous peoples (Leonard & Nelson, 1980). Claims were located on turquoise showings between 1895 and 1898, and turquoise was produced from the Solomon's Knob area (about 2½ miles north of the Telegraph Mine property) until 1904.

Gold mining is the Halloran Spring area may date back to the Spanish occupation of California as evidence by an old arrastre found on the Agua Dulce Lomex No. 1 claim – roughly 2500 feet (800 meters) south-southwest of the Telegraph Mine Shaft No. 1 (Ito, 1968).

The first evidence of American gold mining in the Halloran Spring area is reportedly provided by a 1902 miners' map of the desert that showed "Hyten's" at the site of James Huyten's Wanderer Mine (about a dozen miles northwest of the Telegraph Mine property). Huyten continued to work the mine throughout the ensuing years, occasionally leasing it out. By 1930 there were a number of shallow shafts, the deepest being 125 feet. There was also a 20 ton per day mill. With revived interest in the district following the discovery of gold at the Telegraph Mine in 1930, the group of 15 claims were leased to American Hellenic Gold Mining Company of Las Vegas.

The Telegraph mining claims were first located on November 19, 1930, by brothers Ralph and A.A. Brown of Salina, Utah. One Telegraph sample showed free gold in calcite and quartz and reportedly assayed up to $800 per ton in gold, and the brothers returned to Utah and interested Robert and Vivian Burns, who subsequently located a large number of claims.

The main Telegraph vein was mined from 1932 through 1948 in five separate locations with three developed shafts and associated underground workings. O. Perry Riker, of Long Beach, California, leased the property from December of 1932 to 1935. During this period, 220 tons of ore valued at $16.00 per ton was mined and milled at the custom mill at Yucca Grove (Halloran

Summit), three miles northeast of the mine, operated by Consolidated Metal Mines, Ltd., of Salt Lake City, Utah (Ito, 1968). Also, 909 tons of ore was shipped for smelting with a return of $18,963 (Ito, 1968). Total production of the mine for this period was reportedly was $35,200 (Ito, 1968). On the Telegraph Claim a shaft (now referred to as Shaft No. 2, Figures 1 & 6) was completed to a depth of 150 feet with two crosscuts accessing 100 feet drifts at the 50-foot and 100-foot levels. Subsequent operations, according to a Judge Nosser, who was a subsequent owner of the property, brought the total production to approximately $100,000. This figure correlates reasonably well with the totals shown in Table 4 below, from U.S.G.S. Professional Paper 275. The mine was idle in 1943 to 1945 (probably due to WWII), active again in 1946 to 1948 and reportedly had minor activity in the early 1950s. By 1953 all equipment had been removed (Vredenburgh, 1996.)

**Table 4. Telegraph Mine Record of Production Through 1948**

| Year | Crude Ore (tons) | Recoverable Metals | | | Average Au Grade (opt) | Average Ag Grade (opt) |
|---|---|---|---|---|---|---|
| | | Gold (ounces) | Silver (ounces) | Copper (pounds) | | |
| 1932 | 65 | 116.65 | 310 | | 1.80 | 4.77 |
| 1933 | 511 | 298.00 | 1582 | | 0.58 | 3.10 |
| 1934 | 99 | 50.30 | 327 | | 0.51 | 3.30 |
| 1935 | 44 | 16.81 | 113 | | 0.38 | 2.57 |
| 1936 | 442 | 231.65 | 832 | | 0.52 | 1.88 |
| 1937 | 285 | 29.00 | 129 | | 0.10 | 0.45 |
| 1938 | 32 | 12.00 | 114 | | 0.38 | 3.56 |
| 1939 | 199 | 286.00 | 530 | | 1.44 | 2.66 |
| 1940 | 452 | 931.00 | 793 | | 2.06 | 1.75 |
| 1941 | 119 | 188.00 | 187 | | 1.58 | 1.57 |
| 1942 | 216 | 261.00 | 244 | | 1.21 | 1.13 |
| 1946 | 155 | 74.00 | 141 | | 0.48 | 0.91 |
| 1947 | 117 | 47.00 | 100 | 400 | 0.40 | 0.85 |
| 1948 | 13 | 18.00 | 21 | 100 | 1.39 | 1.62 |
| Total | 2749 | 2559.41 | 5423 | 500 | 0.93 | 1.97 |

(Data from: Hewett, 1956, U. S. Geol. Survey Prof. Paper 275)

The mining reported by Judge Nasser, was conducted under the direction of Harrison B. Salisbury, then a young engineer. Mr. Salisbury reported that Shaft No. 1 (Figure 1) was completed in recoverable ore to a depth of 275 feet (W. David Weston, verbal communication, 2013) with exploration and mining on at least two levels. State records (Tucker and Sampson, 1943) reported a 2 inch (5cm) pocket of "high grade" ore in the foot wall of South Telegraph Shaft (Shaft No. 1) contained 18.5 oz./ton Au and 25.5 oz./ton Ag. Mr. Salisbury also instituted an early form of cyanide heap leaching for gold recovery during the development of Shaft No. 1 at the Telegraph Mine. He welded fifty-five gallon drums into a tall column into which he placed the gold bearing ore excavated during shaft construction. He then percolated cyanide solutions through the barrels filled with ore and recovered the gold from the cyanide solution by means of a zinc box. Mr. Salisbury, who later worked for the United States Bureau of Mines in the Salt Lake City research office, made the recommendations for and the initial experimental work for heap leaching which has become a standard in the mining industry world-wide for the recovery of gold from low grade ores.

Figure 6. Mojave Gold Directors Cherrie M. Tilley (left) and W. David Weston (right) at Shaft No. 2 on the Telegraph claim. Hill No. 2 is to the left (mostly out of the picture); the Water Tower on Hill No. 1 is to the rear of the picture. (photo from Mojave Gold Mining Corporation, taken 2010.)

The recorded production from the Telegraph Mine prior to 1948 identifies 2749 tons that were shipped for gold recovery with an average grade of 0.93 tr. oz. gold/ton and 1.97 tr. oz. silver/ton (Table 4). Over the last three years of production (1946-1948), 285 tons were shipped for gold removal with an average grade of 0.48 tr. oz. gold/ton and 0.919 tr. oz. silver/ton. Some intermittent work apparently continued into the 1950's. There are three hills which are silicified outcrops along the main Telegraph vein where the vein has widened presumably due to fissure side slipping. Each of the three hills have developed shafts (Figure 1) and associated underground workings which are results of the earlier mining.

In 1968 geologist Tomo Ito applied for and subsequently received a grant from the federal Office of Mineral Exploration (OME) for a drill program at the Telegraph Mine property (USGS-OME 6727). The federal grant covered $19,798.81 of the approximate total program cost of $27,000.

At the time of Ito's application, the principal historic workings at the Telegraph Mine, as noted in a report accompanying his application (Ito, 1968) included (on claims from south to north, see Figures 1 & 6):

<u>South Telegraph Claim</u>

- Shaft No. 1 (Main Shaft) – begins at a low incline ($-30^0$) for 50 feet, then steepens to $-52^0$ to the 125-foot level and beyond. The shaft extends to 275 feet (oral communication, Harrison Salisbury to W. David Weston [1978?] to author, 2013).

  Ito (1968) refers to records that show a drift at the 75-foot level that was driven 250 feet to the north and stoped in one location to the surface. Another drift goes 115 feet to the south with a reported cross-cut equipped with rails to the west and down dip. At the 125-foot level the vein is explored for 465 feet to the north.

<u>Telegraph Claim</u>

- Shaft No. 2 (Figure 6), located approximately 900 feet (275 meters) north of Shaft No. 1, to the 100-foot level, inclined @ $-76^0$, and underground workings with two cross-cuts at the 50-foot level and the 100-foot level open and accessible in 1968. The 50-foot level cross-cut had two stopes with the main stope open to the surface and a finger stope on the vein at the end of the cross cut.
- No. 2A stope which originally may have been an inclined shaft but now opens into the main stope.
- Surface exposure of 500 feet of massive quartz along the strike.
- Surprise shaft, shallow, approximately 15 feet in depth with 20 feet of drift in a shear zone of intense alteration, encountered a small lenticular vein of quartz obviously not part of the main body. "Shaft is located in alluvial material between two outcrops – appears to be located too far west of Main structure – possibly improperly located." (Ito, 1968.)
- Ito (1968) does not include the Discovery Shaft on the Telegraph claim between Hill No. 2 and Hill No. 3 on the telegraph Extension claim in his list of workings; Ito (1969) does show the Discovery Shaft on his Figure DH.

Telegraph Extension Claim

- Shaft No.3, located approximately 2000 feet (600 meters) north of Shaft No. 1, inclined @ -35$^0$, ±100-foot depth. Located just north of massive quartz outcrop. No drifting or cross-cutting from this shaft.

 Ito (1968) noted a shear zone, 6 to 8 feet wide, with intense alteration but only minor quartz. He also noted that there was curiously no attempt to drift towards the massive quartz outcrop to the south, and referenced records of high-grade ore discovered on this claim. (Ito, 1968.)

Ito drilled 14 holes totaling 2079 feet including 549 feet of core during the program partially funded by the OME grant (Figure 7). Ito estimated a resource within the drilling zone at 72,750 tons averaging 0.51 tr. oz. of gold and 1.16 tr. oz. of silver per ton. His 72,750 tonnage calculations were based upon a vein structure averaging 4 ft. in width, a height of 150 ft. (down-dip) and a total strike length of 2000 feet with the tonnage reduced by 28% (mined out, displaced, non-commercial, etc.). (Ito, 1969). More detailed results from his work are discussed in section **10. Drilling** and section **14. Mineral Resources**, below.

**Telegraph Mine: 1974 to 1981**

In 1974, W. David Weston acquired the Telegraph Mine from the McGilvray family for Cascade Energy and Metals Corporation (Cascade).

In May of 1976, Telegraph Mine Ltd., a Utah limited partnership, acquired the Telegraph Mine Prime lease from Cascade. On January 24, 1979, Gold Technics Ltd., ("Gold Techniques"), a California corporation, acquired a 40% interest in the prime lease from Telegraph Mine Ltd. In May of 1980 Gold Technics and Telegraph Mine Ltd. entered into a joint venture entitled Telegraph Mine Joint Venture. In 1980 Rex Montis Silver Company (Rex Montis), a Utah corporation, acquired 30% of the Gold Technics interest in the Joint Venture.

In 1979 and again in 1980 the mine was evaluated by geologist Joseph Owens, who had been retained by Gold Technics, to confirm the findings of Tomo Ito and assess the mineralized resource. Owens examined the deposit and took numerous channel samples to verify Ito's findings. He calculated an average grade of 0.425 tr. oz. of gold and 1.31 tr. oz. of silver for a "measured" resource of 72,750 tons to the 150-foot depth down-dip and an "inferred" resource of 540,000 tons, projecting Ito's zone to a depth of 450 feet down-dip. Owens also projected the vein to the north and south of the three patented claims, giving it a 9000-foot strike length. He estimated that this zone would contain 1,350,000 tons, less a dilution factor of 25%, for a total projected resource of 1,012,500 tons. His target projection was based on previous stope sampling and observed intensity of alteration in lower workings and recognition of vein structures to the north and south of the existing workings. (Owens, 1980.)

In 1980 the Gold Technics parties promoted a Telegraph Mine Joint Venture offer to lease 35 units of sublease and working interests in the Telegraph Mine to 22 various individual and corporate interests who collectively organized themselves into a general partnership called Telegraph Mine Associates (the "Associates"). The 22 Associate general partners comprised four groups: (1) persons affiliated with Gold Technics, (2) persons affiliated with Rex Montis, (3), Weston and affiliated entities, and (4) a few persons who were un-affiliated with any of the above. Telegraph Mine Associates hired Cascade as their operator; W. David Weston was President of Cascade and its majority owner. From September 1981 through December 1982 the Associates Management Committee provided significant and substantial management and oversight direction to their operation manager Cascade (personal communication, W. David Weston, 2013).

In October of 1981 the Telegraph Mine Associates hired Meade LeRoy Jensen, Ph.D., a noted university professor, consulting economic geologist and co-author of the college text *Economic Mineral Deposits* (John Wiley & Sons, 1981, IBSN 10: 0471090433) to evaluate the work of Ito and Owens. He affirmed acceptance of the resource estimates of both Ito and Owens. In December of 1981 Cascade drilled a vertical 528-foot well for water approximately 400 feet west-southwest of the Telegraph Mine Shaft No. 1 on the Telegraph No. 4 claim and intercepted the projected mineralized shear zone at depths of 305 to 314 feet and 364 to 370 feet (Figure 8) (see section **10. Drilling** for details). Jensen then estimated the resource at 300,000 tons, based on the drill hole results and persistence of the vein with depth (*i.e.*, 450' deep x 4.0' wide x 2000' long /12 $ft^3$/ton = 300,000 tons).

Jensen also noted a high assay on the Gold Dyke vein, about a quarter mile to the west of the Telegraph vein, from which he collected a sample containing 0.464 opt Au. Like the Telegraph vein, the Gold Dyke vein can be traced for several thousand feet and is just one more of over 20 veins in the area noted by U.S.G.S. geologist D.F. Hewett in Professional Paper 275 (Hewett, 1956). Jensen suggested heap leaching for the material produced from the Telegraph vein and strongly recommended a geologic mapping program for the property.

**Table 5. Average Price of Gold by Year 1970-1990**

| Year | Au Price ($/tr. oz.) | Year | Au Price ($/tr. oz.) | Year | Au Price ($/tr. oz.) |
|---|---|---|---|---|---|
| 1970 | $36.02 | 1977 | $147.84 | 1984 | $361.00 |
| 1971 | $40.62 | 1978 | $193.40 | 1985 | $317.00 |
| 1972 | $58.42 | 1979 | $306.00 | 1986 | $368.00 |
| 1973 | $97.39 | 1980 | $615.00 | 1987 | $447.00 |
| 1974 | $154.00 | 1981 | $460.00 | 1988 | $437.00 |
| 1975 | $160.86 | 1982 | $376.00 | 1989 | $381.00 |

(Data from National Mining Association, 2013)

Also in 1981, pursuant to a marked increase in the price of gold over the past several years (see Table 5) a program was instituted to assess the feasibility of identifying a mineralized zone that would be amenable to surface mining and heap leaching.

In late 1981 and 1982 Cascade drilled at least 1,984 feet in 55 percussion exploration holes on the main Telegraph vein on the three patented Telegraph claims as well as another 712 feet in 13 percussion exploration holes on the Gold Dyke vein on unpatented Telegraph Nos. 34 & 35 claims. Figures 9, 10 and 11 show the locations of the 55 percussion holes on the three patented Telegraph claims. Figure 9 shows collar locations and traces of 25 holes that were drilled at the Hill No. 2 area on the Telegraph claim; Figure 10 shows collar locations and traces of 21 holes that were drilled at the Hill No. 1 area on the Telegraph South claim; and Figure 11 shows collar locations and traces of 9 holes that were drilled in the Northern Extension area on the Telegraph Extension claim. Drill cuttings were generally assayed every 2 feet to determine metal content (Daily, 1982) (see section **10. Drilling**, below, for details of this drilling).

During this period Cascade established an assay data base consisting of 3,300 assays and geochem samples comprised of 1,507 drill hole samples, 889 samples from trenches, outcrops and underground workings and 905 geochem surface samples.

A potential the open pit mining zone was identified at Hill No. 2. The drilling also discovered that the foot wall of the main vein in the Hill No. 1 and Hill No. 2 area was intensely fractured, highly silicified, and modestly mineralized, creating a mineralized zone much wider than previously thought.

Dawson Laboratories of Salt Lake City had been retained for metallurgical testing. An April 16, 1981, letter-report on results of cyanidation testing on a 20 lb. split of Telegraph mine ore crushed to -3/8" indicated 78% recovery of gold and nil recovery of silver; a 1 kg sample ground to -100 mesh gave recoveries of 96.2% gold and 51% silver (Salisbury, 1981: Dawson Project No. P-604, Appendix G). In a June 23, 1981, letter-report from Dawson reports an approximate grind work index of 15 kw-hr/short ton for Telegraph Mine ore to produce a grind of 80% passing 100 microns (approximately -150 mesh) in a wet closed circuit using an 8-foot ball mill (Dawson, 1981a: Dawson Project No. P-650, Appendix G). A July 14, 1981, letter-report from Dawson on a Preliminary Batch Bulk Sulfide Floatation Test produced an 84.2% recovery of gold and a 65.0 percent recovery of silver; however, appreciable gold values (0.038 oz. Au/ton) remained in the tailings (Dawson, 1981b: Dawson Project No. P-658, Appendix G).

An open-pit mining operation over a 45-foot width along a strike length of approximately 325 feet was initiated in the silicified zone at Hill No. 2 (Shaft No. 2) on the Telegraph patented claim. A similar silicified zone identified by sampling and drilling was identified along a strike length of 350 feet at Hill No. 1 (Shaft No. 1 – Telegraph South patented clam). Two smaller, but similar, zones were discovered to exist north of Hill No. 2.

**Open Pit Mining and C. M. Daily, Mining Engineer, Report (1982)**

Following the initial exploratory drilling Cascade Energy and Metals entered into a contract to crush the ore for the lessees and obtained a loan from Zions First National Bank of Salt Lake City to purchase a crushing and screening plant. Zion's Bank hired Mr. C.M. Dailey, a mining engineer, who examined the mine during May of 1982 and submitted a report of his findings to the bank. He expressed the following opinion with respect to the then exposed surface ore reserves.

> *...Cascade Energy & Metals Corp. drilled a number of holes, spaced at 20 foot intervals along the course of the principal Telegraph vein .... The drill cuttings were assayed at 2 foot intervals to determine ore grade. The results of this development drilling was an estimated reserve of 108,003 tons (30 ft. depth) averaging 0.189 oz. of gold and 1.16 oz. of silver which was amenable to open-pit excavation....* (Daily, 1982.)

Figure 12. Mojave Gold President and Director W. David Weston standing north-northeast of the open pit from the 1981-1982 mining operation. (photo from Mojave Gold Mining Corporation, 2010.)

During 1981 and 1982 approximately 28,500 tons of ore was mined from an open pit developed at Hill No. 2 (Shaft No. 2) (Figure 12) with mining confined to the vein breccia and the fractured, silicified footwall. The waste to ore ratio was 4 to 1. The pit had a mining width of 58 feet and a height from the normal ground surface, extending to the crest of the hill, of 45 feet along a strike of 325 feet (Daly, 1982). Extraordinary amounts of rain during the spring of 1982 (*El Nino*) delayed operations. Cascade's crushing and haulage records from the summer and fall of 1981 indicate 24,285 tons of ore were crushed to -¼" and agglomerated and stockpiled on the leach pad for gold extraction.

The ore was mined, run through a jaw, cone and roll crusher and crushed to -¼"; then loaded into cement trucks where each load was sampled (see Appendix H), and agglomerated with water, Portland cement flue dust, cyanide and hydrogen peroxide while being transported to the leach pad; then dumped onto the leach pad where it was sprinkled with a cyanide-water mixture. The pregnant solution was drained to a pregnant pond; pumped to a Merrill Crowe system for recovery through de-aeration, a zinc feeder where the gold dropped onto filters with diatomaceous earth. The filters were backwashed into a tub and the concentrate sent to an in-house refinery in Salt Lake City. (personal communication, W. David Weston, 2013.)

**1982-2005 "Legal Limbo"**

Production of gold from the leach pad had been slow in start-up, and in the fall of 1982 a dispute arose among some of the investors in the Telegraph Mine Associates and the Telegraph Mine Joint Venture which led to the mine's closure and prolonged litigation. In the subsequent dispute between the Associates affiliated with Rex Montis and those associated with Cascade, along with some of the unaffiliated Associates (hereafter referred to as the "Cascade Group") were allied against those affiliated with Gold Technics and the rest of the unaffiliated Associates (hereafter referred to as the "Gold Technics Group").

The major issue between these two groups was whether or not the Associates Joint Operating Agreement provided for assessments to pay production costs. The Gold Technics parties claimed it did not and, after their initial payments of $30,000 each, refused to pay their share of the additional start-up expenses, ostensibly questioning the gold production. The Cascade group took the position the Associates Operating Agreement provided for assessments up to the net value of the gold mined milled and removed to the leach pile for extraction.

In the fall of 1982 the Telegraph Mine Associates management committee hired mining engineer Martin Hughes, to evaluate the mining and gold extraction operations from an independent viewpoint. He reported that "This project has been initiated in a very good and effective manner. The property, if properly supported, it is now at the point of consistent operation and good results." (Hughes, 1982).

Hughes made several recommendations, mostly focusing on additional assaying and check assays, grade control, agglomeration methods, and the recovery plant.

Nonetheless the dispute between the Gold Techniques Group and the Cascade Group escalated, and crushing and haulage of ore was discontinued on October 7, 1982, although the plant at the mine site continued to process solution from the pregnant pond until the end of January of 1983, at which time the entire operation was shut down (oral communication, David Weston, 2013).

In October, 1982, upon receipt of Hughes' report the Gold Techniques Group filed a complaint against Rex Montis, Cascade and others, in the Superior Court of California. In 1983 the Cascade, on behalf of the Cascade Group, filed a complaint in the United States District Court for Utah (Cascade v. Banks, C82-1223C) to find the Gold Technics Group in default and for non-payment of assessments; this filing stayed the California action. In its final judgment following a five day trial, the District Court terminated the Gold Technics Group's interest in the Telegraph Mine for default without any refund of their cash invested ($1,050,000). The Court also found in favor of the Gold Technics Group that the collection of production costs was not a contractual obligation and required in its judgment that those monies collected be refunded. In addition, the Court found that there was no common-law fraud in the sale of the sublease interests nor any negligent misrepresentation and that the sale of the sublease interest was not a security. The Gold Techniques Group appealed, and on appeal the appellate court ruled the sale of the sublease interest was a security and ordered a new trial to determine whether there was security fraud in the sale based upon the preponderance of the evidence standard. Following a second trial the District Court ruled there was no securities fraud nor any scienter (*i.e.*, deception, illegality, etc.) in the sale of the sublease interests.

On January 17, 1986, after the time for appeal of the second District Court decision by the Cascade Group had expired, the Gold Technics Group appealed to the Tenth Circuit Court of Appeals (Cascade v. Banks 896 F.2d 1557). However, following the District Court trial, evidence regarding gold production from the Telegraph Mine was lost and this information did not go forward on appeal to the Tenth Circuit Court. The Tenth Circuit Court sustained the District Court's judgment returning the assessments on the basis that no gold had been produced. However the court also held that the associates would have been liable up to the amount of the gold mined had gold been produced.

When it was discovered that evidence items were missing from the record on appeal, the Cascade Group asked the District Court on remand for a new trial to have the District Court make findings as to the amount of gold produced and sold. The District Court denied the motion citing that it was the appellant's (the Cascade Group's) responsibility to ensure a complete record on appeal, and the Tenth Circuit Court in the subsequent appeal of this issue following Remand (Cascade v. Banks, 85 F.3d 640 (10th Cir. 1/17/1996) refused to reconsider its decisions based on the law of the case doctrine.

In the Remand proceeding, the Gold Technics Group took the position that an ore milling receivable owing to the Telegraph Mine Joint Venture from the Associates for the Joint Venture's contract to crush and move the Telegraph vein ore to the leach stockpile was collectible, and thus they were entitled to their share of this collectible. The Gold Technics Group took the new position that the Circuit Court in the first appeal had found that the Associates Joint Operating Agreement provided that if gold ore was mined, milled and removed, the contract provided for assessments up to the value of gold in such ore.

The Cascade Group believed that this was an admission by the Gold Technics Group of contract assessability. The Cascade Group in response then argued the Circuit Court made erroneous findings regarding the production of gold (due to lost evidence), but the District Court denied the Cascade Group's motion for new trial and motion to make findings as to the amount of gold produced.

During the litigation in 1983 the Gold Techniques Group filed a *lis pendens* (a notice of pending action) lien against the Telegraph Mine property and obtained an injunction enjoining the "taking possession of, or otherwise disposing of or impairing the rights of the Associates in the mine project." On October 15, 1985, the Gold Techniques Group asserted a secured interest in the Telegraph Mine property by the recording in San Bernardino County, California (where the Telegraph Mine is located) the Utah District Court's money judgment for return of assessments. On April 10, 1986 they again recorded the judgment as a lien against the mine property. These liens were deemed improper and ordered removed by the United States Court for the District of Utah in 1989 (although the removal did not occur until 1997, see below).

At the time of the first Cascade v. Banks appeal, the Cascade Group had posted a $400,000 *supersedeas* bond (a defendant's appeal bond posted as a type of surety bond to delay any enforcement of a judgment until the appeal is over) to cause a release of the Gold Techniques Groups *lis pendens* so the project could be refinanced and move forward. At the time of the posting of *supersedeas* bond the Gold Technics Group withheld the fact that in addition to the *lis pendens* they had also recorded the judgment as a lien in California. The Cascade Group believed at the time of the *lis pendens* posting that the *lis pendes* was the only encumbrance the Gold Technics Group had posted.

In the spring of 1983, to realign the parties for the purpose of funding continuing operations of the Telegraph Mine, the Cascade Group of the Associates organized Telegraph Resources, Inc., ("Telegraph Resources"), a Utah corporation, and transferred their sublease interests to Telegraph Resources and became shareholders. In May of 1985 all of the interests in the Telegraph Prime Lease were transferred to Telegraph Gold Corporation, a Utah corporation, in exchange for stock. In June of 1985 the Cascade Group of the Associates exchanged all their shares of Telegraph Resources stock for stock of Telegraph Gold Corporation and Telegraph Resources became a subsidiary of Telegraph Gold Corporation, now a public company ("Telegraph Gold").

On November 1, 1986, the Cascade Group, believing that it had secured a clear title to its Telegraph Mine property by filing the *supersedeas* bond, encumbered the Telegraph patented claim, in favor of the Zero Convertible Premium Gold Bonds Indenture Trustee for the purpose of selling one million dollars of Telegraph Gold bonds in California, Hawaii, Utah and Idaho. On April 17, 1987, due to equipment foreclosure proceedings, Cascade Energy and Metals filed a petition under Chapter 11 of the Bankruptcy Code and filed its first disclosure statement dated December 29, 1987. In January, 1988, the Gold Technics Group objected, claiming the statement failed to disclose their recorded judgment. This was the first time the Cascade Group learned of the Gold Technics Group's recording of the Utah judgment in California. Because the lien was not removed, the Zero Convertible Bonds were not sold, nor could the property be joint-ventured.

On May 21, 1989, the U.S. Bankruptcy Court entered an order holding that the Gold Technics Group had improperly recorded the District Court money judgment and that it did not create a valid lien on the Telegraph Mine property in San Bernardino County. Although the judgment liens were held to be invalid, the Gold Technics Group were found not to be liable pursuant to the California privilege statute and subsequent appeals by the Gold Technics Group prevented the liens from being finally removed until 1997. The Cascade bankruptcy was not dismissed until 2005.

Hence from 1982 until the Cascade bankruptcy was dismissed in 2005 the property was in a "legal limbo" which precluded any mining operations.

In 2005, HMI Lenders LLC, ("HMI") (a Utah limited liability company) comprised of the *supersedeas* bond providers, acquired the Telegraph Mine property from Cascade following its bankruptcy court proceedings. HMI subsequently formed a joint-venture on the property (the Telegraph Mine Joint Venture) with Investigold Ventures II LLC, and the Telegraph Mine Joint Venture in 2010 leased the Telegraph Mine to Mojave Gold Mining Corporation.

**Lange-Weston In-Depth Analysis (1984-1988)**

From 1984 through 1988, Peter Lange, a geologist, assisted by W. David Weston, conducted a study of the economic geology of the mining claims of the Telegraph Mine. The study defined the mineralization at the property; identified mineralizing fluid movement, fluid temperature, and fluid pressure of the hydrothermal mineralizing system; defined the relationship of the fault zones and breccia configurations to ore shoots; evaluated fluid inclusions in vein rocks; identified the distribution of gold, silver and trace elements throughout the vein systems and determined an age for the deposit. The study incorporated the drill hole and sample data derived by the several operators' and lessees' prior drilling and sampling, as well as that of Cascade Energy and Metals. Lange created geological maps on a scale of 1 inch = 20 feet for the Telegraph main vein and mapped the regional geological settings at a scale of 1 inch = 200 feet. Over 300 hand samples were collected for geochemical and fluid inclusion studies. Lange found that the finding of the prior geological reports of Mr. Ito, Mr. Owens and Dr. Jensen were consistent with his own findings.

Some of Lange's studies were also incorporated into a Master's degree thesis at Colorado State University (Lange, 1988). Lange's thesis is an excellent work that has stood well the test of time. In it he discusses: (1) the regional geologic setting, (2) the district petrology, (3) the district structural geology and its relationship to the regional structural setting of the southwestern Basin and Range, (4) the district mineralization, (5) Telegraph Mine alteration and mineralization, (6) geochemical implications of his study of fluid inclusions from the vein, (7) the Telegraph system fluid chemistry, and (8) the age and evolution of the Telegraph system. Lange's thesis is referenced numerous times in this report.

Lange's (1988) studies concluded that the top of the boiling zone at the Telegraph Mine was essentially at the surface from Hill No. 1 to Hill No. 3, but that is had been down-dropped by 150 feet north of Hill No. 3. The epithermal boiling deposit model of Lange (1988) predicted that the gold mineralizing events of Stages III, IV and V would extend the average grade of mineralization to a depth of 1500 feet.

The reader is referred to Lange's thesis (Lange, 1988) for additional detail on the geology, alteration and evolution of the Telegraph system. A copy of Lange's thesis can be acquired from Mojave Gold Mining Corporation, 216 Paxton Ave., Salt Lake City, UT 84101.

**1986 Estimation of Gold Remaining on Leach Pad by Charles H. Pitt**

In 1986 Charles H. Pitt, Professor of Metallurgy at the University of Utah, was retained to determine the recoverable gold content of the material on the Telegraph leach pad. Pitt based his estimate on 440 blast hole assays taken on 5-foot intervals during mining and 247 truck load assays taken for each 10.4 tons loaded to the leach pile (Appendix H). He estimated that 24,646 tons of ore had been stacked on the pad containing 5888 ounces of gold. Based on metallurgical studies by Dawson laboratories and the U.S. Bureau of Mines, he estimated 72% of the gold was recoverable through heap leaching, for 4239 ounces of recoverable gold. Accepting an estimate of 300 ounces already removed from the heap, Pitt estimated the recoverable gold remaining would be 3939 ounces and that at an assumed flow rate of 270 tons of cyanide solution per day with a gold content of 13 ounces. Under optimum leaching conditions approximately 303 days would be required to extract the estimated remaining values. (Pitt, 1986.)

**Department of the Interior Unpatented Mining Claim Validity Contest**

In March of 2004, the Department of the Interior challenged the validity of the twelve unpatented claims (Telegraph Nos. 4, 5, 6, 7, 8, 19, 20, 32, 33, 34, 35 and 80) held by Cascade Energy and Metals within the Mojave National Preserve. The patented claims had previously been determined to be valid by the Bureau of Land Management and had been patented to Cascade in 1984. Mining on NPS land is governed by 36 CFR Part 9. Pursuant to the California Desert Protection

Act, before any mining can commence a claimant must have an approved Plan of Operations, a determination of valid existing rights and an approved environmental report.

The Interior complaint charged that: (a) minerals had not been found within the limits of the unpatented claims in sufficient quantities and/or qualities to constitute a valid discovery of a valuable mineral deposit in 1994, the date of withdrawal pursuant to the California Desert Protection Act of October 31, 1994, (Public Law 103-433; CDPA); and (b) the lands are non-mineral in character. The complaint asked that the mining claims be declared null and void.

In 2005 the Telegraph Mine patented and unpatented claims were obtained by HMI Lenders LLC ("HMI") as part of the final resolution of Cascade's bankruptcy, and subsequently HMI entered into the Telegraph Mine Joint Venture with Investigold Ventures II LLC ("Investigold"). The joint venture was (and still is) a partnership owned 77.45% by HMI and 22.55% by Investigold.

HMI Lenders defended contending that: (a) minerals had been found in sufficient quantities and/or qualities to constitute a valid discovery of a valuable mineral deposit on the unpatented claims either within the limits of the claim or by virtue of the down-dip extension of the mineralized vein pursuant to extra lateral rights through Apex rights with respect to the mineralized veins; and (b) the land comprising the unpatented claims both separately and collectively are mineral in character.

A hearing was held on January 8 through 11, 2008. During the hearing, HMI Lenders defended only unpatented claims Telegraph Nos. 4 through 8, inclusive, and Nos. 34 & 35 (Figure 1). Department of the Interior Administrative Law Judge Harvey Sweitzer rendered a decision on March 23, 2009, finding that inference of values from the main Telegraph vein could not be inferred for the unpatented claims. HMI Lenders appealed Judge Sweitzer's decision, which was upheld by the Interior Board of Land Appeals. This matter is now before the United States District Court for the District of Utah. A copy of HMI's brief filed with the U.S. District Court for Utah, Case No. 2:11-cv-00504-DB is available upon request from Mojave Gold Mining Corporation, 216 Paxton Ave., Salt Lake City, UT 84101. The decisions in this matter should have minimal effect on production from the main Telegraph vein where under existing Apex Law the Telegraph main vein outcrops on the Telegraph patented claims and can be followed and mined extra-laterally wherever the vein exists.

**2006 Drilling, 2007-2008 Ryzak Study**

In 2006 geologist David Ryzak, a development and mine production geologist with 30 years' experience with several mines in the western U.S., examined the Telegraph Mine property on behalf of Rocanville Corporation ("Rocanville"), a Texas corporation interested in becoming a partner in the property. As part of Rocanville's assessment of the property a 380-foot vertical drill hole was collared 500 feet west-southwest of Shaft No. 2 (Hill No. 2) on the Telegraph No. 8 unpatented claim (Figures 7 & 13). Details on the drill hole can be found in section **10. Drilling** below.

In 2007 and 2008 HMI Lenders contracted Ryzak to conduct an economic assessment of the Telegraph Mine as an expert witness in the legal proceedings regarding claim validity with the Department of the Interior. Mr. Ryzak's testimony was taken on January 9, 2008.

Ryzak calculated an open-pit mineable resource along the vein with a strike length of 2,000 feet extending from the northern end of the Telegraph South claim across the telegraph claim to the southern end of the Telegraph Extension claim to depth of 130 feet down-dip. He determined a resource of 89,700 ounces of gold in 345,000 tons of ore averaging 0.26 opt Au across a width averaging 45 feet; his proposed pit had a 4:1 strip ratio. Ryzak also calculated an underground mineable resource of 81,600 ounces of gold the vein averaging 0.48 opt Au gold with an average width of 4½ feet from the lowest portion of his hypothetical open pit to the 500-foot vertical depth. (David Ryzak testimony, January 9, 2008, U.S. District Court for Utah, Case No. 2:11-cv-00504-DB.)

**Present Ownership and Telegraph Mine Lease**

HMI Lenders LC owns 77.45% and Investigold Ventures II LLC owns 22.55% of the patented and unpatented mining claims. These parties have formed a joint venture known as the Telegraph Mine Joint Venture with Stone Resources LLC as its manager. In 2012 the Telegraph Joint Venture leased the mining claims to Mojave Gold Mining Corporation for mine development and gold and silver recovery. The lease requires minimum annual payments of $25,000 for the first year commencing January 1, 2013, $50,000 for the second year and $100,000 for each year thereafter reduced by any production royalty payments. The production royalty is 6¼% of the net smelter returns when the price of gold is less than $900.00 per ounce or 7¼% of the net smelter returns when the price of gold is greater than $900.00 per ounce.

## 7. Geological Setting and Mineralization

The Halloran Hills contain rocks ranging in age from the Proterozoic to the latest Holocene (Figures 14 & 15). Precambrian rocks exposed north of the Telegraph Mine area include older, mid-Proterozoic (1800 to 1600 Ma) amphibolite facies biotite gneisses and mafic meta-volcanics and younger foliated gneissic granite to granodiorite rocks overlain by Upper Proterozoic (1100 to 1300 Ma) metamorphic carbonates and quartzites of the Pahrump Group and the Johnnie formation.

Paleozoic rocks in the central Halloran Hills include limestone, shale and quartzite of the Cambrian Riggs Formation, Carrarra Formation, Zabriski Quartzite and Wood Canyon Formation. The Crystal Springs Formation of the Pahrump Group and the overlying Riggs Formation host small base metal replacement deposits in the Silurian Hills (Henderson, 1984) northwest of the Halloran Hills.

Much of the exposed rock in the Halloran Hills (50%?) is composed of Cretaceous igneous intrusions (Figures 14 & 15). The Teutonia quartz monzonite appears to be a composite pluton with as many as eight distinct calc-alkalic to alkalic bodies in three domes stretching from the northwest Halloran Hills to Cima Dome (Hewitt, 1956).

In the Halloran Hills Hewitt (1956) identifies a sequence including:

- an early granodiorite to quartz diorite;
- a three-phase zoned pluton with a granite core and outer quartz monzonite and a peripheral quartz monzo-diorite;
- a large leucocratic adamellite body; and
- separate stocks of leucocratic muscovite-garnet adamellite and late-stage aplite dikes and plugs.

Miller *et al.* (2007) map six distinct units of the Teutonia batholith. They show the Teutonia adamellite (Kt) as the dominant bedrock unit in the area of the Telegraph Mine (Figure 14) and describe it as follows:

> *Informally named unit. White to light-tan, equigranular to porphyritic (contains pink alkali-feldspar phenocrysts) biotite monzogranite, generally medium and coarse-grained. Locally varies in composition to syenogranite and quartz monzonite. Minor muscovite present in places. .... Crops out over much of Cima Dome, where it was dated at 97 Ma in age by U-Pb methods on zircon (DeWitt and others, 1984).*

They also show presumed Cretaceous biotite-rich granitiod rocks (Kb, Figure 14) that crop out a mile south of the Telegraph Mine area, a unit including Miocene rhyolite lava flows and ash flows, tuffaceous sedimentary rocks, tuff breccia, basalt flows and andesite flows ($Tv_2$) a mile and a half east of the mine area, and two small outcrops of Pleistocene to late Miocene basalt lava flows (QTbl) a mile and a half to the southeast. Another mapped unit in the local area of the Telegraph Mine is described as Pliocene and Miocene moderately consolidated and crudely bedded gravel, sand, debris flow deposits, avalanche breccia and gravity-slide breccia (Tg). (Figure 14.)

Lange (1988) includes a much more complex map of the Halloran Hills area which he modified after DeWitt (1980). Lange's approximately 1:500,000-scale map of the Halloran Hills is included herein as Figure 15.

The Telegraph Mine hosts a low-sulfidation, quartz-adularia, epithermal gold- and silver-bearing quartz breccia-vein system hosted in a Miocene fault in the Cretaceous Teutonia adamellite (quartz monzonite or monzo-granite). The Telegraph vein system has been shown to displays some 3500 feet-plus of strike and averages about 4 to 5 feet in width; however, the structure that contains the vein has substantially greater strike length, and the vein may also. It has been interpreted by Lange (1988) to be a boiling-type epithermal deposit.

Lange (1988) describes the Telegraph vein system as:

> *.... composed of rebrecciated wall rock fragments replaced and cemented by products of five stages of hydrothermal fluids. The main breccia zone ranges in width from 0.3 m to 3.3 m and is bounded by wall rocks extending 0.5 m to 24 m from the main zone.*

Lange (1988) uses the classification of Sillitoe (1985) in calling the breccia vein "tectono-hydrothermal." Through careful petrographic examination of many samples he determined that both hydrothermal and tectonic factors contributed to the fragment distribution and transport in each paragenetic stage.

# 8. Deposit Type

The Telegraph Mine is a low-sulfidation (quartz-adularia) epithermal gold & silver deposit. Gold- and silver-bearing epithermal breccia-veins, which consist of quartz-sericite-adularia-pyrite and quartz-carbonate, cut the informally named Cretaceous Teutonia adamellite. Although the breccia-veins are hosted in a fault in the Cretaceous intrusive rocks, the age of the mineralization is presumably 10.3±0.4 Ma (Lange, 1988), and likely related to volcanic activity. Hence the deposit is likely best classified as a volcanic-associated low-sulfidation precious metal deposit.

The breccia-veins are composed of brecciated and rebrecciated wall rock (adamellite) cemented by products of the mineralizing hydrothermal fluids: dominantly quartz, adularia, illite, sericite, calcite, other carbonates, and minor pyrite. Central zones of the breccia-vein contain a larger percentage of rebrecciated clasts, smaller clast sizes and a higher percentage of open-space hydrothermal mineral matrix.

The breccia-vein ranges from 1 to 11 feet (0.3 to 3.3 meters) in width and is bounded by altered and more weakly mineralized wall rocks extending 1.5 to 90 feet (0.5 m to 24 meters) from the main zone (Lange, 1988). The main outcrop zone of the Telegraph vein stretches 2000 feet (600 meters) from Hill No. 1 on the southwest to Hill No. 3 to the northeast. However, the breccia-vein system also extends to the north well beyond Hill No. 3 to the northern end of the Telegraph Extension claim and to the south beyond Hill No. 1.

To the north-northeast of Hill No. 3 the vein can be traced some 1200 feet (350 meters) to the northern end of the Telegraph Extension claim. All but two of eleven percussion drill holes drilled in 1981-1982, on the northern portion of the Telegraph Extension claim (the "Northern Extension Area") had intercepts of greater than 1 g/T Au and the two without 1 g/T Au intercepts had >0.5 g/T Au intercepts. (Figure 11, Table 8 and Appendix D). Towards the northern end of the claim, the strike of the N28$^0$E-striking Telegraph vein appears to be curving to the west and tracking to the north and west of north.

There is an abrupt break in topography from relatively hilly and steep on Hill No. 1 to relatively flat to the south of Hill No. 1. This may very well reflect a fault. Two of Ito's core holes (nos. 8 and 15) were drilled towards the projection of the Telegraph vein in the area immediately south of Hill No. 1 (Figure 7). Neither intercepted vein material (Ito, 1969). However, immediately adjacent to the south-southwest of the Telegraph South claim, although off-set to the southeast by about 300 feet (100 meters) are the Aqua Dulce Nos. 1, 2 & 3 claims, also oriented to the north-northeast, essentially parallel to the three patented Telegraph claims. The three Agua Dulce claims were included in the same Mineral Survey (M.S. 6792) as the three patented Telegraph claims. The mineral survey shows a discovery cut on the centerline of each of the Aqua Dulce claims. These cuts and numerous others on the Aqua Dulce claims are on a structure that is sub-parallel to the main Telegraph vein to the north and may be the southern extension of the Telegraph fault, suggesting an extension to the south-southwest of at least 4500 feet (1500 meters) of the Telegraph vein system south of Hill No. 1.

Lange (1988) cites six distinct tectonic/hydrothermal events displaying distinct structural and textural relationships and hydrothermal mineral assemblages. Stage I & Stage II wrench faulting produced chlorite+montmorillonite-altered fault gouge within *en echelon* segments of the Telegraph Fault. Subsequent movement resulted in "nested" 0.3-meter to 3.3-meter silicified breccia zones including: an outer Stage III breccia with a quartz-adularia-pyrite matrix; an inner Stage IV breccia with a quartz-illite-sericite-pyrite matrix; overprinting Stage V veins and crackle breccia cement of quartz-adularia-calcite-pyrite; and crosscutting Stage VI quartz-carbonate fissure veins (Figure 16). Micron-sized gold occurs in each stage, along with silver and mercury. In ore shoots average Au:Ag ratios are 1:1. (Lange, 1988.)

Fluid inclusion analysis by Lange (1988) revealed that the hydrothermal fluids of successively younger stages were progressively cooler, less saline and less acidic, and probably boiled under lessening confining pressures. His studies showed liquid-dominated, very low $CO_2$-bearing, two-phase fluid inclusions in quartz from Stages III, IV and V had entrapment temperatures of 282$^0$C, 260$^0$C and 203$^0$C, respectively. His salinity measurements ranged from 5.0 % NaCl-equivalent (Stage III) to 1.7% NaCl-equivalent (Stage V). He calculated trapping pressures which suggested, assuming near-hydrostatic conditions, a range in boiling depths during the period of mineralization from 720 meters (Stage III) to 560 meters (Stage IV) to 160 meters (Stage V) below the local water table. (Lange 1988.)

Per Lange's paragenetic analysis, the main stages of gold mineralization were Stages III and IV with significant expanded open-space volume leading to Stage V boiling with additional gold mineralization (Lange, 1988 & 2008).

Lange's (1988) studies also concluded that the top of the boiling zone at the Telegraph Mine was essentially at the surface from Hill No. 1 to Hill No. 3, but that is had been down-dropped by 150 feet north of Hill No. 3. The epithermal boiling deposit model of Lange (1988 & 2008) predicted that the gold mineralizing events of Stages III, IV and V would extend the average grade of mineralization to a depth of 1500 feet.

The normal-right lateral Telegraph vein was interpreted by Lange (1988) to have formed within a dextral strike-slip environment, related to the N-S wrenching of the San Andreas and Death Valley Faults and probably the E-W extension of the Southern Basin and Range. The strike of the Telegraph Fault is now to the north-northeast, at a high angle to trends of the regionally extensive strike-slip faults. The mineralization is associated spatially with structures interpreted by Lange (1988) as Riedel shears, which are secondary shears oriented generally at low angles to the general trace of a broad zone of shear. Prominent geomorphic and structural features trending N 20° to 40° E in the general area of the Telegraph Mine acted as open conduits or as breccia-filled high-permeability zones during the mineralization, which has been dated 10.3±0.4 Ma, based on single K-Ar age on adularia (Lange, 1988).

This type of mineralization (near-surface epithermal quartz-adularia gold mineralization hosted in right-lateral strike-slip faulting in substantially older rocks) may be particularly significant in terms of evaluation of the resource because of its geologic similarity to the world-class gold deposit at the Mesquite Mining District, California (Tosdale and Theodore, 2007).

Tosdal and Theodore (2007) describe the Telegraph Mine as appearing to have an analogous setting to Mesquite Mining District located in Imperial County, California, 150 miles (250 km) to the south-southeast of the Telegraph Mine and 45 miles (70 km) northwest of Yuma, Arizona. Large-scale gold production from the Mesquite Mining District began in 1985; as of December 31, 2012, New Gold Inc. reported proven and probable reserves of 2,342,000 troy ounces of gold in 127,549,000 tons of ore with an average grade of 0.57 g/T Au and measured and indicated oxide and non-oxide resources of 5,684,000 troy ounces of gold in 394,100,000 tons with an average grade of 0.45 g/T Au, at their operating Mesquite property (New Gold Inc. press release, February 5, 2013, available on SEDAR).

From Tosdal & Theodore (2007):

> *Gold-bearing veins in the Mesquite Mining District formed in an epithermal setting within a few hundred meters of the surface (Willis and Holm, 1987; Manske and others, 1987; Willis, 1988; Manske and Einaudi, 1989; Manske, 1990; Willis and Tosdal, 1992). Gold-bearing quartz-adularia-sericite and ferroan-carbonate veins are the mineralized structures within the district (Willis, 1988; Manske, 1990). Quartz-cemented breccias are contemporaneous with the simple veins and are common in the parts of the deposit that have the highest economic grades. Younger, barren calcite veins and chalcedonic-quartz veins are present locally. Vein deposition occurred by episodic open-space filling, as indicated by vuggy and comb quartz and carbonate minerals, multiple banding of chalcedonic quartz, and*

*clasts of silica-matrix breccia within other breccias. Veins vary from thin microcracks to breccias a meter or so thick. Little hydrothermal alteration of host lithologies accompanied mineralization (Manske and others, 1987; Willis, 1988). Weakly anomalous, sporadic concentrations of Au, Ag, As, Sb, Hg, W, Zn, and Te were found in surface-rock exposures before mining (Tosdal and Smith, 1987).*

*The veins are steeply dipping and are strongly controlled by right-lateral strike-slip faulting (Willis, 1988), as indicated by the vein geometry in complex dilational jogs (Sibson, 1990), by negative and positive flower structures (Harding, 1985), and by kinematic evidence for strike-slip faulting along the major mineralized faults (Willis and others, 1989; Willis and Tosdal, 1992). Mineralization in the mining district is hosted mostly by gneissic rocks that were metamorphosed at amphibolite grade and, to a lesser extent, by granite, pegmatite, and aplite that intrude the gneissic rocks (Willis, 1988). The ages of these rocks and their subsequent metamorphism have been established as Jurassic and Cretaceous, respectively (R.M. Tosdal, unpub. data, 1987–90). K-Ar and 40Ar/39Ar geochronologic studies indicate an Oligocene age of mineralization sometime between 37 and 27 Ma (Willis, 1988; see also D.L. Martin, as quoted in Shafiqullah and others, 1990), or a minimum of 60 m.y. after the host rocks were formed. The apparent age of the orebodies is, however, somewhat similar to the age of nearby volcanic and plutonic rocks in the Chocolate Mountains (Miller and Morton, 1977; Crowe and others, 1979). No Tertiary volcanic or plutonic rocks are known within the Mesquite Mining District, although they may have provided a heat source to drive the hydrothermal system (Manske, 1990).*

*The large gold deposit in the Mesquite Mining District is a typical epithermal precious-metal deposit similar to many of those hosted by volcanic rocks or by other rocks that are intruded by hypabyssal stocks elsewhere. Major distinctions between orebodies in the Mesquite Mining District and typical epithermal deposits include the gneissic host rocks, the large difference in age between the host rocks and the orebodies, and the lack of volcanic or plutonic rocks of the appropriate age within the district. The strike-slip environment is not unique, although it does provide a structural setting into which hydrothermal fluids could flow away from any associated heat source (Sibson, 1987).*

Similarly the Telegraph Mine vein is interpreted to be a low-sulfidation quartz-adularia epithermal gold deposit. The Miocene-age gold-bearing epithermal quartz-sericite-adularia-pyrite and quartz-carbonate breccia-veins at the Telegraph Mine, likely related to contemporaneous volcanic activity, cut the much older intrusive Cretaceous Teutonia adamellite. At Mesquite Oligocene epithermal gold-bearing quartz-adularia-sericite and ferroan-carbonate veins of similar age to nearby volcanic and plutonic rocks cut Jurassic- and Cretaceous-age metamorphic and intrusive rocks. Both deposits are interpreted to be volcanic-related and emplaced in older rocks in fault/fracture systems that were likely related to the regional extension of the Southern Basin and Range.

## 9. Exploration

No exploration, other than the historic work previously referenced, has been done on the Telegraph Mine property. No exploration activities were conducted as part of this report.

Historic sampling, including drill testing, was reportedly done or supervised by seasoned professionals abiding by industry standards current to the time. All sampling is believed to have been representative unless noted otherwise in the reports accompanying the data.

Historic drill results are discussed in section **10. Drilling** below.

## 10. Drilling

No drilling was done as part of this report.

The Telegraph Mine has, however, seen several historic drill programs since 1968.

**1968-1969 Tomo Ito Drill Program**

In 1968-1969 Tomo Ito (geologist/metallurgist) drilled along the Telegraph main fissure vein at a cost of $30,000, funded in part by a U.S. Government Office of Minerals Exploration (OME) Loan (USGS-OME 6727). Ito drilled fourteen holes totaling 2079 feet, including 549 feet of core, during the program between December 9, 1968, and March 20, 1969 (Ito, 1969). A modified copy of Ito's drill map is included as Figure 7.

Nine of his holes, Nos. 1, 2, 3, 4, 5, 6, 9, 10 and 12, between Hill No. 1 (Shaft No. 1) and Hill No. 3 (Shaft No. 3), recovered gold- and silver-bearing vein material. Hole no. 14 had poor recovery through the potential vein intercept. Hole 11 encountered no vein material, but Ito suspected that the main vein may have been offset to the east in this area sufficiently to prevent intersection by the drill hole (the local topography, with the ridge offset to the east, may also suggest such). Hole no. 7 in the area of Shaft No. 1 may very well have encountered mined-out stopes, but had no visible showings of vein material. Hole no. 15, south of Shaft No. 1 had no showings of vein material and Hole no. 8 had only a few weak stringers and was not sampled. Cross-sections of the drilling are included in his Operators Final Report (Ito, 1969).

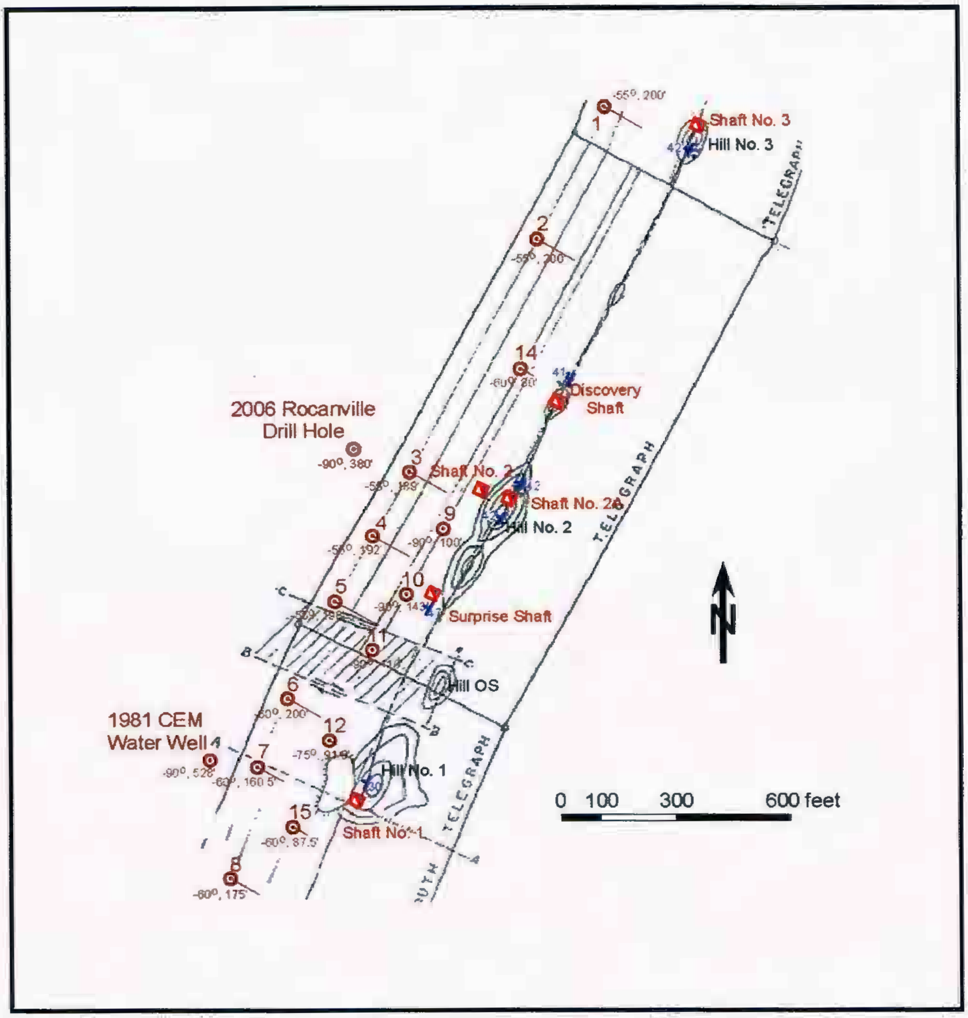


Figure 7. Tomo Ito's 1969 "Layout of Drill Holes" map with 1981 Cascade Energy & Metals water well drill hole and 2006 Rocanville Corporation drill hole added (modified from Ito, 1969, Figure DH).

From Ito (1969):

*Our drilling program was concentrated between shafts No. 1 and No. 2, but we were hopeful of extending our ore reserves both to the north and south.*

1) *Area north of No. 2 shaft – distance of 1100 feet from No. 2 to No. 3, with 4 exploratory holes. Average vein width of 4 ft. with vertical depth of 150' of vein on dip (height) of 200 feet.*
2) *Area between shaft No. 1 and No. 2 – distance of 900 feet; average width of 4 feet; extending down dip for 200 feet. The block containing hole 11 and Hill OS appears to have moved east in relation to the blocks to the north*

*and to the south. In other words, the main vein has been offset to the east sufficient to prevent intersection by our drill hole.*

*3) The camp area, just south of No. 1 shaft produced no evidence of vein structure below line A-A. ... This was not expected as there are quite extensive shallow diggings in this area, according to oral communication with parties who worked in No. 1 shaft. There is an obvious displacement here which requires more exploratory work to establish.*

*The results of the drilling indicates [sic] good vein structure to at least a depth of 200 feet on the dip from shaft No 3 southward to shaft No 1.*

Ito believed that the determination of the vein thickness, structure, attitude and composition could be done from the results of the drilling with a fair bit of accuracy, but the tenor of the ore was difficult to assess due to poor core recovery and likely highly diluted sludge. However, through sampling of many surface outcrops and cuts and underground workings and careful review of old records, as well as consideration of carefully selected samples at the end of his program, he determined an average grade of 0.51 opt gold and 1.16 opt silver. He assigned an average width of 4 feet to the vein. (Ito, 1969.)

**1981 Water Well**

In December of 1981 Cascade Energy & Metals drilled a vertical 528-foot well for water approximately 400 feet west of the Telegraph Mine Shaft No.1 on the Telegraph No. 4 unpatented claim at 576 West and 3175 South on the main Telegraph grid (Figures 7 & 8). The well intercepted the projected mineralized shear zone at depths of 307 to 314 feet and 364 to 371 feet (Jensen, 1981). Analyses by Cascade indicated that the zone from 307 to 314 feet contained 0.005 oz./ton (0.171 ppm) gold and 0.627 oz./ton (21.5 ppm) silver and the zone from 364 to 371 feet contained 0.039 oz./ton (1.342 ppm) gold and 0.400 oz./ton (13.7 ppm) silver.

Taking these intercepts into consideration, Jensen (1981) then estimated the resource at 300,000 tons based on the drill hole results and persistence of the vein with depth (i.e., 450' deep x 4.0' wide x 2000' long /[12 $ft^3$/ton] = 300,000 tons).

**1981-1982 Percussion Drill Hole Program**

In late 1981 and 1982 Cascade Energy & Metals on contract to the Telegraph Associates drilled 1,984 feet in 55 percussion exploration holes on the main Telegraph vein on the three patented Telegraph claims and another 712 feet in 13 percussion exploration holes on the Gold Dyke vein on unpatented Telegraph Nos. 34 & 35 claims. Additional holes were almost certainly drilled during this period, but the author has not found reliable data for any drill holes from this program aside from the 68 referenced above.

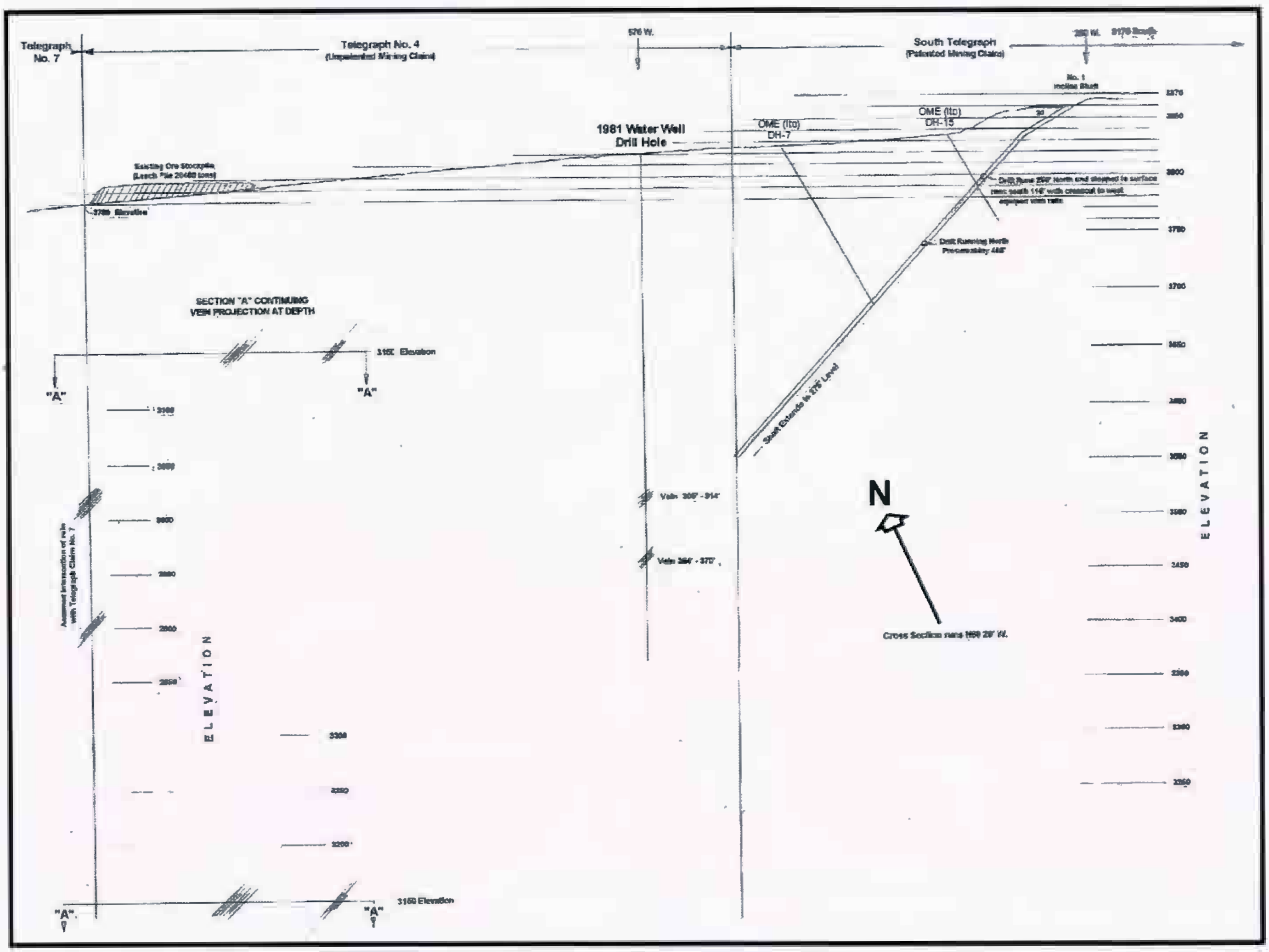


Figure 8. Cross-section of 1981 Cascade Energy & Metals Water Well drill hole on the Telegraph no. 4 claim (modified from HMI Lenders figure).

Figures 9, 10 and 11 show the locations of the 55 percussion holes on the three patented Telegraph claims. Figure 9 shows collar locations and traces of 25 holes that were drilled at the Hill No. 2 area on the Telegraph claim; Figure 10 shows collar locations and traces of 21 holes that were drilled at the Hill No. 1 area on the Telegraph South claim; and Figure 11 shows collar locations and traces of 9 holes that were drilled in the Northern Extension area on the Telegraph Extension claim. Similarly Tables 6, 7 and 8 summarize the 1981-1982 drilling for the three respective areas. Appendices B, C and D contain more detailed data on the drilling including analytical data for each sample and the coded geologic logging from Lange's (1988) Appendix F where available.

Each of Figures 8, 9 and 10 also shows the Telegraph Mine grid established by Cascade Energy and Metals. The sidelines of the Telegraph claims bears N28$^0$43'E (parallel to the main Telegraph vein). The Telegraph mine grid is in feet and essentially parallel to vein and the claim's sidelines with a bearing of $28^0$ east of true north (*i.e.,* "north" on the grid is $N28^0E$); the north arrow shown on each of Figures 8, 9 and 10 is true north. Note that the scale of Figures 8 & 9 is 1:600 (1 inch = 50 feet) while that of Figure 10 is 1:1200 (1 inch = 100 feet).

Data from this drilling has been compiled by the author from historic records from work at the Telegraph Mine in files at Mojave Gold Mining Corporation's Salt Lake City, Utah, office and from information in Appendix F of Lange's thesis (Lange, 1988). That compilation is contained herein in Appendices A, C and D, for the Hill No. 2 area, the Hill No. 1 area, and the Northern Extension area, respectively, with the holes listed in each appendix from north to south by their Telegraph Mine grid coordinates. In some cases the location data and the azimuth and/or incline of the holes in Lange's thesis conflicted with that in Mojave's historic records, and in those cases the Mojave data (from which Lange's appendix was likely compiled) was used unless the Lange data appeared to be almost certainly correct. Lange (1988) used a different numbering sequence for the holes he included in his Appendix F, but holes could be correlated through their location on the Telegraph Mine grid (which was usually included in both sets of records), their length and the analytical results.

Drill-hole numbering by Cascade Energy & Metals was also inconsistent. In some cases more than one hole was given the same number; in some cases holes were not numbered (but were identified by their grid coordinates). In Figures 9 through 11, Tables 6 through 8, and Appendices B, C and D, each hole given a prefix: "2" for the Hill No. 2 area, "1" for the Hill No. 1 area, and "N" for the Northern Extension area, followed by the hole number assigned by Cascade Energy & Metals. For example, at the Hill No. 2 area Cascade's drill hole number 4 is designated "CEM 2-4" in this report. In cases where two holes in an area were given the same number by Cascade, the second hole (by drilling date) is given a suffix "a" after the number. Hence at Hill No. 2 there is a drill hole designated "CEM 2-3" and another designated "CEM 2-3a." Holes which were unnumbered in the historic CEM data have been assigned numbers sequentially following the holes which were numbered, generally from north to south on the Telegraph grid.

Drill cuttings were generally assayed every 2 feet to determine metal content. Gold and silver analyses were generally by atomic absorption with a then state-of-the-art PerkinElmer AA spectrometer in Cascade Energy and Minerals in-house laboratory (named "CEMCorp Laboratory") in Salt Lake City. This technique was deemed more accurate than other analytical techniques available in 1981 at the low levels gold and silver contents in most of the samples (Weston & Dickson, 1983). Gold content of samples ran from nil or a trace to over an ounce per ton, with many in 0.01, 0.02 and 0.03 opt range (see Appendices B, C & D). Analyses from the drilling were given in troy ounces of gold and silver per ton; the original troy ounce per ton values have been mathematically converted to g/T Au in this report; both the opt and g/T values are included in Appendices B, C, D & E. Some samples were also analyzed at Kimball Laboratories and Assay Labs, Inc., both in Salt Lake City, with a similar range of results. Check samples were also routinely run at the other labs.

The Telegraph vein strikes roughly N28$^0$E with measured dips from 30$^0$ to 52$^0$. Most of the drill holes on the three patented Telegraph claims are essentially perpendicular to the vein with azimuths of 118$^0$ (S28$^0$E) and inclines of -45$^0$, and hence most widths of mineralization as shown in Appendices B, C and D are close to true widths. Coded geologic logs for many of these holes are included in Appendix F of Lange (1988) and when available, these are also included in Appendices B, C and D along with an explanation for the coding.

It must be noted that this work was all done prior to implementation of N.I. 43-101, and under the standards of N.I. 43-101, data from this work should not be relied upon.

Additionally the level of precision of the low-level gold analyses done by CEMCorp Laboratory – generally "trace", "0.01" or "0.02" opt Au (= 0.00, 0.34 or 0.68 g/T Au, respectively) – was such that the precision of the lower-level analyses must be considered in any evaluation of this data (*i.e.*, the detection limit of this 1981 work was 0.01 opt Au = 340 ppb Au; common 2013 analyses have a detection limit of 5 ppb Au and a precision of as low as 1 ppb Au, and analytical techniques with even lower detection limits are available today. A 1981 sample with an analysis of 0.34 g/T Au from the CEMCorp work could actually have contained anything from 0.17 to 0.51 g/T Au.)

However, the author believes that the data was collected under then-current industry standard procedures by competent industry professionals and is valid data. Furthermore the assay results from sampling of the drill cuttings from the 1981-1982 program are generally consistent with earlier sampling results, adding further credence to these numbers. Most importantly, this data shows relatively broad areas of significant mineralization at the Telegraph Mine which may not have been important under 1981 economics, but with the rise in the price of gold and improvement in recovery techniques over the past 30 years these areas appear to have excellent economic potential today.

***Hill No. 2 (Shaft No. 2) Area***

Figure 9 shows the locations and surface traces of the 25 holes that were drilled at the Hill No. 2 area on the Telegraph patented claim. Table 6 contains a summary of the drilling at the Hill No. 2 area, and Appendix B contains detailed data from the drilling, including each hole's collar location, azimuth, incline and length, coded geologic logging (where available) and analytical data for each sample.

In the Hill No. 2 area (Figure 9) 10 consecutive holes (CEM 2-1 through CEM 2-10) drilled at an azimuth of 118$^0$ and an incline of -45$^0$ were drilled along the course of the Telegraph vein at mostly 10-foot centers to depths of 30 to 50 feet. Per data from the logs of Lange (1988) these 10 holes showed drill intercepts on the breccia vein ranging from 6 to 12 feet (averaging 9.4 feet).

Two-foot samples across these intercepts contained from 0.03 to 1.69 opt (1.03 to 57.94 g/T) gold and averaged 0.32 opt (10.97 g/T) gold. (See Figure 9, Table 6 and Appendix B.)

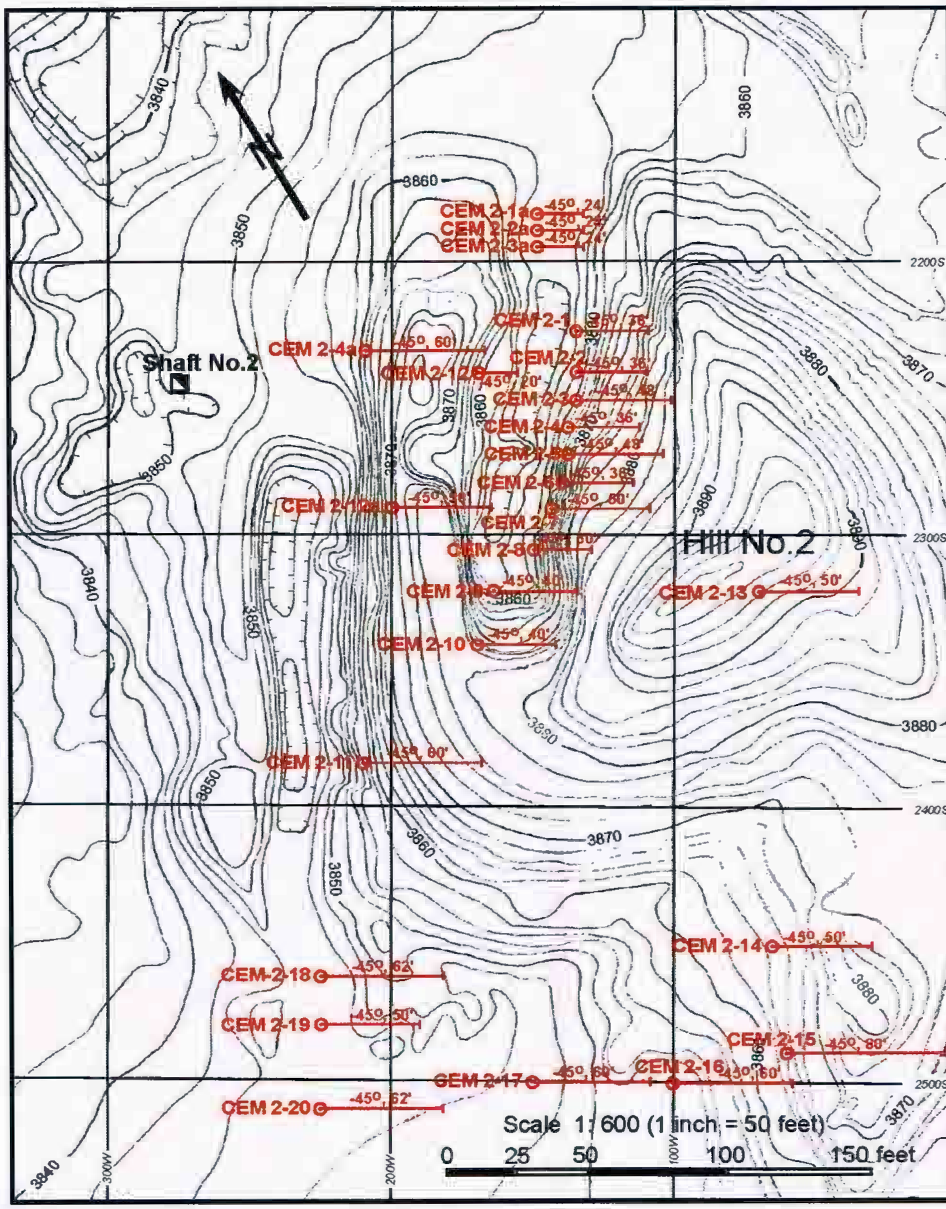


Figure 9. 1981-1982 Cascade Energy & Metals drilling at Hill No. 2 on the Telegraph patented claim (modified after Lange, 1988, Plate 5).

Pursuant to that drilling C.M. Daily, working under contract to Zions First National Bank of Salt Lake City, which was considering making a loan to Cascade Energy and Metals to purchase crushing and screening equipment, affirmed an estimated resource of 108,003 tons (to 30 feet depth down-dip) averaging 0.189 oz. of gold and 1.16 oz. of silver per ton based on the drilling in the Hill No. 2 area, including both the vein and portions of the adjacent mineralized footwall (Daily, 1982). This resource estimate, which was based largely on the ten holes CEM 2-1 through CEM 2-10, is further discussed in section **14. Mineral Resource Estimates**, below.

The results of the 1981-1982 drilling at Hill No. 2 taken as a whole are very impressive. All of the 18 holes drilled north of 2384S in the area, averaged from 1.00 g/T to 16.06 g/T Au over their entire lengths of 24 to 50 feet (Figure 9, Table 6). The mineralized intercepts of most of the holes are open at depth with the last sample in these holes ranging from 1.03 g/T to 9.60 g/T Au.

Holes in the "core area" of Hill No. 2 to the north of 2340S (Figure 9) are among the best drill holes on the Telegraph Mine property. Most of these holes were logged by Lange (1988). Codedgeologic logging data from Appendix F of Lange's thesis is included in Appendix B of this report and indicate that all of these holes encountered mineralized hanging wall, the highly mineralized breccia vein, and mineralized foot wall. Including all samples from each hole, these holes averaged from 1.73 to 16.06 g/T Au across their entire length. (CEM 2-4a, the hole with the 1.73 g/T Au average) was not logged and may have been collared east of the vein or hit the vein in an unmineralized zone; the hole did, however, hit a 2-foot sample of 15.77 g/T from 48 to 50 feet, but this appears likely to have been a stringer vein east of the main Telegraph vein.) Using each hole's average analysis from Table 6 (*i.e.*, not giving more weight to longer holes) the 16 holes north of 2340S in the core area, excluding CEM 2-13, which is east of the core area, average 6.37 g/T Au for their entire lengths of 24 to 50 feet. (See Figure 9, Table 6 and Appendix B.)

While the holes in the "core area" immediately to the west of Hill No. 2 are almost all very good, other holes shown on Figure 9 are of significant interest too. On the east flank of Hill No. 2 and to the south, CEM 2-13, a 50-foot hole, has only 4 2-foot samples containing less that 0.5 g/T Au and has numerous +1.0 g/T Au samples, ranging up to 4.11 g/T Au; the 25 samples from hole CEM 2-13 average 1.00 g/T Au. Data from CEM 2-14, 150 feet to the south of CEM 2-13 are similarly mostly in the 0.5 to 2 g/T range with an average of 0.96 g/T Au for all of the 25 samples collected from the 50-foot hole. CEM 2-15, 40 feet further to the south of CEM 2-14, shows similar mineralization but has a few samples ranging up to 3.09 g/T; the average analysis for the full 80-foot hole is 1.05 g/T Au. (See Figure 9, Table 6 and Appendix B.)

South and slightly west of Hill No. 2, CEM 2-11 is a 60-foot hole with samples ranging from 1.03 to 7.54 g/T Au; the 29 samples from the hole average 2.66 g/T Au. This hole is collared at a lower elevation than the holes to the north and apparently encountered the westerly dipping breccia vein from 8 to 14 feet, then mineralized footwall to the end of the hole at 60 feet. (See Figure 9, Table 5 and Appendix B.)

Further to the south CEM 2-18 showed spotty weak mineralization, but still averaged 0.81 g/T Au. CEM 2-19 encountered weak mineralization near the surface, but the majority of analyses were 0.01 opt (0.34 g/T) Au. CEM 2-20 also returned predominantly 0.01 opt Au analyses. CEM 2-16 and CEM 2-17 each showed spotty weak mineralization and averaged 0.94 and 0.87 g/T Au respectively. (See Figure 9, Table 5 and Appendix B.)

The drilling and the topography both suggest a possible left-lateral off-set on the south side of Hill No. 2. The drilling also suggests that there may be a substantial volume of rock containing +0.5 g/T and/or +1.0 g/T Au is this area. Additional drilling will be needed in this area to determine if a significant structure is present and to better assess the volume of mineralized material here.

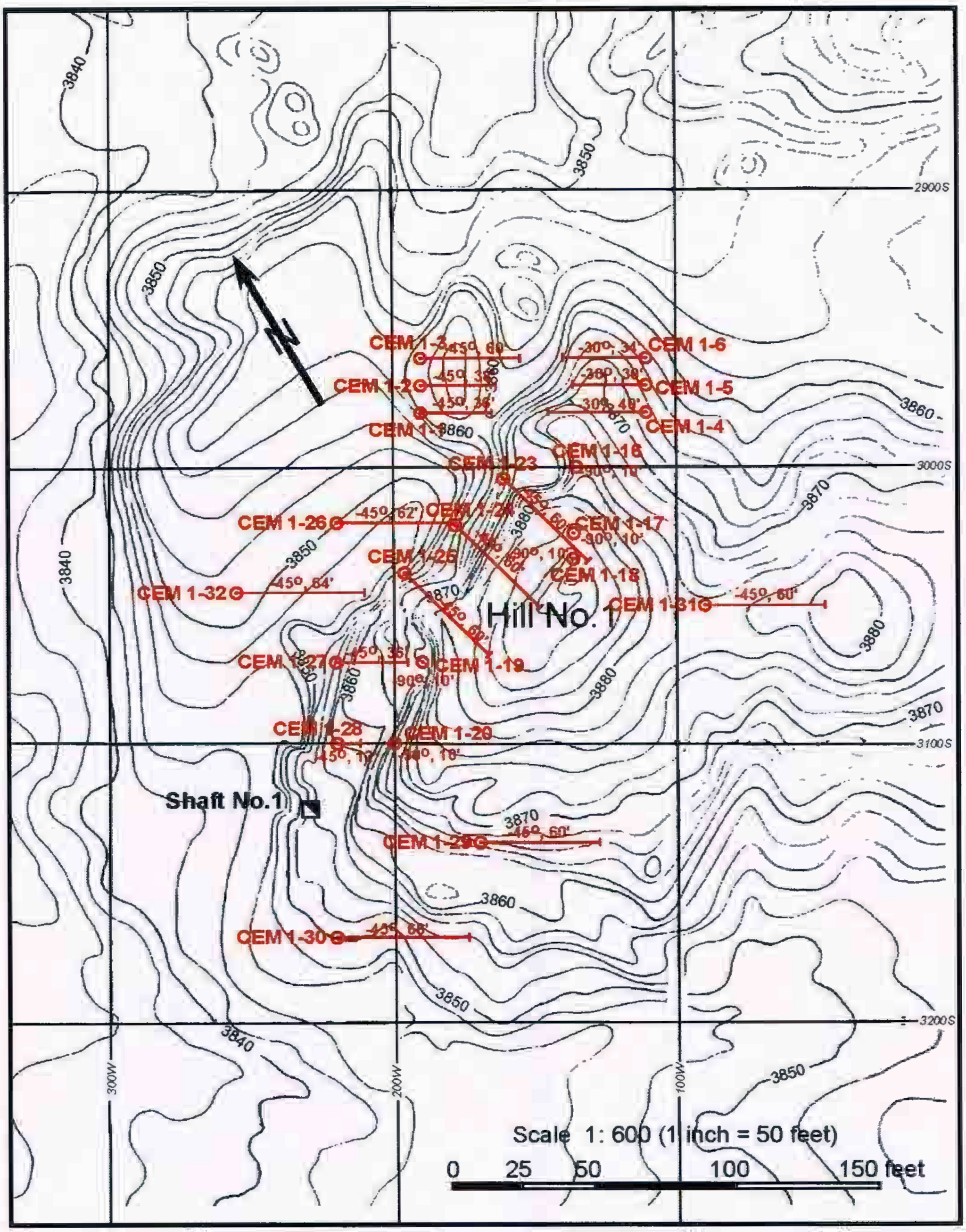


Figure 10. 1981-1982 Cascade Energy & Metals drilling at Hill No. 1 on the Telegraph South patented claim (modified after Lange, 1988, Plate 5).

Hill No. 1 (Shaft No. 1) Area

Figure 10 shows the locations and surface traces of the 21 holes that were drilled at the Hill No. 1 area on the Telegraph South patented claim. Table 7 contains a summary of the drilling at the Hill No. 1 area, and Appendix C contains detailed data from the drilling, including each hole's collar location, azimuth, incline and length, coded geologic logging (where available) and analytical data for each sample.

Nine holes, CEM 1-1 through CEM 1-6 and CEM 1-23 through CEM 1-25, drilled along the course of the Telegraph vein between 2960S and 3038S, each intercepted the Telegraph vein with excellent assay results. CEM 1-1, CEM 1-2 & CEM 1-3 were spaced 10 feet apart and all drilled on an azimuth of 118$^0$ and an incline of -45$^0$; CEM 1-4, CEM 1-5 & CEM 1-6 were collared 80 feet to the "west" (on the Telegraph grid) of CEM 1-1, CEM 1-2 & CEM 1-3 and drilled back at an azimuth of 298$^0$ and an incline of -30$^0$ (Figure 10). Intercepts of the -45$^0$ holes should be essentially true width of the vein/mineralized zones (which dips approximately 45$^0$ towards these drill holes) while the intercepts of the -30$^0$ holes would be far from true widths.

CEM 1-3 and CEM 1-6 were the northernmost pair of holes (Figure 10) and also have the highest analyses (Table 6; Appendix C). CEM 1-3 (the 118$^0$ azimuth and -45$^0$ incline hole) averaged 3.09 g/T Au over its entire 60-foot length and had a 20-foot intercept of 4.97 g/T Au from 32' to 52'; the hole is open at the bottom with the last three 2-foot samples returning analyses of 2.057, 2.057 and 1.714 g/T Au. CEM 1-6 (the 298$^0$ azimuth and -30$^0$ incline "pair" of CEM 1-3) would have sampled the vein well above CEM 1-3. CEM 1-6 averaged 6.07 g/T Au over its 34-foot length and bottomed in a 16-foot (18'-34') intercept (not true width) of 11.49 g/T Au. The hole is open at the bottom with the last three 2-foot samples in the vein with analyses of 14.74, 36.69 and 27.09 g/T Au; hence CEM 1-6 sampled the foot wall and the vein but did not pass through the vein into the hanging wall. (See Figure 10, Table 7 and Appendix C.)

The next pair to the south were CEM 1-2 (the 118$^0$ azimuth and -45$^0$ incline hole) and CEM 1-5 (the 298$^0$ azimuth and -30$^0$ incline hole). CEM 1-2 was only 38 feet long (vs. 60 feet for CEM 1-3 to the north) and averaged only 1.41 g/T Au. No geologic logs were discovered for CEM 1-2, but from the comparison of the analyses to those of CEM 1-3 (Appendix C), parallel and collared 10 feet to the north at the same elevation (Figure 10), it appears that CEM 1-2 may have drilled through the hanging wall and bottomed in the vein with a bottom 2-foot sample of 5.14 g/T Au. CEM 1-5 was a 30-foot hole and averaged 2.54 g/T over its length. Again we have no geologic log for CEM 1-5, but from the comparison of the analyses, the hole appears to be similar to CEM 1-6 with spotty relatively high-grade analyses (to 16.11 and 5.49 g/T Au) throughout the hole and a relatively high analysis of 5.49 g/T Au in the last sample. Presumably this 298$^0$ azimuth and -30$^0$ incline hole also tested the foot wall and bottomed in the vein. (See Figure 10, Table 7 and Appendix C.)

The southernmost of the three pairs to the south were CEM 1-1 (the $118^0$ azimuth and $-45^0$ incline hole) and CEM 1-4 (the $298^0$ azimuth and $-30^0$ incline hole). CEM 1-1 averaged 1.33 g/T Au over it 36-foot length and bottomed with three of its last five two-foot samples containing between 3 and 3.5 g/T Au. Again no geologic logs are available, but it appears that this $-45^0$ incline hole tested the hanging wall and bottomed in the vein. CEM 1-4 averaged 1.78 g/T Au and showed spotty mineralization towards the top of the hole and higher levels of mineralization towards the lower part of the hole. As the hole bottomed with a 2-foot sample of 11.66 g/T Au, it appears that this hole also sampled the footwall and was terminated (lost?) when it hit the Telegraph vein. (See Figure 10, Table 7 and Appendix C.)

CEM 1-23, CEM 1-24 & CEM 1-25 were three 60-foot holes spaced 20 feet apart and drilled at an azimuth of $163^0$ ("SE" on the Telegraph grid which is oriented at $28^0$ east of due north; see Figure 10) and an incline of $-45^0$. CEM 1-23 averaged 1.53 g/T Au over its 60-foot length, but the bottom half (30'-60') of the hole averaged 2.65 g/T (Table 7; Appendix C). No geologic logs were found for CEM 1-23. CEM 1-24 averaged 2.72 g/T Au over its 60-foot length with the intercept from 30' to 56' averaging 6.06 g/T Au. Lange's (1988) logs indicate the CEM 1-24 encountered the breccia vein from 30 feet to 42 feet; hence the higher grade zone is in the vein and footwall below. CEM 1-25 averaged 1.94 g/T Au over its 60-foot length; from 20' to 60' the hole averaged 2.71 g/T. Lange's (1988) log of CEM 1-25 indicated the hole encountered the breccia vein at 20 feet, so again the more mineralized material is in the vein and foot wall below. The last 2-foot sample in CEM 1-25 contained 1.71 g/T Au. (See Figure 10, Table 7 and Appendix C.)

Five ten-foot vertical holes were apparently attempts to collar on the outcropping vein in the Hill No. 1 area. CEM 1-16, CEM 1-17, CEM 1-18, CEM 1-19 and CEM 1-20 returned average analyses of 18.00, 16.63, 0.34, 3.60 and 0.51 g/T Au. Clearly CEM 1-16 and CEM 1-17 "hit" the $\sim 45^0$-dipping vein squarely. CEM 1-18 appears to have either missed the vein or hit an unmineralized zone in it. CEM 1-19 with analyses of 1.03 g/T from 0' to 5' and 6.17 g/T Au from 5' to 10' may have been collared in rubble or overburden, but apparently did hit the vein. CEM 1-20 appears to have missed the vein or hit an unmineralized zone in it. (See Figure 10, Table 7 and Appendix C.)

Four holes to the west of Hill No. 1, CEM 1-26, CEM 1-32, CEM 1-27 and CEM 1-28, were all $118^0$ azimuth and $-45^0$ incline holes with lengths of 12 to 62 feet. CEM 1-26 and CEM 1-32 showed only spotty weak mineralization. CEM 1-27 showed nil mineralization at the top of the hole, but the last 8 feet (28'-36') averaged 1.71 g/T Au. CEM 1-28 was only 12 feet long but was weakly mineralized and averaged 0.86 g/T Au over the 12 feet. (See Figure 10, Table 7 and Appendix C.)

To the east of Hill No. 1 CEM 1-31 was a 60-foot hole drilled at a $118^0$ azimuth and $-45^0$ incline. The hole averaged 1.16 g/T Au over its 60-foot length. The hole was mostly very weakly mineralized but had 2-foot samples of 19.54 g/T Au (32'-34') and 7.54 g/T Au (56'-58'), suggesting it crossed a couple of well mineralized stringers. (See Figure 10, Table 7 and Appendix C.)

To the south of Hill No. 1 CEM 1-29 was very weakly mineralized and averaged 0.31 g/T Au over its 60-foot length. CEM 1-30 showed spotty weak mineralization at the top and bottom of the hole but had a 10-foot intercept averaging 5.28 g/T from 8 feet to 18 feet. The 66-foot hole averaged 1.37 g/T Au over the first 60 feet; apparently the last 6 feet were not analyzed. (See Figure 10, Table 7 and Appendix C.)

The topography south of Hill No. 1 suggests another possible left-lateral off-set here on the south side of the hill. Again the drilling at Hill No. 1 suggests that there may be a significant volume of rock containing +0.5 g/T and/or +1.0 g/T Au is this area surrounding and away from the main Telegraph vein. Additional drilling will be needed in this area to determine if a significant structure is present and to better assess the volume of mineralized material here.

***Northern Extension (northern Telegraph Extension claim) Area***

Figure 11 shows the locations and surface traces of the 12 holes that were drilled at the Northern Extension area on the Telegraph Extension patented claim. Table 8 contains a summary of the drilling at the Northern Extension area, and Appendix D contains detailed data from the drilling, including each hole's collar location, azimuth, incline and length, coded geologic logging (where available) and analytical data for each sample.

The Northern Extension area is at the northern end of the Telegraph Extension claim; Shaft No. 3, near the south end of the claim (Figure 1) is at approximately 1100S and 100W on the Telegraph mine grid. The Northern Extension area (Figure 11) stretches from 500S to 300N on the grid or from 600 feet north of Shaft No. 3 to 1400 feet north of the shaft.

The 1981-1982 drilling in the Northern Extension area was essentially exploration drilling to test the main Telegraph vein in this area. This drilling was mostly done early in the 1981-1982 drill program, and it should be noted that most of the sampling of these holes in the Northern Extension area was done with 6-foot sample intervals (vs. 2-foot intervals later in the program). Hence these samples may in some cases be diluted as the vein in this area tends to be only 4 to 6 feet wide in outcrop. Most of these early holes were not logged by a geologist, and the hole location notes, possibly by a driller, required some interpretation; hence some of the Northern Extension holes may be somewhat mis-located (although the locations on Figure 11 and in Table 8 and Appendix D mostly correlate well with Cascade Energy and Metals maps from 1981-1982).

Table 8 summarizes the results of this drilling.

The N28$^0$E-striking Telegraph vein appears to turn to the west at about 100N on the Telegraph grid to become NNW-striking. CEM N-10 is the northernmost hole yet drilled in the area. A 60-foot hole at an azimuth of 68$^0$ and a -45$^0$ incline, the hole hit 12 feet (2 samples) of weak mineralization (1.166 g/T Au) at 36 feet. (See Figure 11, Table 8, and Appendix D.)

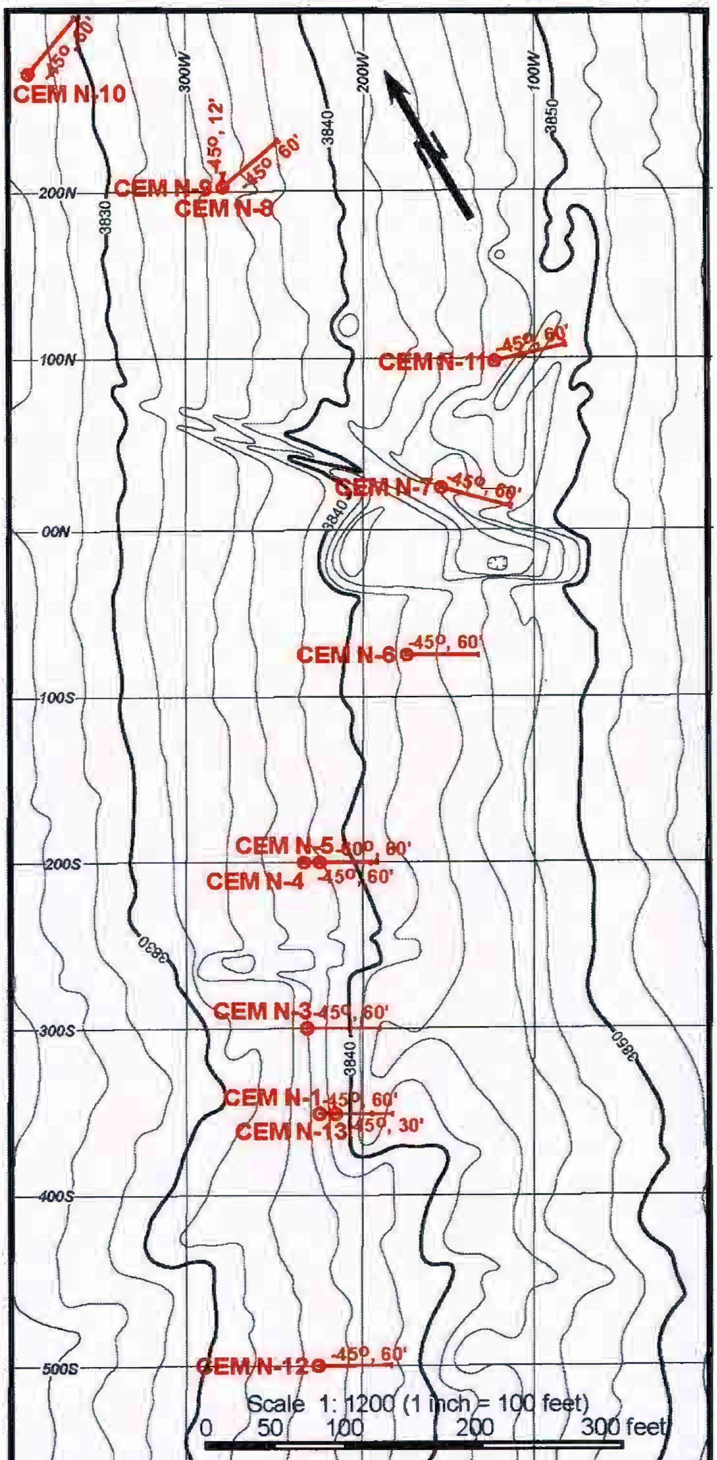

Figure 11. 1981-1982 Cascade Energy & Metals drilling in the "northern extension" area on the Telegraph Extension patented claim (modified after Lange, 1988, Plate 5).

CEM N-9 was a short (12 foot) drill hole directed to test the distance to the Telegraph vein from the collar location of CEM N-8. CEM N-9 with an azimuth of 31$^0$ and a -45$^0$ incline hit the vein at 12 feet. CEM N-8 was a 60-foot hole from the same location was drilled at an azimuth of 78$^0$ and an incline of -45$^0$; the hole intercepted 36 feet of 1.10 g/T Au from 24 to 60 feet and bottomed with a 6-foot sample of 1.15 g/T Au. (See Figure 11, Table 8, and Appendix D.)

CEM N-11 was a 60-foot hole at an azimuth of 105$^0$ and a -45$^0$ incline collared at a point near where the vein appears to turn to the west on surface. The hole returned one 6-foot sample of 0.55 g/T Au at 36 feet. (See Figure 11, Table 8, and Appendix D.)

CEM N-7 was a 60-foot hole at an azimuth of 133$^0$ and a -45$^0$ incline. The hole had one 6-foot intercept of 1.30 g/T Au at 30 feet. (See Figure 11, Table 8, and Appendix D.)

CEM N-6 was a 60-foot hole at an azimuth of 118$^0$ (due "east" on the Telegraph mine grid) and a -45$^0$ incline. The hole had two consecutive weakly mineralized 6-foot samples of 0.41 and 0.69 g/T Au between 36 and 48 feet. (See Figure 11, Table 8, and Appendix D.)

CEM N-4 was a 60-foot hole at an azimuth of 118$^0$ and a -45$^0$ incline. The hole had spotty weak mineralization with three consecutive 6-foot samples of 0.51, 0.86 and 1.54 g/T Au between 36 and 54 feet. Another zone of weak mineralization was encountered at the bottom of the hole where it is open with the last 6-foot sample from 54' to 60' of 1.23 g/T Au. (See Figure 11, Table 8, and Appendix D.)

CEM N-3 is the first hole (from north to south) for which we have a coded geologic log from Lange (1988). It was a 60-foot hole at an azimuth of $118^0$ and a $-45^0$ incline. Lange logs the hole as hanging wall from 12 to 24 feet; as breccia from 24 to 30 feet; and as foot wall from 36 to 48 feet. The 6-foot intercept of "breccia" from 24 to 30 feet returned an assay of 2.23 g/T Au. (See Figure 11, Table 8, and Appendix D.)

CEM N-1 was a 60-foot hole at an azimuth of $118^0$ and a $-45^0$ incline. The hole was weakly to well mineralized throughout, and the upper portion (12' to 36') was logged by Lange (1988). The hole was sampled with 2-foot samples from 12' to 28'; one 4-foot sample from 32' to 36'; and 2-foot samples from 52' to 60'. All taken together, these samples averaged 2.29 g/T Au. Lange (1988) logged breccia and vein from 14 feet to 28 feet with one sample of vein at 22' to 24' returning an analysis of 10.08 g/T Au. The hole is open at the bottom with a bottom sample of 1.37 g/T Au. (See Figure 11, Table 8, and Appendix D.)

CEM N-13 was a 30-foot hole collared 9 feet "west" (on the grid) of CEM N-1 and drilled parallel, apparently designed to intersect the vein at a slightly higher elevation. The hole was mineralized through it length and averaged 1.83 g/T Au with 2-foot samples. The hole was apparently not logged. (See Figure 11, Table 8, and Appendix D.)

CEM N-12 is the southernmost hole drilled in the Northern Extension area. It was a 60-foot hole at an azimuth of $118^0$ and a $-45^0$ incline. 6-foot samples were collected from 12 to 66 feet and three of them (from 30 to 48 feet) were analyzed, averaging 1.53 g/T Au. The hole was apparently not logged. (See Figure 11, Table 8, and Appendix D.)

Lange hypothesizes that there has been a ±150-foot down-drop of the rock north of Shaft No. 3 at the south end of the Telegraph Extension claim. He bases this opinion on alteration and mineralization of the vein in outcrop and core from the area north of the shaft. Specifically he saw no evidence of Stage III or V mineralization in this area. (Lange, 2008, testimony in United States of America v. HMI Lenders, LLC, IBLA No. CACA 45975.)

If indeed this area is, as hypothesized by Lange (1988), 150 feet higher in vein elevation than the present erosional elevation found between the Shaft No. 3 and Shaft No. 1 to the south, higher grade mineralization may very well be present at relatively shallow depths in this area. Additional drilling will be required to test this hypothesis.

***Gold Dyke Area***

At least 13 percussion exploration holes totaling 712 feet were drilled in the Gold Dyke vein area on unpatented Telegraph Nos. 34 & 35 claims in the 1981-1982 program. Most of the relatively sparse data on these holes that have been provided to the author are records of CEMCorp Laboratory. These data are included herein in Appendix E.

Locations for the Gold Dyke drill holes in Appendix E are on the Gold Dyke grid; locations for several of the holes were not included. No logs for the holes have been found. Several of the holes apparently were not analyzed, and several there were analyses showed only spotty weak mineralization.

However, GD-1, apparently a 52-foot hole, returned promising results with several 2-foot samples containing greater than 3 g/T Au and an average of the 25 samples (22' to 24' apparently was not analyzed) of 1.77 g/T Au.

As this report focuses on the Telegraph vein mineralization on three patented Telegraph claims (the Telegraph, Telegraph south and Telegraph Extension claims) and the five adjacent unpatented Telegraph claims (Telegraph Nos. 4 through 8) no major effort was made to locate more Gold Dyke data. However, there is a good possibility that additional resources could be identified on the Gold Dyke claims (Telegraph Nos. 34 & 35) with additional drilling in the area.

**1982 BLM Drilling**

As part of the patenting process of the Telegraph Extension claim the U.S. Bureau of Land Management drilled a 125-foot vertical core hole in April of 1982 on the claim at approximately 195 South and 175 West on the Telegraph Mine grid.

Results of this drilling were never provided to Cascade Energy and Metals Corporation. However, the BLM withdrew their challenge of the patent of the Telegraph Extension claim after the drilling of this hole.

The results of this drilling could likely be obtained through a GRAMA (Government Records Access Management Act) request.

**2006 Rocanville Drilling**

In 2005 the Telegraph Mine property was being examined by Rocanville Corporation ("Rocanville"), a Texas corporation interested in becoming a partner in the project. Geologist David Ryzak was contracted by Rocanville to evaluate the property, and after reviewing the literature available on the mine, he issued a favorable report to Rocanville. In 2006 Rocanville had Ryzak study the property on site and take samples following which he located and supervised a deep drill hole at approximately 2240S and 640W on the Telegraph No. 5 claim (Figures 7 & 13).

The 2006 vertical drill hole was drilled with a reverse-circulation drill to a depth of 380 feet. From 376 to 378 feet the hole penetrated two feet of apparent vein material which returned an analysis of 11.10 ppm Au and 8.2 ppm Ag (0.323 opt Au & 0.239 opt Ag); from 378 to 380 feet the hole returned an analysis of 0.45 ppm Au and 2.9 ppm Ag (0.013 opt Au & 0.085 opt Ag). Rocanville terminated the hole at 380 feet after apparently having penetrated the Telegraph vein.

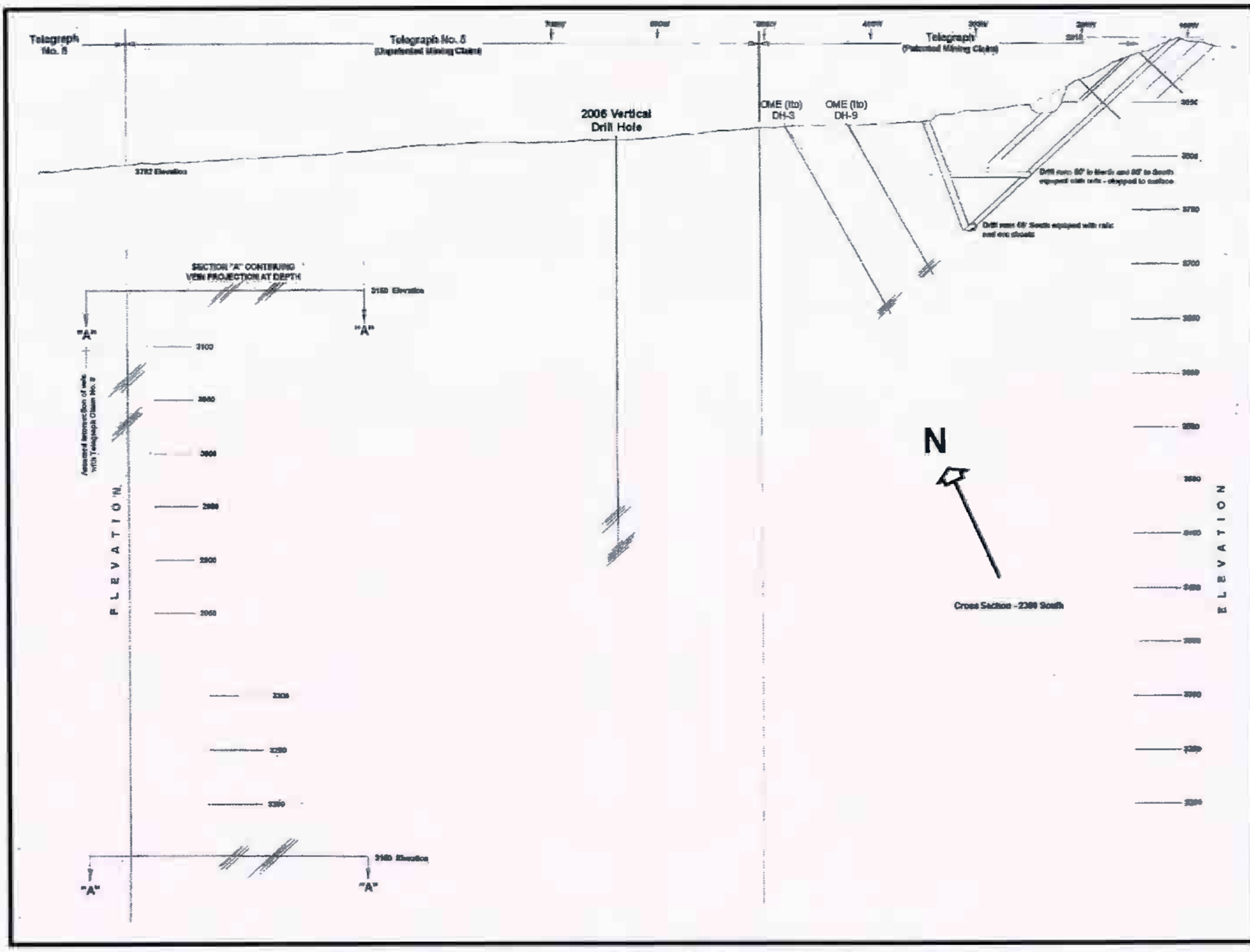


Figure 13. Cross-section of 2006 Rocanville Corportation drill hole on the Telegraph No. 5 claim (modified from HMI Lenders figure).

## 11. Sample Preparation, Analysis and Security

The author has no personal knowledge regarding the preparation and security of samples from the historic Telegraph Mine work. However, that work was performed or supervised by seasoned professional geologists and engineers, and presumably done to the level of professional standards at the time.

Analytical data (including assay certificates) from the historic sampling is largely available and shows that the analyses have done by reputable laboratories such as Assay Lab, Inc., West Jordan, UT (1981-1982); Kimball Laboratories, Draper, UT (1982); Rocky Mountain Geochemical

Corp., West Jordan, UT (1985 & 1986); ALS-Chemex Labs, Sparks, NV (2000); American Assay Laboratories, Sparks, NV (2006).

During the 1981-1982 drilling program and the production work in 1982 Cascade Energy & Metals operated their own in-house lab in Salt Lake City which they called CEMCorp Laboratory. Check samples were also submitted to other labs during this program.

Gold and silver analyses were generally by atomic absorption spectrometry with a then state-of-the-art PerkinElmer AA spectrometer in Cascade Energy and Minerals in-house laboratory, CEMCorp Laboratory, in Salt Lake City. This technique was deemed more accurate than other analytical techniques available in 1981 at the low levels gold and silver contents in most of the samples (Weston & Dickson, 1983). Gold content of samples ran from nil or a trace to over an ounce per ton, with many in 0.01, 0.02 and 0.03 opt range (see Appendices B, C & D). Analyses from the drilling were given in troy ounces of gold and silver per ton. Some samples were also analyzed at Kimball Laboratories and Assay Labs, Inc., both in Salt Lake City, with a similar range of results. Check samples were also routinely run at the other labs.

In 1983 CEMCorp Laboratory conducted a study comparing results of CEMCorp's AA spectrometry analyses against (1) neutron activation analyses by General Activation Analysis Inc. of San Diego, California, (2) ICP analyses by Ford Laboratories of Sandy, Utah, (3) two sets of research grade fire-assay analyses by Assay Lab Inc. of West Jordan, Utah, and (4) research grade fire-assay analyses by Union Assay Office Inc. of Salt Lake City, Utah, and (5) Kimball Laboratories and Consulting of Draper, Utah. The general conclusion of the study was that the AA spectroscopy results were more accurate at low gold concentrations while fire assay was better at higher gold contents (say, over 0.5 opt Au). Generally the CEMCorp results compared well to the other laboratories. (Weston and Dickson, 1983).

The level of precision of the low-level gold analyses done by CEMCorp Laboratory – generally "trace", "0.01" or "0.02" opt Au (= 0.00, 0.34 or 0.68 g/T Au, respectively) – was such that the precision of the lower-level analyses must be considered in any evaluation of this data (*i.e.*, the detection limit of this 1981 work was 0.01 opt Au = 340 ppb Au; common 2013 analyses have a detection limit of 5 ppb Au and a precision of as low as 1 ppb Au, and analytical techniques and even lower detection limits are available today. A 1981 sample with an analysis of 0.01 opt Au or 0.34 g/T Au from the CEMCorp work could actually have contained anything from 0.17 to 0.51 g/T Au.)

Of special note, splits of all historic samples collected by Cascade and other operators since 1974 are in the possession of Mojave Gold Mining Corporation and are available for future check analyses.

## 12. Data Verification

The author has made no attempt to verify much of the historic data on which this report is based beyond his site visit on May, 18, 2013.

However, as part of the court proceedings involving the validity challenge over some of the unpatented claims at the Telegraph Mine (U.S. District Court for Utah, Case No. 2:11-cv-00504-DB) almost all of the historic data on which this report has been based has been submitted as evidence, and many of the professionals who gathered the technical data have testified under oath as to the data's validity.

The author accepts this as *prima facie* evidence of validity and truthfulness of the data.

Moreover, the Telegraph Mine property has been sampled repeatedly across several decades of time and by numerous professional experts, and the results of that sampling and other examinations have consistently led to similar tenor estimates and conclusions.

In section **26. Recommendations** the author recommends a modest sampling effort and a limited amount of core drilling of to satisfy any concerns with the existing resource estimates prior to development of the project. However, the author strongly suspects that such sampling and drilling will only confirm the historic estimates of tenor and tonnage.

## 13. Mineral Processing and Metallurgical Testing

No metallurgical testing has been done as part of this study.

In September of 1976 a carbon leach column-absorption test was performed on mineralized rock from the Telegraph Mine by the U.S. Bureau of Mines in Salt Lake City. The test indicated that the Telegraph material would need to be ground to about 100 mesh to achieve acceptable recovery (Salisbury, 1976: see Appendix G).

Prior to the 1982 production of the 24,000 tons of ore from the open-pit operation at the Shaft No. 2 area, samples of the material to be mined were submitted to Dawson Laboratories of Salt Lake City for metallurgical testing.

An April 16, 1981, letter-report on results of cyanidation testing on a 20 lb. split of Telegraph mine ore crushed to -3/8" by Dawson Metallurgical Laboratories of Salt Lake City indicated 78% recovery of gold and nil recovery of silver; a 1 kg sample ground to -100 mesh gave recoveries of 96.2% gold and 51% silver. (Salisbury, 1981: Dawson Project No. P-604, Appendix G.)

In a June 23, 1981, letter-report Dawson Laboratories reports an approximate grind work index of 15 kw-hr/short ton for Telegraph Mine ore to produce a grind of 80% passing 100 microns (approximately 150 mesh) in a wet closed circuit using an 8-foot diameter ball mill. (Dawson, 1981a: Dawson Project No. P-650, Appendix G.)

A July 14, 1981, letter-report from Dawson on a Preliminary Batch Bulk Sulfide Floatation Test produced an 84.2% recovery of gold and a 65.0 percent recovery of silver. However, appreciable gold values (0.038 oz. Au/ton) remained in the tailings. (Dawson, 1981b: Dawson Project No. P-658, Appendix G.)

A 300-pound sample of low-grade (0.04 opt Au) Telegraph mine ore was submitted to the U.S. Bureau of Mines in October of 1982. The Bureau of Mines conducted agitation-cyanidation experiments and a series of column percolation leaching experiments to determine the ore's amenability to heap leaching. The agitation-cyanidation experiments indicated that the gold was recoverable by direct cyanidation and that fine grinding did not improve gold recovery which was between 88.9% and 90.9% (it did improve silver recovery from 33% to over 90%). The column percolation leaching experiments indicated the gold was recoverable by then-current heap leaching technology. The small column percolation experiments suggested that agglomeration did not improve percolation rates; however, the Bureau of Mines suggested that agglomeration might well be required in large-scale production heaps. The Bureau of Mines recommended that additional metallurgical testing be conducted to answer questions regarding agglomeration requirements and better quantify recoveries, reagent requirements and leaching periods. (McClelland, 1982: see Appendix G.)

In the 1982 mining operation the ore was mined, run through a Joy crusher and roll crusher and crushed to -¼"; then loaded into cement trucks where each load was sampled (see Appendix H), and agglomerated with water, Portland cement flue dust, cyanide and hydrogen peroxide while being transported to the leach pad. The agglomerated ore was then dumped onto the leach pad where it was sprinkled with a cyanide-water mixture. The pregnant solution was drained to a pregnant pond; pumped to a Merrill Crowe system for recovery through de-aeration, a zinc feeder where the gold dropped onto filters with diatomaceous earth. The filters were backwashed into a tub and the concentrate sent to an in-house refinery in Salt Lake City. (personal communication, 2013, W. David Weston.)

The author's visual inspection of the Telegraph vein at several locations on the property showed it to be very low in sulfide content with no chalcopyrite or copper oxides or copper carbonates identified. This would suggest that heap or vat leaching with NaCN would probably be the logical and most efficient gold extraction technique.

## 14. Mineral Resource Estimates.

No mineral resource estimates were made as part of this study.

Historic mineral resource estimates (at the time usually called "reserve estimates") were made in 1969 by geologist Tomo Ito and again in 1980 by geologist Joseph Owens. In 1981 geologist Meade LeRoy Jensen reviewed the findings of Ito and Owens and affirmed their estimates; later that year, after a water well on the property intercepted the down-dip extension of the Telegraph vein, Jensen made his own resource estimate. In 1982 mining engineer C.M. Daly assessed results of the 1981-1982 drill program and made a resource estimate of resources amenable to open-pit mining in the area of the Hill No. 2 (Shaft No. 2). In 2007 and 2008 HMI Lenders contracted geologist David Ryzak to compile a resource estimate and conduct an economic assessment of the Telegraph Mine as an expert witness in the legal dispute with the Department of the Interior involving the validity of the unpatented Telegraph Nos. 4 through 8, inclusive, and Telegraph Nos. 34 & 35 claims. In 2010 Mojave Gold compiled a resource estimate which has since been included in a 2012 Private Placement Memorandum.

**1969 Ito Resource Estimate**

Ito drilled 15 holes totaling 2079 feet including 549 feet of core and sampled accessible underground workings during the 1968-1969 program partially funded by the federal OME grant. Ito estimated a resource (he referred to it as an "ore reserve") within the drilling zone at 72,000 tons averaging 0.51 tr. oz. of gold and 1.16 tr. oz. of silver per ton in two blocks. While Ito had substantial core recovery problems, particularly when within the vein, he had numerous outcrops to sample and good access to the underground working for additional sampling for his grade estimates. He felt that the results of the drilling indicated good vein structure to at least a depth of 200 feet along the dip from Shaft No 3 southward to Shaft No 1. (Ito, 1969.)

In the northern block, north of the Hill No. 2 (Shaft No. 2), the mineable vein was assumed to be 1100 feet long with an average width of 4 feet. To a depth of 150 feet down-vein (an actual depth of about 107 feet on the ~$45^0$-dipping vein) and assuming a 25% deduction for non-commercial or displaced material and a density of the material of 12 $ft^3$/ton, he calculated a resource of 41,000 tons. In the southern block, between Hill No. 1 (Shaft No. 1) and Hill No. 2 (Shaft No. 2), the mineable vein was assumed to be 900 feet long with a similar average width of 4 feet. To a depth of 150 feet down-vein (again, an actual depth of about 107 feet on the ~$45^0$-dipping vein) and assuming a deduction of 10% for mined-out material and 20% for non-commercial or displaced material and a similar 12 $ft^3$/ton density, he calculated a resource of 31,000 tons. (Ito, 1969.)

Ito's reserve estimates were approved by Mr. Hall Stager, a geologist employed by the federal Office of Mineral Exploration which issued a Certificate of Possible Production. The USGS issued a Certificate certifying to a measured 72,000 ton ore body having an average grade of .50 opt Au. (Stager, 1969.)

At average grades of 0.51 opt Au and 1.16 opt Ag, Ito's 72,000 tons of resources contain 36,720 ounces of gold and 83,520 ounces of silver. It is worth noting that Ito's 72,000 tons of resources were only to a depth of slightly over 100 feet.

It is the author's opinion Ito's work was done to industry standards as of 1969 and that his resource estimate is valid. Today it might be considered a "geologically inferred resource estimate" based on limited surface and underground sampling and drill results (largely because he had significant core recovery problems). However, all of this work was done prior to implementation of N.I. 43-101, and per N.I. 43-101 Ito's work was contracted by the McGilvrays, then owners of the Telegraph property. Under the standards of N.I. 43-101 Ito's resource estimate would be considered a "historic resource estimate" and prospective investors would be advised that the work should not be relied upon.

**1980 Owens Resource Estimates**

In 1979 and again in 1980 the mine was evaluated by geologist Joseph Owens, who had been retained by Gold Technics, a California firm that was a joint-venture partner in the Telegraph Mine property, to confirm the findings of Ito and assess the mineralized resource.

Owens examined the deposit and took numerous surface and underground channel samples to verify Ito's findings. He calculated an average grade of 0.425 tr. oz. of gold and 1.31 tr. oz. of silver per ton (vs. Ito's estimated average of 0.51 tr. oz. of gold and 1.16 tr. oz. of silver). He found silver content to be more erratic than gold but determined the ratio of gold to silver was generally 1:3. (Owens, 1980.)

Owens noted that he believed that Ito's tonnage estimates were "extremely conservative." He calculated "Tonnage Estimates – Inferred Ore" of 540,000 tons within the area of the 1968-1969 drilling (mostly between Shafts No 1 and No. 3) by extending the ore zone to a depth of 450 feet. Using assumed grades of 0.50 opt gold and 1.16 opt silver Owens estimated the 540,000 ton resource would contain 270,000 ounces of gold and 626,400 ounces of silver. Using an overall strike length of 9,000 feet, extending to the north and south of the three patented claims, and an average vein width of 4 feet, he projected a target resource of 1,350,000 tons to a depth of 450 feet. With a dilution factor of 25% his geologically inferred resource was 1,012,500 tons. (Owens, 1980.)

His target projection was based on previous stope sampling and observed intensity of alteration in lower workings and recognition of vein structures to the north and south of the existing workings. (Owens, 1980.)

Owens' work was done prior to implementation of N.I. 43-101, and was partially dependent on the historic work of Ito done in 1968 and 1969 (Ito, 1968; Ito, 1969). Owen's work was contracted by the Gold Techniques, then investors of the Telegraph property. Under the standards of N.I. 43-101 Owen's resource estimate would be considered a "historic resource estimate" and prospective investors would be advised that the work should not be relied upon.

The author feels that a significant percentage of his resource estimates would currently be considered to be "geologically inferred resources."

1981 Jensen Resource Estimate

In October of 1981 the Telegraph Mine Associates, a group of individuals and entities that had subleased a working interest in the project, hired Meade LeRoy Jensen, Ph.D., a noted university professor, consulting economic geologist and co-author of the college text *Economic Mineral Deposits* (John Wiley & Sons, 1981, IBSN 10: 0471090433) to evaluate the work of Ito and Owens. He affirmed acceptance of the resource estimates of both Ito and Owens (Jensen, 1981.) In testimony in court Jensen testified that he felt that Ito's resource estimate of 72,000 tons to be "proven reserves" (Cascade v. Banks, Utah District Court C82-1223C).

In December of 1981 Cascade Energy and Metals drilled a vertical 528-foot well for water approximately 400 feet west of the Telegraph Mine Shaft No. 1 (Hill No. 1) on the Telegraph No. 4 unpatented claim and intercepted the projected mineralized shear zone at depths of 305 to 314 feet and 364 to 370 feet (Figure 8). Jensen then estimated the resource in the vein between Shafts No. 1 and No. 3 at 300,000 tons based on the drill hole results and persistence of the vein with depth (i.e., 450' deep x 4.0' wide x 2000' long /12 $ft^3$/ton = 300,000 tons). (Jensen, 1981.)

Jensen assumed an average grade of 0.354 tr. oz. of gold per ton for a total resource 106,200 troy ounces of gold in the 300,000 tons (Jensen, 1981).

Jensen's work was done prior to implementation of N.I. 43-101, and was partially dependent on the historic work of Ito done in 1968 and 1969 (Ito, 1968; Ito, 1969) and Owens in 1980 (Owens, 1980). Jensen's work was contracted by the Telegraph Associates, then lessors of the Telegraph property. Under the standards of N.I. 43-101 Owen's resource estimate would be considered a "historic resource estimate" and not to be relied upon by prospective investors.

The author must note that Meade LeRoy Jensen was an icon of economic geology. While his resource estimate may not "pass muster" per N.I. 43-101 standards, in his report he clearly supported the development of the Telegraph property (Jensen, 1981).

**1982 Daily Resource Estimate**

In 1982 Zions First National Bank of Salt Lake City, Utah, which was making a loan to Cascade Energy & Metals Corp. to purchase a crushing and screening plant, hired mining engineer C.M. Daily to examine the Telegraph Mine operation and submit a report of his findings to the Bank.

In late 1981 and 1982 Cascade Energy & Metals on contract to the Telegraph Associates drilled 1,984 feet in 55 percussion exploration holes on the main Telegraph vein on the three patented Telegraph claims. The drilling at Hill No. 1 (Shaft No. 1) and Hill No. 2 (Shaft No. 2) showed the footwall of the Telegraph vein to be fractured and highly silicified and mineralized, creating a mineralized zone much wider than previously anticipated.

Daily's report was dated May26, 1982, and he should have had access to the drill data from (listed from north to south, Figure 9) CEM 2-1, 2-2, 2-12, 2-3, 2-4, 2-5, 2-6, 2-7, 2-12a, 2-8, 2-13, 2-9, 2-10, 2-11, 2-14, 2-15, 2-16, and 2-17 (see Figure 9, Table 5 and Appendix B.)

Pursuant to that drilling Daily affirmed an estimated resource of 108,003 tons to the 30 feet depth down-dip, averaging 0.189 oz. of gold and 1.16 oz. of silver per ton, in the Hill No. 2 area, including both the vein and portions of the adjacent mineralized footwall (Daily, 1982).

During 1982 approximately 28,500 tons of ore was mined from the open pit developed at the Number 2 Shaft. The pit was confined to a small hill (Hill No. 2) with mining confined to the vein breccia and the fractured, silicified footwall. The waste to ore ratio was 4 to 1 (Daily, 1982). The pit had a mining width of approximately 58 feet and a height from the normal ground surface, extending to the crest of the hill, of approximately 45 ft.

Again Daily's work was done prior to implementation of N.I. 43-101, and was partially dependent on the historic work of Ito done in 1968 and 1969 (Ito, 1968; Ito, 1969), Owens in 1980 (Owens, 1980) and Jensen in 1981 (Jensen, 1981). Daily's work was contracted by Zions Bank, a third-party prospective loaner to the project, and per N.I. 43-101 Daily's resource estimate would be considered a "historic resource estimate" and not to be relied upon by prospective investors.

**2007 Ryzak Resource Estimates**

In 2006 geologist David Ryzak, a development and mine production geologist with 30 years' experience with several mines in the western U.S., examined the Telegraph Mine property on behalf of Rocanville Corporation, a Texas corporation interested in becoming a partner in the property. Ryzak also supervised the drilling of a 380-foot vertical drill hole 500 feet west-southwest of Shaft No. 2 on the Telegraph No. 8 unpatented claim (Figures 7 & 13).

In 2007 and 2008 HMI Lenders contracted Ryzak to compile a resource estimate and conduct an economic assessment of the Telegraph Mine as an expert witness in the legal dispute with the Department of the Interior involving the validity of the unpatented claims Telegraph Nos. 4 through 8, inclusive, and Telegraph Nos. 34 & 35. Mr. Ryzak's testimony was taken on January 9, 2008 (Ryzak, 2008). (U.S. District Court for Utah, Case No. 2:11-cv-00504-DB.)

Ryzak, in close consultation with Peter Lange, calculated an open-pit mineable resource along the vein with a strike length of 2,400 feet extending from the area of Hill no. 1 (Shaft No. 1) at the northern end of the patented Telegraph South claim across the patented Telegraph claim to the area of Hill No. 3 (Shaft No. 3) at the southern end of the patented Telegraph Extension claim to depth of 130 feet down-dip. He determined a resource of 89,700 ounces of gold in 345,000 tons of ore averaging 0.26 opt Au with a 4:1 strip ratio. Ryzak also calculated an underground mineable resource of 204,000 tons from the bottom of his proposed pit to the 500-foot depth in the vein with an average width of 4 feet and a strike length of 2400 feet. With an average grade of 0.48 opt Au, this resource to be mined underground would contain 97,920 ounces. Hence Ryzak identified a total estimated resource of 187,620 tr. oz. of gold in the Telegraph vein to the 500-foot depth (Ryzak, 2008).

Ryzak also did an economic assessment of the project, factoring in mining costs, milling costs, dilution, recovery, etc. This part of his study is discussed in section **22. Economic Analyses**, below.

Again Ryzak's resource estimates, while done after implementation of N.I. 43-101, was not done per N.I. 43-101 guidelines and would not be considered N.I. 43-101 compliant.

### 2010 Mojave Gold Resource Estimates

In 2010 Mojave Gold's directors produced a current resource estimate which is discussed in detail below and is in a 2012 Private Placement Memorandum by the company (Mojave Gold Mining Corporation, 2012). They categorized the resources as "Measured Mineral Reserve," "Probable Mineral Reserve," "Inferred Mineral Reserve," and "Potential Mineral Reserve." Mojave's classified resource estimate is listed in Table 1 in section **1. Summary**, above. For the convenience of the reader, Table 1 is repeated here:

**Table 1. Mojave Gold In-House Classified Mineral Resources**

| Mojave Gold Mineral Reserves Classification | Quantity (tons) | Gold Grade (g/T) | Gold Total (tr. oz.) | Silver Grade (g/T) | Silver Total (tr. oz.) |
|---|---|---|---|---|---|
| Measured | 510,440 | 7.20 | 107,192 | 12.24 | 182,227 |
| Probable | 525,728 | 7.20 | 110,403 | 12.24 | 187,685 |
| Inferred | 2,102,912 | 7.20 | 441,612 | 12.24 | 750,740 |
| Potential | 1,350,000 | 7.20 | 283,500 | 12.24 | 481,950 |

The "Measured Mineral Reserve" was determined based on the 1968-1969 drilling and surface and underground sampling by Ito (Ito, 1969), sampling results from the two deep holes (the 1981 water well and the 2006 drill hole) by Cascade and Rocanville, the 1981-1982 drilling at Hill No. 1 and Hill No. 2, and blast-hole sampling done during the mining in 1982, as well as geophysical surveying (EM-VLF), vein mapping, and epithermal boiling deposit evaluations (Lange, 1988) and the evaluation of David Ryzak (Ryzak, 2008). The mineralized zones include the vein/ore contours identified at Hill No. 1 & Hill No. 2, the Surprise Stope, the Discovery Shaft contour and the Shaft No. 3 contour to the 250-foot depth (~330 feet down-dip). These resources are estimated to contain 510,440 tons (680,587 tons less 25% for non-commercial/mined out) of material containing 107,192 ounces of gold and 182,227 ounces of silver (average grade 0.21 opt [7.20 g/T] Au and 0.36 opt [12.24 g/T] Ag).

The "Probable Mineral Reserve" includes these same zones to the 500-foot depth with the assumption that the vein zone between the 250-foot depth and the 500-foot depth will include 50% of the 2000-foot strike length from Hill No. 1 to Hill No. 3 for a mineralized resource of 525,728 tons.

The "Inferred Mineral Reserve" of 2,102,912 tons extends the "measured" and "probable" zones to a depth of 1500 feet. The epithermal boiling deposit model of Lange (1988) predicted that the gold mineralizing events of Stages III and IV would extend the average grade of mineralization to a depth of 1500 feet.

Lange's (1988) studies concluded that the top of the boiling zone at the Telegraph Mine was essentially at the surface from Hill No. 1 to Hill No. 3, but that is had been down-dropped by 150 feet north of Hill No. 3. The "Potential Mineral Reserve" includes the potential ore zone of the Telegraph vein within the Telegraph Extension claim north of Shaft No. 2 and traceable for another 1200 feet to the north between the 150-foot and 1500-foot elevations and totals another 1,350,000 tons.

Hence Mojave Gold's resource estimates include 510,440 tons of "Measured Mineral Reserve," 525,728 tons of "Probable Mineral Reserve," 2,102,912 tons on "Inferred Mineral Reserve," and 1,350,000 tons of "Potential Mineral Reserve" for a total of a little under 4.5 million tons.

These resource estimates, while done after implementation of N.I. 43-101, were in part dependent on the historic work of Ito (1968 &1969), Owens (1980) and Jensen (1981), as well as on the work by Ryzak (2008). This historic work was largely not done per N.I. 43-101 guidelines and as an in-house resource estimate would not be considered N.I. 43-101-compliant.

However, Mojave's work was done by persons qualified by professional degrees and experience. The work is based on sworn testimony elicited in the court proceedings before the U.S. Department of the Interior, IBLA 2012-233, presently pending before the United States District Court for Utah where it is known as HMI Lenders v. Ken Salazar, Civ. No. 2:11-cv-00504-DB. The in-house resource estimates have been authorized and approved by Mojave Gold's Directors (Appendix A).

## 15. Mineral Reserve Estimates

No mineral reserve estimate was made as part of this study, and no formal historic reserve estimates have been done.

Several of the historic resource estimates discussed in section **14. Mineral Resource Estimates**, above, were caller "reserve estimates" at the time they were made. However, only current resource estimate by Mojave Gold's Directors was accompanied by a pre-feasibility study (their 2010 *Pro Forma* analysis) as would be required for a resource estimate under current N.I. 43-101 guidelines and industry standards.

The *pro forma* analysis (pre-feasibility study) by Mojave Gold Mining Corporation is discussed in section **22. Economic Analyses**, below.


Figure 16. Underground view looking south-southwest along the main drift on the 3800-foot level of Shaft No. 2 (Hill No. 2) of the Telegraph Mine. The west dipping attitude of the main breccia-vein is evident and all stages of mineralization are exposed. Light tan Stage IV breccia (a) hosting white Stage V veins (b) occupy the zone's central exposure, with greenish-grey Stage III breccia developed along the footwall and hanging wall (c). Note large Stage III clasts included within Stage IV breccia (d). Managnese-oxide-rich Stage VI fissure veins occupy both re-opened shallow structures within the main zone (e) and high-angle structures in the hanging wall (f). (photo from Lange, 1988, Figure 28.)

# 16. Mining Methods

The author is a geologist, not a mining engineer, and is only marginally qualified to comment on mining methods proposed for the Telegraph Mine property.

Mojave Gold Mining Corporation's current proposed mining plan consists of two phases. The first phase will expand the open-pit mining of the zones mined in 1982 along an estimated 2400-foot strike length of the vein from the Hill No. 1 (Shaft No. 1) area to the Hill No. 3 (Shaft No. 3) area to a depth of 130 feet (40 meters) and the construction of a vat leaching facility. (Mojave Gold Mining Corporation, 2011.)

Simultaneously Mojave will embark on shaft sinking for phase two underground mining. The present Shaft No. 1 on Hill No. 1 on the Telegraph South claim will be enlarged to a 6x18-foot three-compartment shaft and extended to a depth of as much as 1500 feet (so far as ore is encountered). A drift will be driven from the bottom of the incline shaft to the north a distance of 1000 feet (300 meters) to create a bore-raised vertical production shaft, centrally located, to bring ore to the surface. Access drifts spaced at 200 feet (60 meters) vertically will be extended to the north from Shaft No. 1 starting at the 400-foot level. (Mojave Gold Mining Corporation, 2011.)

Mining would be by overhand cut-and-fill, shrinkage stoping and resuing depending on the geometry, geology and accessibility of the ore in the vein at a rate of 250 to 350 tons per day. Mining would proceed at two shifts per day, five days a week. (Mojave Gold Mining Corporation, 2011.)

Treatment of the underground ore would consist of crushing, grinding and high column floatation in conjunction with vat cyanide leaching. The modular plant would likely operate three shifts per day, seven days per week. (Mojave Gold Mining Corporation, 2011.)

The actual mining plan to be followed at the Telegraph Mine would be generated out of additional studies. Mojave Gold has management (Appendix A) and personnel well versed in underground mining techniques, and the author has no reason to suspect that they are not fully capable of devising a sound plan to exploit these mineral resources with minimal effects on surface resources in the area.

# 17. Recovery Methods.

Again, the author is a geologist and not a metallurgist and is only marginally qualified to comment on recovery methods proposed for the Telegraph Mine property.

The Telegraph project anticipates that after the ore is extracted from the ground it will require milling consisting of crushing, grinding, and separation including possibly column floatation followed by cyanide leaching. A 250-ton per day, modular milling plant with modular units erected over concrete slabs is envisioned. Ultimate recovery will be by vat cyanide leaching. (Mojave Gold Mining Corporation, 2011.)

However, Mojave also realizes that the location of the deposit within the Mojave National Preserve and in California may result in conventional milling and floatation being a more desirable recovery technique. Preliminary studies by Dawson Laboratories in the early 1980s (see Appendix G) indicate similar and acceptable recoveries for milling/floatation vs. vat cyanide leaching.

## 18. Project Infrastructure.

From a standpoint of logistics, the Telegraph Mine project should be relatively straight-forward and easy. The project is immediately adjacent to an Interstate highway with clear right-of-way to and from the mine site. The terrain at the mine site is relatively flat.

Sufficient water for mining operations should be available on the property from an existing well and mine water.

Power should be available from California Power which has an existing power line on the north side of Interstate 15. Contractual arrangements will need to be made with California Power and a transmission line will need to be permitted to get the electricity across (under?) the freeway.

Existing roads will need to be upgraded, and a basic mine infrastructure constructed.

If the mine's location within the Mojave National Preserve significantly complicates construction and operation of mill and tailings facilities on site, Mojave Gold plans to locate these facilities on the north side of Interstate 15, probably near the Halloran Summit interchange, on BLM lands outside of the preserve. This would entail just a three-mile haul of the ore from the mine to this potential mill location.

## 19. Market Studies and Contracts.

No market studies have been conducted as part of this study.

## 20. Environmental Studies, Permitting and Social or Community Impact.

A formal assessment of permitting requirements has not been done for the Telegraph mine project, but permitting requirements will likely require a waste discharge permit, an Environmental

Impact Report (EIR), and mandatory backfill of mine waste into the excavation at reclamation, as well as a California Land Use Permit.

Mojave Gold anticipates an 18- to 24-month period for all approvals following submission of a final mine plan and all permit applications.

## 21. Capital and Operating Costs

While capital and operating cost are beyond the parameters of this report, Mojave Gold Mining Corporation completed in 2011 an in-house capital and operating cost study: Mining Method and Cost study for the Telegraph Mine (Mojave Gold Mining Corporation, 2010a & 2010b).

Mojave's anticipated total capital costs (including permitting, bonding, power infrastructure, site clean-up and preparation, surface and underground mining capital costs, metallurgical plant purchase/installation, mining equipment, contingency and working capital) of $5,407,000. Surface mining cost per ton (Hill No. 1 & Hill No. 2) is estimated at $12.66; open-pit mining (to a 105-foot depth) cost per ton at $34.38; underground mining cost per ton at $75.76; and processing costs (for a 250-ton per day plant) per ton at $42.32.

## 22. Economic Analyses

No economic analysis has been done as part of this report. However, economic analyses were compiled by David J. Ryzak in 2007 and by Mojave Gold Mining Corporation in 2011.

### 2007 Ryzak Economic Analysis

In 2007 and 2008 HMI Lenders contracted Ryzak to compile a resource estimate and conduct an economic assessment of the Telegraph Mine as an expert witness in the legal dispute with the Department of the Interior involving the validity of the unpatented claims Telegraph Nos. 4 through 8, inclusive, and Telegraph Nos. 34 & 35. Mr. Ryzak's testimony was taken on January 9, 2008 (Ryzak, 2008).

Ryzak determined the costs for the open pit mine based on a 4:1 strip between Hill No. 1 on the South Telegraph claim to Hill No. 3 on the Telegraph Extension claim. He then also determined the costs for the underground mine, just below the open pit mine to a vertical depth in mining of 500 feet. Ryzak calculated an open-pit mineable resource along the vein with a strike length of 2,400 feet extending from the northern end of the Telegraph South claim across the telegraph claim to the southern end of the Telegraph Extension claim to depth of 130 feet down-dip. He determined a resource of 89,700 ounces of gold in 345,000 tons of ore averaging 0.26 opt Au across a width of with a 4:1 strip ratio. Ryzak also calculated an underground mineable resource of 81,600 ounces of ore the vein averaging 0.48 opt Au gold with an average width of 4½ feet from the lowest portion of his hypothetical open pit to the 500-foot vertical depth. (Ryzak, 2008.)

For the surface mine Ryzak determined the capital costs to be $1,509,000. He calculated the open pit mining costs of $33.97 and processing costs of $19.33 per ton for 2008. He determined total mining, processing, and capital costs for the 345,000 tons of ore to be $19,898,000. At a gold price of $860.00/tr. oz. and a recovery rate of 92% he projected gross income $70,971,000 for a gross profit before taxes of $51,073,000. (Ryzak, 2008.)

For the underground mine Ryzak opined the strike length would be 2400 feet which he reduced to 2000 feet to give weight for 20% dilution. He projected underground mining to extend an additional 320 feet down dip with an average vein width of four and a half feet which will develop about 200,000 tons of ore, factoring in 20% dilution. Ryzak cut the average grade of 0.48 opt Au to 0.40 opt Au ounce per ton to take into account dilution. He then determined the mining costs to be $73.87 per ton with processing costs the same for the open pit at $19.33 per ton. Total mining and processing costs would be $93.20 per ton. Capital costs for the underground operation would be $1,406,000, and mining, processing and capital costs for the 200,000 tons would total $20,012,000. 200,000 tons of ore at a diluted grade of 0.4 ounces per ton and a recovery of 92 percent in the mill and a gold price of $860 per ounce, would produce a gross income of approximately $63,296,000. Deducting the capital, mining and processing costs of $20,012,000, the gross profit before taxes would be approximately $43,284,000 for the underground portion of the operation. (Ryzak, 2008.)

Adding the gross profit for the open pit mining and underground mining would provide a gross profit of $94 million without any consideration for silver (3% of total revenue). Ryzak (2008) testified he personally would be willing to go forward with the expenditure of labor and means to develop a mine on the Telegraph claims based upon his knowledge and expertise. (Ryzak, 2008.)

**2010 Mojave Gold Mining Corporation *Pro Forma* Analysis (Pre-Feasibility Study)**

Mojave Gold conducted an in-house *pro forma* financial analysis of the Telegraph Mine project in 2010 (Mojave Gold Mining Corporation, 2010b). This analysis is essentially a pre-feasibility study.

Mojave Gold anticipated mining the deposit in three operations: a "surface mining" operation to remove ore on Hill No. 1 and Hill No. 2; an "open-pit" operation to remove ore along Ryzak's 2400 strike length from Hill No. 1 to Hill No. 3 to a depth of 105 feet (roughly equivalent to Ryzak's 130 feet down-dip); and an "underground" operation to remove ore to the 250-foot vertical depth. In total this model would involve the 510,440 tons of their "Measured" ore (see section **14.**

**Mineral Resource Estimates**, above): 21,751 in the "surface mining" operation; 116,484 tons in the "open pit" operation; 372,206 tons in the "underground" operation. Additionally they would process 4,000 tons of unprocessed crushed ore left over from the 1981-1982 mining operation. Development of their "Probable," "Inferred," and "Potential" resources (see section **14. Mineral Resource Estimates**, above) was not considered in the calculations in their *pro forma* financial analysis.

They anticipated an average grade of 0.21 opt (7.20 g/T) Au and 0.36 opt Ag (12.34 g/T) in the "surface mining," "open pit," and "underground" ore and an average recovery rate of 92% for both metals. Cut-off grade would be 0.11 opt (3.77 g/T) Au.

Per Mojave Gold's analysis, total revenue at a price of $1,350 per ounce for gold and $20 per ounce for silver would be $137,435,772. Total capital investment required would be $5,024,637, and total operating costs for the ten-year mine life would be $59,329,326.

The net present value of the operation would be $48,427,617 and break-even price for gold would be $856/ounce.

The reader is referred to Mojave Gold's *pro forma* financial analysis (Mojave Gold Mining Corporation, 2010b) for details of this analysis.

## 23. Adjacent Properties

There are no adjacent properties known to the author that have had technical information on them released pursuant to N.I. 43-101.

Historic properties in the area of the Telegraph Mine include the Henry Mine on Shadow Mountain (12 miles north of the Telegraph Mine), the Huyten Mine (5 miles west-northwest of Halloran Springs and about 8 miles west and slightly north of the Telegraph Mine), and a few turquoise mines in the Halloran Hills. The Copper World Mine, 16 miles to the northeast of the Telegraph Mine on the southwest flank of the Clark Mountains, was the largest of several copper and base metal mines in the Clark Mountains. There were also several small gold and silver mines in the Clark Mountains.

The Henry Mine on Shadow Mountain was opened as early as 1895 (Tucker and Sampson, 1943) and had a principal exploration tunnel about 750 feet long. The Henry Mine explored a quartz vein striking N10$^{0}$W and dipping 50$^{0}$E that lay between granite gneiss below and syenite gneiss above. The vein was stoped as much as 100 feet upward from the tunnel and along it for 300 feet. As the vein is not stoped where it is less than 8 inches wide, much of it must have been wider. Production records from 1913 to 1919 show 35 tons of ore that contained about 2.90 ounces of gold to the ton and a little silver, copper, and lead. In the 1940s and 1950s the mine was an intermittent source of small shipments. (Hewett, 1956.)

At the Huyten Mine, five miles northwest of Halloran Springs and reportedly discovered prior to 1902, several shafts were sunk on a vein that outcrops conspicuously for several hundred feet. By 1930 there were a number of shallow shafts, the deepest being 125 feet. There was also a 20 ton per day mill. The vein trends N40$^{0}$E, dips 70$^{0}$SE, and ranges from 2 to 4 feet wide. It is largely layered quartz but contained also considerable limonite and some copper minerals. Probably gold is the most valuable constituent as it is reported that some of the ore was crushed and treated nearby. The enclosing rock is gray monzonite (now mapped as Teutonia adamellite). With revived interest in the district following the discovery of gold at the Telegraph Mine in 1930, the group of 15 claims was leased to American Hellenic Gold Mining Company of Las Vegas. (mostly from Hewett, 1956.)

The most productive copper mine in the Ivanpah 1-degree quadrangle is the Copper World Mine, located on the southeast slope of a westward spur from Clark Mountain, some 16 miles northeast of the Telegraph Mine. The Copper World Mine was one of the first ·mines of the region to be explored, and there is a record of shipments as early as 1869. However, little work was done at the property until 1898 when a smelter was erected at Valley Wells (located 5 miles southwest of the Copper World at a location now 2 miles north of Exit 272 on I-15). After a brief campaign of exploration which yielded copper worth about $750,000, it again lay idle until 1906. From 1906 to 1908, under the ownership of the Cocopah Copper Co., the Copper World was the source of 3,638 tons of ore containing about 7 percent copper. The mine's principal period of operation extended from 1916 to 1918 when about 1,735 tons of crude ore containing about 4 percent copper and 1,353 tons of matte containing 25-28 percent copper were shipped. The explorations include several thousand feet of tunnels and drifts and a shaft 100 feet deep, from the bottom of which there are several hundred feet of drifts. In 1943 3,743 tons of old slag from the Valley Wells smelter were processed, producing another 286,000 pounds of copper, 2,226 ounces of silver and 21 ounces of gold. Total production from the mine is estimated (by the author from references he has reviewed) at about 22,350,000 pounds of copper, 60,000 ounces of silver and 123 ounces of gold. (much of this information from Hewett, 1956.)

Turquoise was produced from the western and eastern slopes of Turquoise Mountain (about 8 and 6 miles northwest of the Telegraph Mine area) as well as from the Solomon's Knob area (about 3 miles north of the Telegraph Mine property) by aboriginals (Leonard & Drover, 1980). Later turquoise was produced commercially after the staking of claims in 1896 and 1898. The commercial operations apparently focused in the Turquoise Mountain area (mostly on the west side) and continued until 1904; total production is not known, but one major shipment to New York in 1900 was reportedly worth an estimated $28,000 (Vrebenburgh, 1996).

# 24. Other Relevant Data and Information

### Potential for a Large-Volume, Low-Grade Gold Deposit at the Telegraph Mine

The production and historic exploration at the Telegraph Mine property has always been directed towards production from the main Telegraph vein itself and, in 1982, the near-surface mineralized footwall. However, review of the results of the 1981-1982 drilling program at the Telegraph Mine and at the adjacent Gold Dyke property suggest there may be excellent potential for a substantially larger, albeit lower-grade deposit on the property.

The historic work and the 1981-1982 work were all done under substantially different economic conditions from those of today (December, 2013). The price of gold has increased dramatically since this work was done and gold recovery techniques from deposits like the Telegraph Mine have advanced appreciably. Results from the 1981-1982 percussion drilling program show numerous drill holes well away from the main Telegraph vein with 40-foot to 80-foot intercepts of about 1.0 g/T Au or greater. Additionally many of the holes into and through the vein itself bottomed with their last sample greater than 1.0 g/T and should be considered "open at depth." (See Tables 6, 7 & 8; Figures 9, 10 & 11; and Appendices B, C & D.)

The author believes that a very good possibility exists for the development of a surface-mineable resource of a ten or more million tons of material grading +1.0 g/T in the immediate area of the main Telegraph vein on the three patented claims. A substantial amount of surface drilling would be required to establish this potential resource, but the drilling could be phased to not involve a substantial commitment of funds until encouraging results were in hand.

### VLF-EM Geophysical Survey Results

As part of the Lange-Weston work in 1984-1986 and Lange's M.S. thesis at Colorado State University (Lange, 1988), a VLF-EM survey was conducted over the Telegraph mine property, presumably with a Geonics EM-16 unit. VLF-EM has been shown to be an effective and inexpensive means of identifying water-filled geologic structures that respond as weak electromagnetic conductors.

Lange (1988) contoured filtered VLF-EM dip data and field strength on a base map of the Telegraph Mine system (Lange, 1988; Table 2 & Plate 7). Contoured dip cross-over peaks form straight "ridges" appear to approximate the average N28$^0$E strike of the buried Telegraph vein. The correlation is excellent from the Hill No. 1 (Shaft No.1) area to the Hill No. 2 (Shaft No. 2) area where the "ridge" is off-set to south-southwest from location of the outcropping vein outcrop, presumably reflecting where the westward-dipping vein intersects the water table below surface (Lange, 1988, Plate 7). North of the Hill No. 2 (Shaft No. 2) area the "ridge" displays an offset between Hill No. 2 and Hill No. 3 (Shaft No. 3); this may be reflecting a post-mineral fault. North of Hill No. 3 the "ridge" appears to weaken somewhat and another, parallel ridge appears to the east, possible reflecting a post-mineral fault or a second vein.

In testimony in the claims validity case (U.S. Department of the Interior, IBLA 2012-233, presently pending before the United States District Court for Utah where it is known as HMI Lenders v. Ken Salazar, Civ. No. 2:11-cv-504-DB), Lange stated that he thought that the VLF-EM data had successfully traced the Telegraph vein for some 1070 meters (3500 feet).

More EM work and additional drilling will be needed to fully assess EM as a tool for better targeting drilling efforts at the Telegraph Mine. However, VLF-EM and probably other ground EM or airborne EM surveying appear to be a potentially very valuable tool for further exploration at the Telegraph Mine.

The reader is referred to Lange (1988) for a more detailed description of the work that was done as part of Lange's M.S. thesis.

**Accounting for 1981-1982 Gold Production from the Telegraph Mine**

During the period of production at the Telegraph Mine in 1981 and 1982 the ore was mined, run through a Joy crusher and roll crusher and crushed to -¼"; then loaded into cement trucks where each load was sampled, and agglomerated with water, Portland cement flue dust, cyanide and hydrogen peroxide while being transported to the leach pad; then dumped onto the leach pad where it was sprinkled with a cyanide-water mixture. The pregnant solution was drained to a pregnant pond; pumped to a Merrill Crowe system for recovery through de-aeration, a zinc feeder where the gold dropped onto filters with diatomaceous earth. The filters were backwashed into a tub and the concentrate sent to an in-house refinery in Salt Lake City.

However, operations were shut down early in 1982 after an estimated 24,600 tons or ore had been stacked on the heap. Mojave Gold reports that actual gold production from Cascade Energy and Metal's Salt Lake City refining laboratory totaled 91 ounces of gold and silver in the form of dore bars that was distributed to the Associates and 504.67 ounces of gold that was sold by the Associates to refineries (W. David Weston, personal communication, 2013).

In 1985 the pile was saturated with sodium hypochlorite to destroy the cyanide as part of the reclamation following the 1981-1982 mining.

According to the 1986 report of Charles H. Pitt, Professor of Metallurgy at the University of Utah, (Pitt, 1986), based his assessment of on truck loading data and chemical analyses (Appendix H), an estimated 24,646 tons of ore had been stacked on the pad containing an estimated 5888 ounces of gold. Pitt estimated 72% of the gold was recoverable through heap leaching, for 4239 ounces of recoverable gold, based on metallurgical studies by the U.S. Bureau of Mines (Salisbury, 1976) and Dawson Metallurgical Laboratories (Salisbury, 1981). Pitt accepted an estimate of 300 ounces already removed from the heap and concluded that the recoverable gold remaining would be 3939 ounces and that at an assumed flow rate of 270 tons of cyanide solution per day with a gold content of 13 ounces and under optimum leaching conditions, approximately 303 days would be required to extract the estimated remaining values. (Pitt, 1986.)

In 2011 Russell Sorenson, who had worked in the Cascade refining laboratory (part of the CEMCorp Laboratory) as technical director and performed all operations for the smelting and recovery of gold and silver metals produced from the Telegraph Mine, suffering from a terminal illness came to W. David Weston and confessed that during the course of his employment by Cascade and CEMCorp Laboratory, he had engaged in malfeasance and systematically under-reported the amount of gold and silver he had received and misappropriated this under-reported gold and silver doré bullion for his own use. Weston reports that Sorenson admitted that he had stolen as much as half of the gold and silver that he refined. A copy of a witnessed affidavit from Sorenson is available in Mojave Gold's files. (W. David Weston, personal communication, 2013).

Weston reports that in an effort to assess the gold remaining in the heap he dug and sampled several pits with a backhoe in 2009. Sampling of the material in the pits showed no gold remaining. (W. David Weston, personal communication, 2013.) (The author doubts the analytical work done in 2009 as there should at least have been some unrecovered gold in the pile Weston sampled if Pitt's [1986] estimate of 72% recovery from the pile was at all accurate.)

With Mojave Gold's reported production of about 600 ounces and Sorenson's admission of stealing another 600 ounces, some 3000 ounces still remain unaccounted and should have been in the heap when Weston sampled it in 2009.

The Telegraph Associates operated the mine from 1981 to the end of production in early 1982 and controlled the property from 1981 until 1989. In late 1981 a dispute was developing between the Associates and Cascade Energy and Metals over the apparently low gold recovery from the operation, and the Associates who were controlling the operation at the mine site may have taken this opportunity to recoup some of their investment by taking concentrates or gold- and silver-laden diatomaceous earth mats may have been taken from the plant at the mine site to another refining operation unknown to Cascade.

However, what has happened to that gold is only conjecture, and it is now 30 years after-the-fact. The author believes that Pitt's (1986) estimate of what went into the pile in 1981-1982 was probably accurate. The author has seen the pit in the area of Hill No. 2 and the leach pile, and Pitt's estimates of gold onto the leach pile conforms to all earlier sampling data from the Telegraph mine property and conforms to the sampling data from the 1981-1982 drill program in the area of the pit. While the author can certainly accept that there may have been pilferage in the refinery and at the mine site, he doubts that such pilferage could account for all of the missing gold, and he suspects that some of that gold still remains in the heap leach pile.

The pile should be systematically sampled and tested.

## 25. Interpretation and Conclusions

In the author's professional opinion the Telegraph Mine is an excellent property with a well-identified gold resource and considerable potential to enlarge that resource. The majority of resources that have been identified are near-surface and amenable to heap or vat leaching with a NaCN solution. Good recoveries have also been found in preliminary metallurgical testing for conventional milling and floatation. The deposit is adjacent to an interstate highway with excellent access; all required services should be available either in Las Vegas, Nevada, 70 miles to the east, or Barstow, California 83 miles to the west.

Drill sampling at the Telegraph Mine has not been done up to current industry standards with most of the drilling by percussion hammer drill. However, most of this drilling was done over 30 years ago, and under the then current drilling technology, percussion drilling may very well have been the best drill sampling method for this deposit. The core drilling at the Telegraph Mine which had been done by Ito (1969) resulted in very poor core recovery results, particularly in the vein itself. The percussion drilling done in the early 1980s should have produced satisfactory recovery, and issues with dilution of the samples common to percussion drilling would have been minimized due to the holes all being relatively short. Similarly the analyses at CEMCorp Laboratory with AA spectrometry did not have the precision that would be available with current (2013) techniques, but the AA-spectrometry may very well have been the best analytical technique then available for these relatively low-level samples (Weston & Dickerson, 1983).

Significant sampling efforts by Ito (1968 & 1969), Owens (1980), Jensen (1981) and Cascade Energy & Minerals (1981-1982) displays a consistence in tenor that is particularly reassuring. Resource estimates by Ito (1968 & 1969), Owens (1980), Jensen (1981), Daily, (1982), Ryzak (2009) and Mojave Gold (2011) display a similarly reassuring consistency in tenor and a steady increase in tonnage that would be expected.

The potential for a large-volume, low-grade gold deposit at the Telegraph Mine is particularly noteworthy. Historically exploration and development efforts at the Telegraph Mine have always been directed towards production from the main Telegraph vein itself and immediately adjacent hanging wall and footwall. However, review of the results of the 1981-1982 drilling program at the Telegraph Mine and at the adjacent Gold Dyke property suggest there may be excellent potential for a substantially larger, albeit lower-grade deposit on the property.

Future work at the property should recognize today's economic conditions. Results from the Cascade Energy and Metals 1981-1982 percussion drilling program show numerous drill holes well away from the main Telegraph vein with 40-foot to 80-foot intercepts of about 1.0 g/T or greater. Additionally many of the holes into and through the vein itself bottomed with their last sample greater than 1.0 g/T and should be considered "open at depth." (See Tables 6, 7 & 8; Figures 9, 10 & 11; and Appendices B, C & D.)

The author believes that a very good possibility exists for the development of a surface-mineable resource of up to ten or more million tons of material grading +1.0 g/T Au in the immediate area of the main Telegraph vein on the three patented claims. Additional resources of similar grade may exist on the adjacent Telegraph and Gold Dyke claims and on unclaimed lands in the area.

Resolution of the current litigation regarding claim validity and a thorough assessment of the permitting requirements for development of the Telegraph Mine must be accomplished to determine which of these potential resources may be exploitable.

## 26. Recommendations

Mojave Gold's intent with the Telegraph Mine property is to move directly towards production first from a surface mine and later from an underground mine, exploiting the high-grade Telegraph vein and the somewhat lower-grade footwall and hanging wall, initially between the Hill No. 1 (Shaft No. 1) and Hill No. 2 (Shaft No. 2) areas.

The author recommends the following preliminary work to be done prior to commencement of any mining activities. This work could be done during the engineering phase for the proposed surface mining operation.

(1) Field checking of Lange's (1988) geologic map.
(2) Plotting of all historic drill and sampling data in a 3-dimensional electronic model. This could be anything from ArcGIS to a more sophisticalte exploration software (Gemcom Surpak or similar) to a mining software (Vulcan or similar).
(3) Selection of 50 historic samples for check analyses to determine accuracy and precision of the historic analytical work.
(4) Core drilling of the main Telegraph vein, initially in the area of Hill No. 1 to Hill No. 2 (specifically a program should be designed to drill six to eight 300-foot vertical HQ or PQ holes sited on line along an azimuth of approximately N28$^{0}$E on roughly 200-foot centers, designed to intersect the vein at a depth of 250 feet, in the area).

Lange's (1988) geologic map should be field checked not so much to check Lange's mapping but to familiarize the geologists working on the project with the local geology. This should be one of the first tasks performed. The Telegraph property is more complex geologically than it may first appear to be, and Lange appears to have done an excellent job with it. His work should be continued with particular attention to hydrothermal alteration of the intrusive host rocks.

The plotting of the historic sampling and drill data in ArcGIS or a similar GIS program would greatly aid future work on the property. Higher-level versions of ArcGIS can also be used to display data in three dimensions, and while they cannot be used for modeling of deposits, the three dimensional view of the mineralized zones at the Telegraph Mine would greatly aid in evaluation of the property.

Historic analytical data can always be questioned by potential joint-venture partners or investors in a property. Cascade Energy and Metals and subsequent holders of the property have wisely kept splits of all samples collected since 1974 at the Telegraph Mine so that they would be available for future check analyses. The author recommends that up to 50 of these historic samples be selected based on their sample location and initial analyses. New analyses of these should erase any concerns regarding the quality of the historic analytical work and should also result in data with better precision and a decision as to whether or not a systematic program of re-analyses of the historic samples should be undertaken.

Core drilling is recommended to obtain samples from the Telegraph vein and the hanging and foot wall at depth. Historic drilling was mostly by percussion drilling because historic core drilling had resulted in poor core recovery. Today's core drilling technologies are much advanced from 1982, and good recovery should be anticipated. If initial drilling does not result in adequate recovery, the program should be suspended until a drilling or mud engineer can be brought onto the property to re-design the drill program to obtain satisfactory recovery. Larger diameter core (HQ or PQ) is recommended both to help with recovery and to reduce to the extend practical the "nugget effect" common with vein-hosted gold deposits. 888

Initially a program with six or so 300-foot holes collared about 250 feet west (on the Telegraph Grid) from the vein outcrop and spaced about 200 feet apart from roughly 2100 South to roughly 3100 South and designed to intercept the Telegraph vein at a depth of 250 feet (which would be about 350 feet down-dip) is recommended. Additional core drilling could be done to the north or south or closer to the vein if such were determined to be beneficial to the assessment of the project.

In addition to this work recommended for the Telegraph vein, the author recommends that the 1982 heap leach pile should be thoroughly drilled and sampled to determine how much gold may remain in the pile. Because the pile is all material that has been ground to -¼-inch and agglomerated, this should be a relatively inexpensive sampling program. Per Pitt's (1986) estimation, based on truck loading data, an estimated 24,646 tons of ore from the Telegraph Mine were mined, ground, agglomerated, and stacked on the pile in 1981-1982. The heap leach pile is approximately 330 feet by 150 feet and averages about 10-feet in height. Total recovery of gold from the pile is unknown, and significant gold may very well remain in the pile. If such is the case efforts should be directed towards recovering it. A drilling company should be consulted to determine the best means of sampling this material. There could also be significant gold that has been dissolved out from the leach pile and precipitated into the pregnant pond over the years, and the sediments at the bottom of the pond should be checked.

A reconnaissance program to assess the potential for a large-volume, low-grade deposit is also recommended following completion of the above work recommendations.

The VLF-EM data from Lange's (1988) M.S. thesis should be examined and evaluated by a competent geophysicist, and, if warranted, an electro-magnetic program designed to help map the location of the Telegraph vein and other veins in the area.

Pending results of the geophysical work and the alteration mapping and assessment of the historic drill data after it has been loaded into ArcGIS or some similar software and plotted, a reverse-circulation program of relatively shallow (initially up to 100 feet?) drill holes should be designed to sample the Telegraph vein area and surroundings in an attempt to develop a large-volume mineable target.

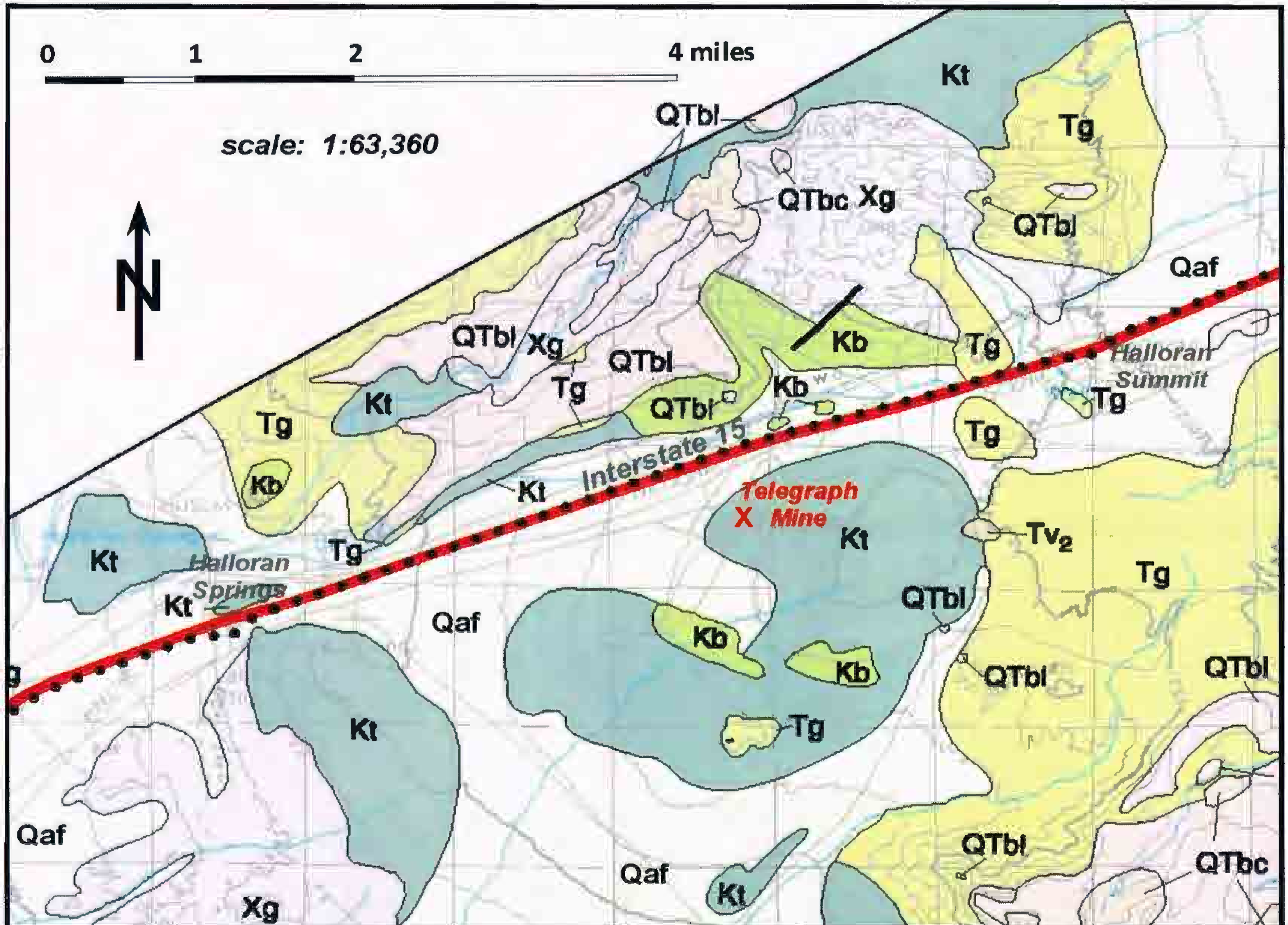


Figure 14. General geology of the central Halloran Hills (Telegraph Mine area) (from Miller *et al.*, 2007, U.S.G.S. Bul. 2160, Plate 1).

## Description of Map Units for Figure 14

| | |
|---|---|
| Qaf | **Alluvial fan deposits and alluvium (Holocene and Pleistocene)**—Unconsolidated deposits of poorly sorted gravel, sand, and silt. Deposited as alluvial cones at mouths of canyons and gullies, as alluvial floodplains that border streams, and as braided-stream sediments in stream channels. Older deposits form piedmonts that flank mountain ranges, as well as typically underlie raised, paved, and varnished surfaces |
| QTbl | **Basalt lava flows (Pleistocene to late Miocene)**—Alkaline basalt and hawaiite flows. |
| QTbc | **Basalt cinder deposits (Pleistocene to late Miocene)**—Unconsolidated deposits of basalt-scoria fragments, consolidated pyroclastic breccia, and tuffaceous conglomerate formed by phreatic eruption during vent opening. |
| Tg | **Gravel (Pliocene and Miocene)**—Moderately consolidated, crudely bedded, fluvial boulder to pebble gravel and sand interbedded with coarse to extremely coarse debris-flow deposits, avalanche breccia, and gravity-slide breccia. Sand is siliciclastic and volcaniclastic, locally arkosic. In and east of New York Mountains, typically forms highly incised raised terraces. Intercalated gravity-slide blocks between Cima Dome and Old Dad Mountain consist of breccias of dolomite, limestone, chert, quartzite, and volcanic, metamorphic, and granitoid rocks |
| $Tv_2$ | **Older volcanic rocks (Miocene)**—Rhyolite lava flows and ash flows, tuffaceous sedimentary rocks, tuff breccia, basalt flows, and andesite flows |
| Kt | **Teutonia adamellite of Beckerman and others (1982) (Cretaceous)**—Informally named unit. White to light-tan, equigranular to porphyritic (contains pink alkali-feldspar phenocrysts) biotite monzogranite, generally medium and coarse grained. Locally varies in composition to syenogranite and quartz monzonite. Minor muscovite present in places. These rocks were called granitic rocks of Kelso Peak by Dunne (1972). Crops out over much of Cima Dome, where it was dated at 97 Ma in age by U–Pb methods on zircon (DeWitt and others, 1984) |
| Kb | **Biotite-rich granitoid rocks (Cretaceous)**—Gray, equigranular to porphyritic (contains small pink alkali-feldspar phenocrysts), biotite-rich granitoid rocks, generally medium or coarse grained. Biotite content 10 volume percent or greater; biotite-rich schlieren widely present, abundant in places. Mapped in Halloran Wash and to south. Considered Cretaceous in age by DeWitt and others (1984) |
| Xg | **Gneiss and granitoids (Early Proterozoic)**—Undivided migmatite, granitoid gneiss, and granitoids mapped in many poorly known locations across map area. Also includes quartzite and quartzo-feldspathic paragneiss at Old Dad Mountain |

**Contact**—Dashed where approximately located

**Normal fault**—Dashed where inferred; dotted where concealed

**Boundary of East Mojave National Scenic Area (EMNSA, this report)**

**Boundary of Mojave National Preserve (current as of March 2007)**

Figure 14 explanation (from Miller *et al.*, 2007, U.S.G.S. Bul. 2160, Plate 1).

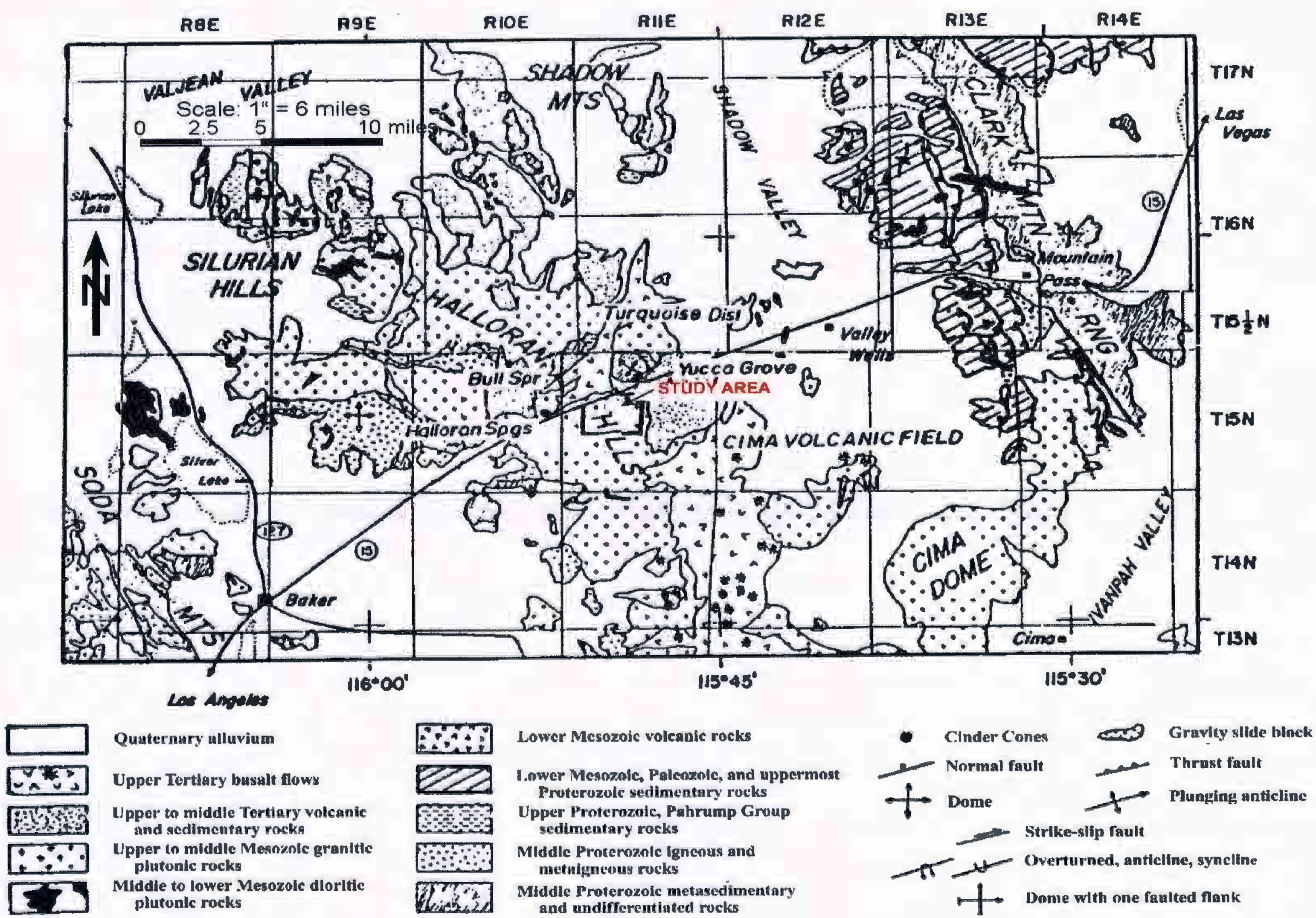


Figure 15. Geology of the Halloran Hills and environs (from Lange, 1988, modified after DeWitt, 1980).

| Table 6. Summary of 1981-1982 Telegraph Mine Hill No. 2 Area Drill Results | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| CEM Drill Hole No. | Collar | | | | | | Samples | | Comments |
| | N-S | E-W | Elev. | Az. | Incl. | length | No. of samples | Average Au (g/T) | |
| CEM 2-1a | 2182S | 149W | 3855 | 118 | -45 | 24' | 12 | 15.37 | open at bottom; last sample 9.60 g/T Au. |
| CEM 2-2a | 2188S | 149W | 3855 | 118 | -45 | 24' | 12 | 9.69 | open at bottom; last sample 3.77 g/T Au. |
| CEM 2-3a | 2194S | 149W | 3855 | 118 | -45 | 24' | 12 | 5.09 | open at bottom; last sample 3.43 g/T Au. |
| CEM 2-1 | 2225S | 135W | 3856 | 118 | -46 | 36' | 18 | 16.06 | open at bottom; last sample 3.09 g/T Au. |
| CEM 2-4a | 2232S | 210W | 3876 | 118 | -45 | 60' | 30 | [illegible] | mostly spotty weak mineralization; 14-16' -- 6.86 g/T; 48-50' -- 15.77 g/T Au. |
| CEM 2-2 | 2240S | 135W | 3858 | 118 | -45 | 36' | 18 | 5.07 | open at bottom; last sample 8.57 g/T Au. |
| CEM 2-12 | 2240S | 170W | 3862 | 118 | -45 | 20' | 10 | [illegible] | open at bottom; last sample [illegible] g/T Au. |
| CEM 2-3 | 2250S | 135W | 3893 | 118 | -45 | 48' | 24 | 6.79 | open at bottom; last sample [illegible] g/T Au. |
| CEM 2-4 | 2260S | 138W | 3862 | 118 | -45 | 36' | 18 | 6.95 | open at bottom; last sample 7.54 g/T Au. |
| CEM 2-5 | 2270S | 138W | 3867 | 118 | -45 | 48' | 24 | [illegible] | open at bottom; last sample [illegible] g/T Au. |
| CEM 2-6 | 2280S | 140W | 3866 | 118 | -45 | 36' | 18 | 7.77 | open at bottom; last sample 7.54 g/T Au. |
| CEM 2-7 | 2290S | 144W | 3862 | 118 | -45 | 50' | 25 | 4.06 | last sample (48-50') 0.34 g/T; 46-48' -- 3.43 g/T Au. |
| CEM 2-12a | 2291S | 200W | 3870 | 118 | -45 | 50' | 25 | 4.21 | open at bottom; last sample 9.26 g/T Au. |
| CEM 2-8 | 2305S | 150W | 3860 | 118 | -45 | 30' | 11 | 7.73 | no sample 0-2', 4-6', 6-8' & 22-24'; open at bottom; last sample 3.77 g/T Au. |
| CEM 2-13 | 2320S | 70W | 3894 | 332 | -45 | 50' | 25 | [illegible] | mostly spotty weak mineralization; 24-26' intercept of 4.11 g/T Au. |
| CEM 2-9 | 2320S | 164W | 3858 | 118 | -45 | 40' | 20 | 3.46 | open at bottom; last sample [illegible] g/T Au. |
| CEM 2-10 | 2340S | 170W | 3874 | 118 | -45 | 40' | 20 | [illegible] | open at bottom; last sample [illegible] g/T Au. |
| CEM 2-11 | 2384S | 210W | 3856 | 118 | -45 | 60' | 30 | [illegible] | open at bottom; last sample [illegible] g/T Au. |
| CEM 2-14 | 2450S | 65W | 3865 | 118 | -45 | 60' | 30 | 0.96 | spotty weak mineralization; three 2-foot sections of [illegible] g/T Au. |
| CEM 2-18 | 2462S | 225W | 3845 | 118 | -45 | 62' | 28 | 0.81 | spotty weak mineralization; no samples 0-6'; two 2-foot sections of [illegible] g/T Au. |
| CEM 2-19 | 2480S | 225W | 3849 | 118 | -45 | 50' | 25 | 0.44 | minor spotty weak mineralization. |
| CEM 2-15 | 2490S | 60W | 3864 | 118 | -45 | 80' | 40 | [illegible] | spotty weak mineralization; three 2-foot sections of 3.09 g/T Au. |
| CEM 2-16 | 2500S | 100W | 3851 | 118 | -45 | 60' | 30 | 0.94 | spotty weak mineralization; one 2-foot sections of 3.09 g/T and one of [illegible] g/T Au. |
| CEM 2-17 | 2500S | 150W | 3847 | 118 | -45 | 60' | 30 | 0.87 | spotty weak mineralization; two consecutive 2-foot sections of [illegible] g/T Au. |
| CEM 2-20 | 2510S | 225W | 3845 | 118 | -45 | 60' | 30 | 0.39 | spotty very weak mineralization. |

See Appendix Y for detail.

| | | |
|---|---|---|
| Color coding: | 0.50 to 0.99 g/T Au | yellow |
| | 1.00 to 2.99 g/T Au | [illegible] |
| | 2.99 g/T Au or greater | red |

| Table 7. Summary of 1981-1982 Telegraph Mine Hill No. 1 Area Drill Results | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| CEM Drill Hole No. | Collar | | | | | | Samples | | Comments |
| | N-S | E-W | Elev. | Az. | Incl. | length | No. of samples | Average Au (g/T) | |
| CEM 1-6 | 2960S | 110W | 3863 | 298 | -30 | 34' | 17 | 6.07 | drilled -30$^0$ to west; open at bottom; last 3 samples: 14.74, 36.69 & 27.09 g/T Au. |
| CEM 1-3 | 2960S | 190W | 3861 | 118 | -45 | 60' | 30 | 3.09 | open at bottom; last sample [illegible] g/T; 32'-52' intercept of 4.97 g/T Au. |
| CEM 1-5 | 2970S | 110W | 3865 | 298 | -30 | 30' | 15 | [illegible] | drilled -30$^0$ to west; open at bottom; last sample 5.49 g/T Au. |
| CEM 1-2 | 2970S | 190W | 3861 | 118 | -45 | 38' | 19 | [illegible] | open at bottom; last sample 5.14 g/T Au. |
| CEM 1-4 | 2980S | 110W | 3867 | 298 | -30 | 40' | 20 | [illegible] | drilled -30$^0$ to west; open at bottom; last sample 11.66 g/T Au. |
| CEM 1-1 | 2980S | 190W | 3860 | 118 | -45 | 36' | 18 | [illegible] | open at bottom; last sample 3.43 g/T Au. |
| CEM 1-16 | 3000S | 135W | 3770 | 0 | -90 | 10' | 2 | 18.00 | 10' vertical hole (collared on vein). |
| CEM 1-23 | 3004S | 161W | 3876 | 163 | -45 | 60' | 30 | [illegible] | open at bottom; last sample [illegible] g/T; 30'-60' intercept of [illegible] g/T incl. 30'-48' of 3.96 g/T Au. |
| CEM 1-26 | 3020S | 220W | 3850 | 118 | -45 | 62' | 30 | 0.49 | spotty weak mineralization with two 2-foot samples of [illegible] g/T Au. |
| CEM 1-24 | 3021S | 178W | 3857 | 163 | -45 | 60' | 30 | [illegible] | spotty weak mineralization at top; 30'-56' intercept of 6.06 g/T incl. 32'-48' of 8.49 g/T Au. |
| CEM 1-17 | 3024S | 136W | 3885 | 0 | -90 | 10' | 2 | 16.63 | 10' vertical hole (collared on vein). |
| CEM 1-18 | 3033S | 136W | 3888 | 0 | -90 | 10' | 2 | 0.34 | 10' vertical hole (collared on vein?). |
| CEM 1-25 | 3038S | 195W | 3852 | 163 | -45 | 60' | 30 | [illegible] | open at bottom; spotty weak mineralization at top to 20'; 20'-60' intercept of [illegible] g/T Au. |
| CEM 1-32 | 3045S | 255W | 3851 | 118 | -45 | 64' | 30 | 0.49 | spotty weak mineralization; one 2-foot samples of [illegible] g/T Au. |
| CEM 1-31 | 3050S | 90W | 3877 | 118 | -45 | 60' | 30 | [illegible] | mostly weak mineralization; one 2-foot samples of 19.54 g/T Au at 32'-34'. |
| CEM 1-19 | 3070S | 190W | 3870 | 0 | -90 | 10' | 2 | 3.60 | 10' vertical hole (collared on vein). |
| CEM 1-27 | 3070S | 220W | 3854 | 118 | -45 | 36' | 18 | 0.65 | weak mineralization to 28'; 28'-36' intercept of [illegible] g/T; open at bottom; last sample [illegible] g/T Au. |
| CEM 1-20 | 3100S | 200W | 3868 | 0 | -90 | 10' | 2 | 0.51 | 10' vertical hole (collared on vein?). |
| CEM 1-28 | 3100S | 220W | 3858 | 118 | -45 | 12' | 6 | 0.86 | spotty weak mineralization; open at bottom; last sample [illegible] g/T Au. |
| CEM 1-29 | 3135S | 170W | 3866 | 332 | -45 | 60' | 30 | 0.31 | weak to nil mineralization throughout hole. |
| CEM 1-30 | 3169S | 220W | 3850 | 118 | -45 | 66' | 30 | [illegible] | mostly spotty weak mineralization; 8'-18' intercept of 5.28 g/T Au. |

See Appendix Y for detail.

| Color coding: | 0.50 to 0.99 g/T Au | yellow |
|---|---|---|
| | 1.00 to 2.99 g/T Au | [illegible] |
| | 2.99 g/T Au or greater | red |

**Table 8. Summary of 1981-1982 Telegraph Mine Northern Extension Area Drill Results.**

| CEM Drill Hole No. | Collar | | | | | | Samples | | Comments |
|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | length | No. of samples | Average Au (g/T) | |
| CEM N-10 | 270N | 390W | 3827 | 68 | -45 | 60' | 4 | [illegible] | 6-foot samples; only last 24 feet (36'-60') sampled. |
| CEM N-9 | 202N | 285W | 3835 | 31 | -45 | 12' | 0 | - | no samples collected. |
| CEM N-8 | 202N | 285W | 3835 | 78 | -45 | 60' | 6 | [illegible] | 6-foot samples; only last 36 feet (24'-60') sampled; open at bottom with 1.51 g/T Au sample. |
| CEM N-11 | 102N | 120W | 3847 | 105 | -45 | 60' | 2 | **0.36** | 6-foot samples; only 12-foot intercept from 30' to 42' sampled. |
| CEM N-7 | 25N | 155W | 3842 | 133 | -45 | 60' | 5 | [illegible] | 6-foot samples; only last 30 feet (30'-60') sampled. |
| CEM N-6 | 75S | 175W | 3843 | 118 | -45 | 60' | 2 | **0.22** | 6-foot samples; only 12-foot intercept from 36' to 48' sampled. |
| CEM N-4 | 200S | 234W | 3837 | 118 | -45 | 60' | 5 | [illegible] | 6-foot samples; only last 30 feet (24'-30' & 36'-60') sampled. |
| CEM N-5 | 200S | 225W | 3838 | 118 | -60 | 60' | 6 | **0.49** | 6-foot samples; only last 36 feet (24'-60') sampled; open at bottom with 1.23 g/T Au sample. |
| CEM N-3 | 300S | 332W | 3836 | 118 | -45 | 60' | 4 | [illegible] | 12-foot & 6-foot samples; only intercept from 12" to 42' sampled. |
| CEM N-13 | 350S | 216W | 3839 | 118 | -45 | 30' | 12 | [illegible] | 2-foot samples; entire hole sampled. |
| CEM N-1 | 350S | 225W | 3837 | 118 | -45 | 60' | 13 | [illegible] | 2-foot samples; 12' to 60' sampled; open at bottom with 1.37 g/T Au sample. |
| CEM N-12 | 500S | 225W | 3835 | 118 | -45 | 60' | 3 | [illegible] | 6-foot samples; only 18-foot intercept from 30' to 48' sampled. |

| Color coding: | | |
|---|---|---|
| | 0.50 to 0.99 g/T Au | [illegible] |
| | 1.00 to 2.99 g/T Au | [illegible] |
| | 2.99 g/T Au or greater | red |

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# Appendix

# Appendix A

**Mojave Gold Mining Corporation Management Team**

# Appendix A.  Mojave Gold Mining Corporation Management Team

## W. DAVID WESTON, PRESIDENT, TREASURER and DIRECTOR

Mr. Weston was CEO of Cascade Energy and Metals Corporation from 1968-2002.  He managed copper porphyry and precious metals exploration programs for Pickands Mather & Company (Cleveland, Ohio).  He acquired, explored and developed the Rex Montis Mine (silver/gold) in Inyo, California, the Alexo Mine (Nickel) and Gawgonda (silver) properties in Ontario, Canada.  He also acquired and developed the Telegraph Mine (gold/silver), in San Bernardino County, California.  In the late 1960s he acquired and managed Minerals Drilling Co., located in Ely, Nevada, and the Arno Diamond Drilling Company, located in Timmins, Ontario.  On behalf of these companies he engaged in extensive drilling, exploration and mine development programs for precious metals in the western United States and Canada.

## KEN CLIFFORD, Ph.D., (Metallurgist), VICE PRESIDENT and DIRECTOR

Dr. Clifford received his Ph.D. in Metallurgy in 1971 from the University of Utah.  He joined St. Joe Minerals Corporation in 1972.  He was Director of Metallurgical Research over the Viburnum, Fletcher, Brushy Creek and Indian Creek mills in the Viburnum trend of Missouri through 1976.  For two years he managed the coal cleaning program at the Electric Power Research Institute.  He was Chief Metallurgist with Chevron Resources and assisted in developing the Stillwater PGM resource in Montana and phosphate expansion at Vernal, Utah. Dr. Clifford was General Manager of Golden Bear Operating Company joint venture, subsumed into Homestake Mining Co.  He held mill supervisory assignments at Timmins, Ontario; Greens Creek, Alaska, and Kennecott Utah Copper.  He has provided consulting to the Rio Grande Mining Co. on the Shafter mine production circuit in Texas, and evaluated the Gold Hill mining area in Utah and Minas de Oro mining property in Honduras.   Dr. Clifford has conducted a consulting practice in the U.S., Canada, Europe, South America and Australia to establish advanced mining and milling practices.

## CHERIE M. TILLEY, (Mine Manager) DIRECTOR

Mr. Tilley has 50 years' experience in the mining industry with over 37 years as a mine supervisor.   He was General Mine Superintendent at the Mariano Lake Mine, a 450 tpd uranium mine, and at the Mt. Taylor Project (uranium) in New Mexico, sinking shafts to 3,300 foot depth. He was Development Manager at the Nose Rock Project in Crown Point, New Mexico, for Phillips Uranium Corporation, sinking shafts to 3,000 foot depth, and was Mine Development Director for Phillips Petroleum Company, responsible for evaluating and developing mines worldwide.  He was Vice President, Mine Operations, for American Mine Services Corporation, a worldwide contractor for shaft sinking and mine development.  He was Mine Manager at the Stillwater Mine in Montana for Chevron Resources Corporation.  He was Project Manager for Dynatec Mining Corporation, including the Barrick Meikle Shaft Deepening, and at the Ken Snyder Mine.  At the Barick Mielke Mine he oversaw mine development and sinking production, ventilation shafts, the development of three mine levels, seven shaft stations and two loading pockets.  At the 2013 Annual Meeting of the Society of Mining Engineers the M&E division awarded Mr. Tillie it's prestigious "Miner of the Year Award."  Mr. Tilley consults through his company, Tilley Exploration and Development Company.

DAVID RYZAK, (Geologist), DIRECTOR

Mr. Ryzak is a mine development and production geologist with a B.S. in geology from Michigan Technological University. He was employed as an underground mine geologist at the Hecla Mining Company's Lakeshore Copper Mine in Arizona, and by Cobb Resources' as the mine development geologist at their underground uranium mine in the Ambrosia Lake district of New Mexico and as a development and underground mine geologist their London Mine (gold) near Fairplay, Colorado. He was employed by C&S Resources to reopen an underground silver mine at Gold Point, Nevada. He worked as a developmental and production geologist for Pegasus Gold Corporation at their Zortman and Landusky mining operations at Zortman, Montana. Pegasus Gold transferred Mr. Ryzak as Senior Geologist to the New Black Pine Mine located southeast of Burley, Idaho. Mr. Ryzak has worked as a consulting geologist providing geologic reports, mine economic evaluations and reclamation permitting for his clients.

TY WESTON , VICE PRESIDENT, SECRETARY and DIRECTOR

Mr. Weston most recently served as the Chief Operating Officer of XOLogic Corp, the leading provider of e-commerce, retail data services to the lighting industry. He was CEO of Deseret Health Group (11 nursing & assisted living facilities) and Director of Operations Support for Deltacom, a $600m/year public company. He was Director of Operations Excellence for Worldcom, a public telecommunications company. He served as Director of U.S. Technical Support at Packard Bell NEC. He has been certified as a Six Sigma Black Belt by the American Society for Quality (ASQ), the largest organization of quality professionals in the world.

# Appendix B

**Telegraph Hill No. 2 Area Drill Data**

Appendix B.  Telegraph Hill No. 2 Area Drill Data.

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM 2-1a | 2182S | 149W | 3855.0 | 118 | -45 | 24' | | | | | | | | | | |
| | -2182 | 147.6 | 3853.6 | | | | 2343 | T2579 | 0'-2' | | | | 0.060 | **2.06** | | |
| | -2182 | 146.2 | 3852.2 | | | | 2344 | T2580 | 2'-4' | | | | 0.030 | **1.03** | | |
| | -2182 | 144.8 | 3850.8 | | | | 2345 | T2581 | 4'-6' | | | | 0.060 | **2.06** | | |
| | -2182 | 143.3 | 3849.3 | | | | 2346 | T2582 | 6'-8' | | | | 0.230 | **7.89** | | |
| | -2182 | 141.9 | 3847.9 | | | | 2347 | T2583 | 8'-10' | | | | 0.250 | **8.57** | | |
| | -2182 | 140.5 | 3846.5 | | | | 2348 | T2584 | 10'-12' | | | | 0.330 | **11.31** | | |
| | -2182 | 139.1 | 3845.1 | | | | 2349 | T2585 | 12'-14' | | | | 0.060 | **2.06** | | |
| | -2182 | 137.7 | 3843.7 | | | | 2350 | T2586 | 14'-16' | | | | 3.660 | **125.49** | | |
| | -2182 | 136.3 | 3842.3 | | | | 2351 | T2587 | 16'-18' | | | | 0.290 | **9.94** | | |
| | -2182 | 134.9 | 3840.9 | | | | 2352 | T2588 | 18'-20' | | | | 0.010 | 0.34 | | |
| | -2182 | 133.4 | 3839.4 | | | | 2353 | T2589 | 20'-22' | | | | 0.180 | **6.17** | | |
| | -2182 | 132.0 | 3838.0 | | | | 2354 | T2590 | 22'-24' | | | | 0.280 | **9.60** | | |
| | | | | | | | | | | | | | | | | |
| CEM 2-2a | 2188S | 149W | 3855.0 | 118 | -45 | 24' | | | | | | | | | | |
| | -2188 | 147.6 | 3853.6 | | | | 2355 | T2591 | 0'-2' | | | | 0.040 | **1.37** | | |
| | -2188 | 146.2 | 3852.2 | | | | 2356 | T2592 | 2'-4' | | | | 0.110 | **3.77** | | |
| | -2188 | 144.8 | 3850.8 | | | | 2357 | T2593 | 4'-6' | | | | 0.290 | **9.94** | | |
| | -2188 | 143.3 | 3849.3 | | | | 2358 | T2594 | 6'-8' | | | | 0.340 | **11.66** | | |
| | -2188 | 141.9 | 3847.9 | | | | 2359 | T2595 | 8'-10' | | | | 1.350 | **46.29** | | |
| | -2188 | 140.5 | 3846.5 | | | | 2360 | T2596 | 10'-12' | | | | 0.200 | **6.86** | | |
| | -2188 | 139.1 | 3845.1 | | | | 2361 | T2597 | 12'-14' | | | | 0.170 | **5.83** | | |
| | -2188 | 137.7 | 3843.7 | | | | 2362 | T2598 | 14'-16' | | | | 0.510 | **17.49** | | |
| | -2188 | 136.3 | 3842.3 | | | | 2363 | T2599 | 16'-18' | | | | 0.020 | **0.69** | | |
| | -2188 | 134.9 | 3840.9 | | | | 2364 | T2600 | 18'-20' | | | | 0.050 | **1.71** | | |
| | -2188 | 133.4 | 3839.4 | | | | 2365 | T2601 | 20'-22' | | | | 0.200 | **6.86** | | |
| | -2188 | 132.0 | 3838.0 | | | | 2366 | T2602 | 22'-24' | | | | 0.110 | **3.77** | | |
| | | | | | | | | | | | | | | | | |
| CEM 2-3a | 2194S | 149W | 3855.0 | 118 | -45 | 24' | | | | | | | | | | |
| | -2194 | 147.6 | 3853.6 | | | | 2367 | T2603 | 0'-2' | | | | 0.230 | **7.89** | | |
| | -2194 | 146.2 | 3852.2 | | | | 2368 | T2604 | 2'-4' | | | | 0.080 | **2.74** | | |
| | -2194 | 144.8 | 3850.8 | | | | 2369 | T2605 | 4'-6' | | | | 0.050 | **1.71** | | |
| | -2194 | 143.3 | 3849.3 | | | | 2370 | T2606 | 6'-8' | | | | 0.480 | **16.46** | | |
| | -2194 | 141.9 | 3847.9 | | | | 2371 | T2607 | 8'-10' | | | | 0.360 | **12.34** | | |
| | -2194 | 140.5 | 3846.5 | | | | 2372 | T2608 | 10'-12' | | | | 0.150 | **5.14** | | |
| | -2194 | 139.1 | 3845.1 | | | | 2373 | T2609 | 12'-14' | | | | 0.120 | **4.11** | | |
| | -2194 | 137.7 | 3843.7 | | | | 2374 | T2610 | 14'-16' | | | | 0.020 | **0.69** | | |
| | -2194 | 136.3 | 3842.3 | | | | 2375 | T2611 | 16'-18' | | | | 0.160 | **5.49** | | |
| | -2194 | 134.9 | 3840.9 | | | | 2376 | T2612 | 18'-20' | | | | 0.030 | **1.03** | | |
| | -2194 | 133.4 | 3839.4 | | | | 2377 | T2613 | 20'-22' | | | | 0.100 | **3.43** | | |
| | | | | | | | | | | | | | | | | |
| CEM 2-1 | 2225S | 135W | 3856.0 | 118 | -46 | 36' | | | | | | | | | | |
| | -2225 | 133.6 | 3854.6 | | | | 246 | T1080 | 0'-2' | Hw | Aout | 0 | 0.070 | **2.40** | 0.07 | 2.40 |
| | -2225 | 132.2 | 3853.2 | | | | 247 | T1081 | 2'-4' | Hw | Aout | 0 | 0.060 | **2.06** | 0.13 | 4.46 |
| | -2225 | 130.8 | 3851.8 | | | | 403 | T1238 | 4'-6' | .Hw | A in | Qfn | 0.260 | **8.91** | 0.40 | 13.71 |
| | -2225 | 129.3 | 3850.3 | | | | 248 | T1082 | 6'-8' | Hw | A in | 0 | 0.060 | **2.06** | 0.13 | 4.46 |
| | -2225 | 127.9 | 3848.9 | | | | 404 | T1239 | 8'-10' | Hw | 0 | Qfnp | 1.140 | **39.09** | 0.48 | 16.46 |
| | -2225 | 126.5 | 3847.5 | | | | 249 | T1083 | 10'-12' | Hw | 0 | Qfnp | 2.230 | **76.46** | 2.81 | 96.34 |
| | -2225 | 125.1 | 3846.1 | | | | 250 | T1084 | 12'-14' | Hw | 0 | Qfnp | 1.250 | **42.86** | 0.57 | 19.54 |
| | -2225 | 123.7 | 3844.7 | | | | 405 | T1240 | 14'-16' | Hw | QSP | Qfn | 0.700 | **24.00** | 0.41 | 14.06 |
| | -2225 | 122.3 | 3843.3 | | | | 406 | T1241 | 16'-18' | Bx | QSP | Qfn | 0.610 | **20.91** | 0.47 | 16.11 |
| | -2225 | 120.9 | 3841.9 | | | | 251 | T1085 | 18'-20' | Bx | QSP | Qfn | 0.470 | **16.11** | 0.20 | 6.86 |
| | -2225 | 119.4 | 3840.4 | | | | 407 | T1242 | 20'-22' | Bx | Pin | Qvg | 0.430 | **14.74** | 0.44 | 15.09 |
| | -2225 | 118.0 | 3839.0 | | | | 408 | T1243 | 22'-24' | Fw | Pin | QFe | 0.310 | **10.63** | 0.61 | 20.91 |
| | -2225 | 116.6 | 3837.6 | | | | 409 | T1244 | 24'-26' | Fw | Pin | Qcmn | 0.200 | **6.86** | 0.33 | 11.31 |
| | -2225 | 115.2 | 3836.2 | | | | 252 | T1086 | 26'-28' | Fw | Pin | Qvgp | 0.270 | **9.26** | 0.87 | 29.83 |
| | -2225 | 113.8 | 3834.8 | | | | 253 | T1087 | 28'-30' | Fw | Pin | Qvgp | 0.110 | **3.77** | 0.08 | 2.74 |
| | -2225 | 112.4 | 3833.4 | | | | 254 | T1088. | 30'-32' | Fw | Pin | Qvgp | 0.100 | **3.43** | 0.10 | 3.43 |
| | -2225 | 111.0 | 3832.0 | | | | 410 | T1245 | 32'-34' | Fw | Pout | Qvgp | 0.070 | **2.40** | 0.09 | 3.09 |
| | -2225 | 109.5 | 3830.5 | | | | 255 | T1089 | 34'-36' | Fw | Pout | Qvgp | 0.090 | **3.09** | 0.08 | 2.74 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | | | | | | | | | | | | | | | | |
| CEM 2-4a | 2232S | 210W | 3876.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2232 | 208.6 | 3874.6 | | | | 2378 | T2614 | 0'-2' | | | | 0.040 | 1.37 | | |
| | -2232 | 207.2 | 3873.2 | | | | 2379 | T2615 | 2'-4' | | | | 0.070 | 2.40 | | |
| | -2232 | 205.8 | 3871.8 | | | | 2380 | T2616 | 4'-6' | | | | 0.020 | 0.69 | | |
| | -2232 | 204.3 | 3870.3 | | | | 2381 | T2617 | 6'-8' | | | | 0.060 | 2.06 | | |
| | -2232 | 202.9 | 3868.9 | | | | 2382 | T2618 | 8'-10' | | | | 0.030 | 1.03 | | |
| | -2232 | 201.5 | 3867.5 | | | | 2383 | T2619 | 10'-12' | | | | 0.060 | 2.06 | | |
| | -2232 | 200.1 | 3866.1 | | | | 2384 | T2620 | 12'-14' | | | | 0.030 | 1.03 | | |
| | -2232 | 198.7 | 3864.7 | | | | 2385 | T2621 | 14'-16' | | | | 0.200 | 6.86 | | |
| | -2232 | 197.3 | 3863.3 | | | | 2386 | T2622 | 16'-18' | | | | 0.060 | 2.06 | | |
| | -2232 | 195.9 | 3861.9 | | | | 2387 | T2623 | 18'-20' | | | | 0.030 | 1.03 | | |
| | -2232 | 194.4 | 3860.4 | | | | 2388 | T2624 | 20'-22' | | | | 0.030 | 1.03 | | |
| | -2232 | 193.0 | 3859.0 | | | | 2389 | T2625 | 22'-24' | | | | 0.060 | 2.06 | | |
| | -2232 | 191.6 | 3857.6 | | | | 2390 | T2626 | 24'-26' | | | | 0.010 | 0.34 | | |
| | -2232 | 190.2 | 3856.2 | | | | 2391 | T2627 | 26'-28' | | | | 0.020 | 0.69 | | |
| | -2232 | 188.8 | 3854.8 | | | | 2392 | T2628 | 28'-30' | | | | 0.060 | 2.06 | | |
| | -2232 | 187.4 | 3853.4 | | | | 2393 | T2629 | 30'-32' | | | | 0.020 | 0.69 | | |
| | -2232 | 186.0 | 3852.0 | | | | 2394 | T2630 | 32'-34' | | | | 0.020 | 0.69 | | |
| | -2232 | 184.5 | 3850.5 | | | | 2395 | T2631 | 34'-36' | | | | 0.020 | 0.69 | | |
| | -2232 | 183.1 | 3849.1 | | | | 2423 | T2660 | 36'-38' | | | | 0.010 | 0.34 | | |
| | -2232 | 181.7 | 3847.7 | | | | 2424 | T2661 | 38'-40' | | | | 0.010 | 0.34 | | |
| | -2232 | 180.3 | 3846.3 | | | | 2425 | T2662 | 40'-42' | | | | 0.020 | 0.69 | | |
| | -2232 | 178.9 | 3844.9 | | | | 2426 | T2663 | 42'-44' | | | | 0.020 | 0.69 | | |
| | -2232 | 177.5 | 3843.5 | | | | 2427 | T2664 | 44'-46' | | | | 0.050 | 1.71 | | |
| | -2232 | 176.1 | 3842.1 | | | | 2428 | T2665 | 46'-48' | | | | 0.040 | 1.37 | | |
| | -2232 | 174.7 | 3840.6 | | | | 2429 | T2666 | 48'-50' | | | | 0.460 | 15.77 | | |
| | -2232 | 173.2 | 3839.2 | | | | 2430 | T2667 | 50'-52' | | | | 0.010 | 0.34 | | |
| | -2232 | 171.8 | 3837.8 | | | | 2431 | T2668 | 52'-54' | | | | 0.000 | 0.00 | | |
| | -2232 | 170.4 | 3836.4 | | | | 2432 | T2669 | 54'-56' | | | | 0.020 | 0.69 | | |
| | -2232 | 169.0 | 3835.0 | | | | 2433 | T2670 | 56'-58' | | | | 0.010 | 0.34 | | |
| | -2232 | 167.6 | 3833.6 | | | | 2434 | T2671 | 58'-60' | | | | 0.020 | 0.69 | | |
| | | | | | | | | | | | | | | | | |
| CEM 2-2 | 2240 | 135W | 3858.0 | 118 | -45 | 36' | | | | | | | | | | |
| | -2240 | 133.6 | 3856.6 | | | | 256 | T1090 | 0'-2' | Hw | Pout | 0 | 0.080 | 2.74 | 0.09 | 3.09 |
| | -2240 | 132.2 | 3855.2 | | | | 257 | T1091 | 2'-4' | Hw | Pout | 0 | 0.140 | 4.80 | 0.17 | 5.83 |
| | -2240 | 130.8 | 3853.8 | | | | 258 | T1092 | 4'-6' | Hw | Pout | 0 | 0.080 | 2.74 | 0.07 | 2.40 |
| | -2240 | 129.3 | 3852.3 | | | | 411 | T1246 | 6'-8' | Hw | Pout | Qfnp | 0.040 | 1.37 | 0.09 | 3.09 |
| | -2240 | 127.9 | 3850.9 | | | | 412 | T1247 | 8'-10' | Hw | Pout | 0 | 0.090 | 3.09 | 0.16 | 5.49 |
| | -2240 | 126.5 | 3849.5 | | | | 413 | T1248 | 10'-12' | Hw | Pin | 0 | 0.050 | 1.71 | 0.11 | 3.77 |
| | -2240 | 125.1 | 3848.1 | | | | 414 | T1249 | 12'-14' | Bx | QSP | Qvg | 0.630 | 21.60 | 0.88 | 30.17 |
| | -2240 | 123.7 | 3846.7 | | | | 415 | T1250 | 14'-16' | Bx | QS | Qvg | 0.150 | 5.14 | 0.19 | 6.51 |
| | -2240 | 122.3 | 3845.3 | | | | 416 | T1251 | 16'-18' | Bx | QCSP | Qvg | 0.090 | 3.09 | 0.15 | 5.14 |
| | -2240 | 120.9 | 3843.9 | | | | 417 | T1252 | 18'-20' | Bx | QCP | Qfn | 0.210 | 7.20 | 0.23 | 7.89 |
| | -2240 | 119.4 | 3842.4 | | | | 259 | T1093 | 20'-22' | Fw | Pin | 0 | 0.140 | 4.80 | 0.17 | 5.83 |
| | -2240 | 118.0 | 3841.0 | | | | 260 | T1094 | 22'-24' | Fw | Pin | Qvg | 0.150 | 5.14 | 0.51 | 17.49 |
| | -2240 | 116.6 | 3839.6 | | | | 261 | T1095 | 24'-26' | Fw | Pout | 0 | 0.090 | 3.09 | 0.10 | 3.43 |
| | -2240 | 115.2 | 3838.2 | | | | 262 | T1096 | 26'-28' | Fw | Pout | Qcrnn | 0.130 | 4.46 | 0.08 | 2.74 |
| | -2240 | 113.8 | 3836.8 | | | | 263 | T1097 | 28'-30' | Fw | Pout | Qvg | 0.170 | 5.83 | 0.08 | 2.74 |
| | -2240 | 112.4 | 3835.4 | | | | 418 | T1253 | 30'-32' | Fw | Pout | 0 | 0.060 | 2.06 | 0.08 | 2.74 |
| | -2240 | 111.0 | 3834.0 | | | | 264 | T1098 | 32'-34' | Fw | Pout | 0 | 0.110 | 3.77 | 0.09 | 3.09 |
| | -2240 | 109.5 | 3832.5 | | | | 265 | T1099 | 34'-36' | Fw | Pout | 0 | 0.250 | 8.57 | 0.13 | 4.46 |
| | | | | | | | | | | | | | | | | |
| CEM 2-12 | 2240S | 170W | 3862.0 | 118 | -45 | 20' | | | | | | | | | | |
| | -2240 | 168.6 | 3860.6 | | | | 329 | T1163 | 0'-2' | Hw | Pin | | 0.100 | 3.43 | 0.06 | 2.06 |
| | -2240 | 167.2 | 3859.2 | | | | 330 | T1164 | 2'-4' | Hw | Pin | | 0.100 | 3.43 | 0.12 | 4.11 |
| | -2240 | 165.8 | 3857.8 | | | | 331 | T1165 | 4'-6' | Hw | Pin | Qfn | 0.040 | 1.37 | 0.01 | 0.34 |
| | -2240 | 164.3 | 3856.3 | | | | 332 | T1166 | 6'-8' | Hw | Pin | Qfnp | 0.100 | 3.43 | 0.12 | 4.11 |
| | -2240 | 162.9 | 3854.9 | | | | 333 | T1167 | 8'-10' | Bx | Pin | 0 | 0.090 | 3.09 | 0.12 | 4.11 |
| | -2240 | 161.5 | 3853.5 | | | | 334 | T1168 | 10'-12' | Bx | Pin | Qvgp | 0.130 | 4.46 | 0.02 | 0.69 |
| | -2240 | 160.1 | 3852.1 | | | | 335 | T1169 | 12'-14' | Bx | QC | Qvgp | 0.030 | 1.03 | 0.07 | 2.40 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2240 | 158.7 | 3850.7 | | | | 336 | T1170 | 14'-16' | Bx | QC | Qvgp | 0.110 | 3.77 | 0.13 | 4.46 |
| | -2240 | 157.3 | 3849.3 | | | | 337 | T1171 | 16'-18' | Bx | QC | Qvg | 0.060 | 2.06 | 0.18 | 6.17 |
| | -2240 | 155.9 | 3847.9 | | | | 338 | T1172 | 18'-20' | Fw | Pin | Qvg | 0.040 | 1.37 | 0.02 | 0.69 |
| | | | | | | | | | | | | | | | | |
| CEM 2-3 | 2250S | 135W | 3893.0 | 118 | -45 | 48' | | | | | | | | | | |
| | -2250 | 133.6 | 3891.6 | | | | 419 | T1254 | 0'-2' | Hw | 0 | QFe | 0.060 | 2.06 | 0.03 | 1.03 |
| | -2250 | 132.2 | 3890.2 | | | | 420 | T1255 | 2'-4' | Hw | QSP | Qvg | 0.470 | 16.11 | 0.50 | 17.14 |
| | -2250 | 130.8 | 3888.8 | | | | 421 | T1256 | 4'-6' | Hw | Pout | Qcmn | 0.270 | 9.26 | 0.23 | 7.89 |
| | -2250 | 129.3 | 3887.3 | | | | 422 | T1257 | 6'-8' | Hw | Pout | Qvgp | 1.230 | 42.17 | 0.32 | 10.97 |
| | -2250 | 127.9 | 3885.9 | | | | 423 | T1258 | 8'-10' | Hw | Pout | Qvg | 0.180 | 6.17 | 0.16 | 5.49 |
| | -2250 | 126.5 | 3884.5 | | | | 424 | T1259 | 10'-12' | Hw | Pout | 0 | 0.080 | 2.74 | 0.08 | 2.74 |
| | -2250 | 125.1 | 3883.1 | | | | 425 | T1260 | 12'-14' | Hw | Pin | Qvgp | 0.180 | 6.17 | 0.08 | 2.74 |
| | -2250 | 123.7 | 3881.7 | | | | 266 | T1100 | 14'-16' | Bx | QCSP | Qfn | 0.370 | 12.69 | 0.09 | 3.09 |
| | -2250 | 122.3 | 3880.3 | | | | 426 | T1261 | 16'-18' | Bx | QCP | Qfn | 0.280 | 9.60 | 0.10 | 3.43 |
| | -2250 | 120.9 | 3878.9 | | | | 267 | T1101 | 18'-20' | Bx | QCSP | Qvgp | 0.160 | 5.49 | 0.04 | 1.37 |
| | -2250 | 119.4 | 3877.4 | | | | 427 | T1262 | 20'-22' | Bx | QC | Qvg | 0.070 | 2.40 | 0.06 | 2.06 |
| | -2250 | 118.0 | 3876.0 | | | | 428 | T1263 | 22'-24' | Bx | QSP | Qvg | 0.080 | 2.74 | 0.02 | 0.69 |
| | -2250 | 116.6 | 3874.6 | | | | 429 | T1264 | 24'-26' | Fw | Pin | Qcmn | 0.280 | 9.60 | 0.05 | 1.71 |
| | -2250 | 115.2 | 3873.2 | | | | 430 | T1265 | 26'-28' | Fw | QS | FeO | 0.080 | 2.74 | 0.03 | 1.03 |
| | -2250 | 113.8 | 3871.8 | | | | 431 | T1266 | 28'-30' | Fw | Pout | FeO | 0.060 | 2.06 | 0.05 | 1.71 |
| | -2250 | 112.4 | 3870.4 | | | | 432 | T1267 | 30'-32' | Fw | Pout | FeO | 0.080 | 2.74 | 0.13 | 4.46 |
| | -2250 | 111.0 | 3869.0 | | | | 433 | T1268 | 32'-34' | Fw | Pout | Qvgp | 0.260 | 8.91 | 0.11 | 3.77 |
| | -2250 | 109.5 | 3867.5 | | | | 434 | T1269 | 34'-36' | Fw | QC | 0 | 0.180 | 6.17 | 0.05 | 1.71 |
| | -2250 | 108.1 | 3866.1 | | | | 268 | T1102 | 36'-38' | Fw | Pout | Qfn | 0.070 | 2.40 | 0.04 | 1.37 |
| | -2250 | 106.7 | 3864.7 | | | | 435 | T1270 | 38'-40' | Fw | Pout | Qfn | 0.040 | 1.37 | 0.05 | 1.71 |
| | -2250 | 105.3 | 3863.3 | | | | 436 | T1271 | 40'-42' | Fw | Pout | 0 | 0.090 | 3.09 | 0.16 | 5.49 |
| | -2250 | 103.9 | 3861.9 | | | | 437 | T1272 | 42'-44' | Fw | QC | 0 | 0.100 | 3.43 | 0.08 | 2.74 |
| | -2250 | 102.5 | 3860.5 | | | | 438 | T1273 | 44'-46' | Fw | Pout | 0 | 0.040 | 1.37 | 0.09 | 3.09 |
| | -2250 | 101.1 | 3859.1 | | | | 439 | T1274 | 46'-48' | Fw | Pout | 0 | 0.040 | 1.37 | 0.08 | 2.74 |
| | | | | | | | | | | | | | | | | |
| CEM 2-4 | 2260S | 138W | 3862.0 | 118 | -45 | 36' | | | | | | | | | | |
| | -2260 | 136.6 | 3860.6 | | | | 269 | T1103 | 0'-2' | Hw | Pout | 0 | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2260 | 135.2 | 3859.2 | | | | 440 | T1275 | 2'-4' | Hw | Pout | 0 | 0.060 | 2.06 | 0.06 | 2.06 |
| | -2260 | 133.8 | 3857.8 | | | | 270 | T1104 | 4'-6' | Hw | Pout | 0 | 0.100 | 3.43 | 0.05 | 1.71 |
| | -2260 | 132.3 | 3856.3 | | | | 441 | T1276 | 6'-8' | Hw | Pout | 0 | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2260 | 130.9 | 3854.9 | | | | 442 | T1277 | 8'-10' | Hw | QC | 0 | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2260 | 129.5 | 3853.5 | | | | 271 | T1105 | 10'-12' | Hw | QC | Qvg | 0.060 | 2.06 | 0.05 | 1.71 |
| | -2260 | 128.1 | 3852.1 | | | | 272 | T1106 | 12'-14' | Bx | QCSP | Qvg | 1.520 | 52.11 | 0.65 | 22.29 |
| | -2260 | 126.7 | 3850.7 | | | | 443 | T1278 | 14'-16' | Bx | QCS | Qvg | 0.370 | 12.69 | 0.75 | 25.71 |
| | -2260 | 125.3 | 3849.3 | | | | 273 | T1107 | 16'-18' | Bx | QCS | Qvg | 0.110 | 3.77 | 0.04 | 1.37 |
| | -2260 | 123.9 | 3847.9 | | | | 274 | T1108 | 18'-20' | Bx | Pin | Qvg | 0.280 | 9.60 | 0.06 | 2.06 |
| | -2260 | 122.4 | 3846.4 | | | | 444 | T1279 | 20'-22' | Fw | A in | Qfn | 0.230 | 7.89 | 0.06 | 2.06 |
| | -2260 | 121.0 | 3845.0 | | | | 445 | T1280 | 22'-24' | Fw | Aout | Qvg | 0.170 | 5.83 | 0.11 | 3.77 |
| | -2260 | 119.6 | 3843.6 | | | | 446 | T1281 | 24'-26' | Fw | Aout | Qvg | 0.080 | 2.74 | 0.16 | 5.49 |
| | -2260 | 118.2 | 3842.2 | | | | 447 | T1282 | 26'-28' | Fw | Aout | Qvg | 0.240 | 8.23 | 0.05 | 1.71 |
| | -2260 | 116.8 | 3840.8 | | | | 275 | T1109 | 28'-30' | Fw | Pout | D | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2260 | 115.4 | 3839.4 | | | | 448 | T1283 | 30'-32' | Fw | Pout | 0 | 0.040 | 1.37 | 0.08 | 2.74 |
| | -2260 | 114.0 | 3838.0 | | | | 449 | T1284 | 32'-34' | Fw | Pout | 0 | 0.020 | 0.69 | 0.07 | 2.40 |
| | -2260 | 112.5 | 3836.5 | | | | 276 | T111O | 34'-36' | Fw | Pout | 0 | 0.220 | 7.54 | 0.12 | 4.11 |
| | | | | | | | | | | | | | | | | |
| CEM 2-5 | 2270S | 138W | 3867.0 | 118 | -45 | 48' | | | | | | | | | | |
| | -2270 | 136.6 | 3865.6 | | | | 450 | T1285 | 0'-2' | Hw | Aout | 0 | 0.110 | 3.77 | 0.04 | 1.37 |
| | -2270 | 135.2 | 3864.2 | | | | 451 | T1286 | 2'-4' | Hw | Aout | 0 | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2270 | 133.8 | 3862.8 | | | | 277 | T1111 | 4'-6' | Hw | Aout | Qfn | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2270 | 132.3 | 3861.3 | | | | 454 | T1288 | 6'-8' | Bx | Ain | 0 | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2270 | 130.9 | 3859.9 | | | | 278 | T1112 | 8'-10' | Vn | 0 | Qfn | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2270 | 129.5 | 3858.5 | | | | 455 | T1289 | 10'-12' | Bx | Ain | Qvg | 0.560 | 19.20 | 0.07 | 2.40 |
| | -2270 | 128.1 | 3857.1 | | | | 279 | T1113 | 12'-14' | Bx | QS | Qvg | 0.270 | 9.26 | 0.06 | 2.06 |
| | -2270 | 126.7 | 3855.7 | | | | 456 | T1290 | 14'-16' | Bx | QSP | Qvg | 0.030 | 1.03 | 0.12 | 4.11 |
| | -2270 | 125.3 | 3854.3 | | | | 457 | T1291 | 16'-18' | Fw | Ain | Qvg | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2270 | 123.9 | 3852.9 | | | | 458 | T1292 | 18'-20' | Fw | Aout | Qcmn | 0.040 | 1.37 | 0.11 | 3.77 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2270 | 122.4 | 3851.4 | | | | 459 | T1293 | 20'-22' | Fw | Pout | 0 | 0.040 | 1.37 | 0.03 | 1.03 |
| | -2270 | 121.0 | 3850.0 | | | | 460 | T1294 | 22'-24' | Fw | Pout | 0 | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2270 | 119.6 | 3848.6 | | | | 461 | T1295 | 24'-26' | Fw | Pout | 0 | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2270 | 118.2 | 3847.2 | | | | 462 | T1296 | 26'-28' | Fw | Pout | 0 | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2270 | 116.8 | 3845.8 | | | | 463 | T1297 | 28'-30' | Fw | Pout | 0 | 0.080 | 2.74 | 0.01 | 0.34 |
| | -2270 | 115.4 | 3844.4 | | | | 464 | T1298 | 30'-32' | Fw | Pout | 0 | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2270 | 114.0 | 3843.0 | | | | 465 | T1299 | 32'-34' | Fw | Pout | 0 | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2270 | 112.5 | 3841.5 | | | | 280 | T1114 | 34'-36' | Fw | Pout | 0 | 0.100 | 3.43 | 0.06 | 2.06 |
| | -2270 | 111.1 | 3840.1 | | | | 466 | T1300 | 36'-38' | Fw | Pout | 0 | 0.060 | 2.06 | 0.19 | 6.51 |
| | -2270 | 109.7 | 3838.7 | | | | 467 | T1301 | 38'-40' | Fw | Pout | 0 | 0.070 | 2.40 | 0.13 | 4.46 |
| | -2270 | 108.3 | 3837.3 | | | | 281 | T1115 | 40'-42' | Fw | Pout | 0 | 0.100 | 3.43 | 0.15 | 5.14 |
| | -2270 | 106.9 | 3835.9 | | | | 468 | T1302 | 42'-44' | Fw | Pout | 0 | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2270 | 105.5 | 3834.5 | | | | 469 | T1303 | 44'-46' | Fw | Pout | 0 | 0.090 | 3.09 | 0.07 | 2.40 |
| | -2270 | 104.1 | 3833.1 | | | | 282 | T1116 | 46'-48' | Fw | Pout | 0 | 0.070 | 2.40 | 0.08 | 2.74 |
| | | | | | | | | | | | | | | | | |
| CEM 2-6 | 2280S | 140W | 3866.0 | 118 | -45 | 36' | | | | | | | | | | |
| | -2280 | 138.6 | 3864.6 | | | | 283 | T1117 | 0'-2' | Hw | Pout | 0 | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2280 | 137.2 | 3863.2 | | | | 470 | T1304 | 2'-4' | Hw | Pout | 0 | 0.020 | 0.69 | 0.03 | 1.03 |
| | -2280 | 135.8 | 3861.8 | | | | 453 | T1287 | 4'-6' | HW | Pout | 0 | 0.060 | 2.06 | 0.08 | 2.74 |
| | -2280 | 134.3 | 3860.3 | | | | 284 | T1118 | 6'-8' | Hw | Pout | 0 | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2280 | 132.9 | 3858.9 | | | | 471 | T1305 | 8'-10' | Hw | Pout | 0 | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2280 | 131.5 | 3857.5 | | | | 285 | T1119 | 10'-12' | Hw | Pout | 0 | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2280 | 130.1 | 3856.1 | | | | 472 | T1306 | 12'-14' | Bx | QCS | Qvg | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2280 | 128.7 | 3854.7 | | | | 473 | T1307 | 14'-16' | Bx | QCSP | Qvg | 1.69 | 57.94 | 0.37 | 12.69 |
| | -2280 | 127.3 | 3853.3 | | | | 286 | T1120 | 16'-18' | Vn | 0 | Qfn | 0.950 | 32.57 | 0.17 | 5.83 |
| | -2280 | 125.9 | 3851.9 | | | | 287 | T1121 | 18'-20' | Vn | 0 | Qfn | 0.130 | 4.46 | 0.05 | 1.71 |
| | -2280 | 124.4 | 3850.4 | | | | 288 | T1122 | 20'-22' | Vn | 0 | Qfn | 0.210 | 7.20 | 0.06 | 2.06 |
| | -2280 | 123.0 | 3849.0 | | | | 474 | T1308 | 22'-24' | Fw | QCS | Qcmn | 0.070 | 2.40 | 0.04 | 1.37 |
| | -2280 | 121.6 | 3847.6 | | | | 475 | T1309 | 24'-26' | Bx | QC | Qvg | 0.050 | 1.71 | 0.06 | 2.06 |
| | -2280 | 120.2 | 3846.2 | | | | 289 | T1123 | 26'-28' | Fw | Aout | 0 | 0.130 | 4.46 | 0.09 | 3.09 |
| | -2280 | 118.8 | 3844.8 | | | | 476 | T1310 | 28'-30' | Fw | Aout | 0 | 0.080 | 2.74 | 0.06 | 2.06 |
| | -2280 | 117.4 | 3843.4 | | | | 290 | T1124 | 30'-32' | Fw | Pout | 0 | 0.360 | 12.34 | 0.13 | 4.46 |
| | -2280 | 116.0 | 3842.0 | | | | 477 | T1311 | 32'-34' | Fw | Pout | 0 | 0.080 | 2.74 | 0.15 | 5.14 |
| | -2280 | 114.5 | 3840.5 | | | | 291 | T1125 | 34'-36' | Fw | Pout | 0 | 0.130 | 4.46 | 0.07 | 2.40 |
| | | | | | | | | | | | | | | | | |
| CEM 2-7 | 2290S | 144W | 3862.0 | 118 | -45 | 50' | | | | | | | | | | |
| | -2290 | 142.6 | 3860.6 | | | | 292 | T1126 | 0'-2' | Hw | Pout | 0 | 0.010 | 0.34 | 0.01 | 0.34 |
| | -2290 | 141.2 | 3859.2 | | | | 478 | T1312 | 2'-4' | Hw | Pout | 0 | 0.030 | 1.03 | 0.01 | 0.34 |
| | -2290 | 139.8 | 3857.8 | | | | 479 | T1313 | 6'-8' | Hw | Pout | 0 | 0.040 | 1.37 | 0.01 | 0.34 |
| | -2290 | 138.3 | 3856.3 | | | | 480 | T1314 | 8'-10' | Hw | Pout | 0 | 0.010 | 0.34 | 0.01 | 0.34 |
| | -2290 | 136.9 | 3854.9 | | | | 293 | T1127 | 10'-12' | Hw | Pout | 0 | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2290 | 135.5 | 3853.5 | | | | 294 | T1128 | 12'-14' | Hw | Pout | 0 | 0.030 | 1.03 | 0.09 | 3.09 |
| | -2290 | 134.1 | 3852.1 | | | | 481 | T1315 | 14'-16' | Bx | QSP | Qvg | 0.340 | 11.66 | 0.01 | 0.34 |
| | -2290 | 132.7 | 3850.7 | | | | 295 | T1129 | 16'-18' | Bx | QCP | Qvg | 0.310 | 10.63 | 0.17 | 5.83 |
| | -2290 | 131.3 | 3849.3 | | | | 296 | T1130 | 18'-20' | Bx | QCP | Qfn | 0.400 | 13.71 | 0.29 | 9.94 |
| | -2290 | 129.9 | 3847.9 | | | | 298 | T1132 | 20'-22' | Bx | QCS | Qvg | 0.140 | 4.80 | 0.04 | 1.37 |
| | -2290 | 128.4 | 3846.4 | | | | 297 | T1131 | 22'-24' | Bx | QC | 0 | 0.330 | 11.31 | 0.16 | 5.49 |
| | -2290 | 127.0 | 3845.0 | | | | 482 | T1316 | 24'-26' | Fw | Aout | Qvgp | 0.070 | 2.40 | 0.04 | 1.37 |
| | -2290 | 125.6 | 3843.6 | | | | 483 | T1317 | 26'-28' | Fw | Pout | Qvg | 0.130 | 4.46 | 0.01 | 0.34 |
| | -2290 | 124.2 | 3842.2 | | | | 299 | T1133 | 28'-30' | Fw | Aout | Qvg | 0.200 | 6.86 | 0.08 | 2.74 |
| | -2290 | 122.8 | 3840.8 | | | | 484 | T1318 | 30'-32' | Fw | Aout | Qvgp | 0.040 | 1.37 | 0.01 | 0.34 |
| | -2290 | 121.4 | 3839.4 | | | | 300 | T1134 | 32'-34' | Fw | Aout | Qvgp | 0.430 | 14.74 | 0.14 | 4.80 |
| | -2290 | 120.0 | 3838.0 | | | | 485 | T1319 | 34'-36' | Fw | Pout | 0 | 0.060 | 2.06 | 0.01 | 0.34 |
| | -2290 | 118.5 | 3836.5 | | | | 301 | T1135 | 36'-38' | Fw | Pout | 0 | 0.060 | 2.06 | 0.03 | 1.03 |
| | -2290 | 117.1 | 3835.1 | | | | 486 | T1320 | 38'-40' | Fw | Pout | 0 | 0.040 | 1.37 | 0.01 | 0.34 |
| | -2290 | 115.7 | 3833.7 | | | | 302 | T1136 | 40'-42' | Fw | Pout | 0 | 0.030 | 1.03 | 0.06 | 2.06 |
| | -2290 | 114.3 | 3832.3 | | | | 487 | T1321 | 42'-44' | Fw | Pout | Qvgp | 0.070 | 2.40 | 0.04 | 1.37 |
| | -2290 | 112.9 | 3830.9 | | | | 303 | T1137 | 44'-46' | Fw | Pout | 0 | 0.030 | 1.03 | 0.96 | 32.91 |
| | -2290 | 111.5 | 3829.5 | | | | 488 | T1322 | 46'-48' | Fw | Pout | 0 | 0.100 | 3.43 | 0.00 | 0.00 |
| | -2290 | 110.1 | 3828.1 | | | | 489 | T1323 | 48'-50' | Fw | Pout | 0 | 0.010 | 0.34 | 0.00 | 0.00 |
| | | | | | | | | | | | | | | | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM 2-12 | 2291S | 200W | 3870.0 | 118 | -45 | 50' | | | | | | | | | | |
| | -2291 | 198.6 | 3868.6 | | | | ns | | | | | | | | | |
| | -2291 | 197.2 | 3867.2 | | | | 914 | T1747 | 2'-4' | Hw | Pout | 0 | 0.040 | 1.37 | 0.07 | 2.40 |
| | -2291 | 195.8 | 3865.8 | | | | 915 | T1748 | 4'-6' | Hw | Pout | 0 | 0.070 | 2.40 | 0.04 | 1.37 |
| | -2291 | 194.3 | 3864.3 | | | | 916 | T1749 | 6'-8' | Hw | Pout | Qfn | 0.100 | 3.43 | 0.07 | 2.40 |
| | -2291 | 192.9 | 3862.9 | | | | 917 | T1750 | 8'-10' | Hw | Aout | 0 | 0.100 | 3.43 | 0.06 | 2.06 |
| | -2291 | 191.5 | 3861.5 | | | | 918 | T1751 | 10'-12' | Hw | Aout | 0 | 0.080 | 2.74 | 0.05 | 1.71 |
| | -2291 | 190.1 | 3860.1 | | | | 919 | T1752 | 12'-14' | Hw | Pin | Qvg | 0.080 | 2.74 | 0.05 | 1.71 |
| | -2291 | 188.7 | 3858.7 | | | | 920 | T1753 | 14'-16' | Hw | Pin | Qvg | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2291 | 187.3 | 3857.3 | | | | 921 | T1754 | 16'-18' | Bx | QCP | Qvg | 0.200 | 6.86 | 0.06 | 2.06 |
| | -2291 | 185.9 | 3855.9 | | | | 922 | T1755 | 18'-20' | Bx | QCP | Qvg | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2291 | 184.4 | 3854.4 | | | | 923 | T1756 | 20'-22' | Hw | Aout | 0 | 0.070 | 2.40 | 0.04 | 1.37 |
| | -2291 | 183.0 | 3853.0 | | | | 924 | T1757 | 22'-24' | Hw | Aout | 0 | 0.060 | 2.06 | 0.03 | 1.03 |
| | -2291 | 181.6 | 3851.6 | | | | 925 | T1758 | 24'-26' | Hw | Aout | 0 | 0.150 | 5.14 | 0.09 | 3.09 |
| | -2291 | 180.2 | 3850.2 | | | | 926 | T1759 | 26'-28' | Hw | Aout | Qfn | 0.110 | 3.77 | 0.06 | 2.06 |
| | -2291 | 178.8 | 3848.8 | | | | 927 | T1760 | 28'-30' | Hw | Aout | Qvg | 0.220 | 7.54 | 0.13 | 4.46 |
| | -2291 | 177.4 | 3847.4 | | | | 928 | T1761 | 30'-32' | Hw | Aout | Qvg | 0.340 | 11.66 | 0.16 | 5.49 |
| | -2291 | 176.0 | 3846.0 | | | | 929 | T1762 | 32'-34' | Bx | QCSP | Qvg | 0.240 | 8.23 | 0.11 | 3.77 |
| | -2291 | 174.5 | 3844.5 | | | | 930 | T1763 | 34'-36' | Bx | QCSP | Qvg | 0.170 | 5.83 | 0.10 | 3.43 |
| | -2291 | 173.1 | 3843.1 | | | | 931 | T1764 | 36'-38' | Bx | QC | Qvg | 0.150 | 5.14 | 0.05 | 1.71 |
| | -2291 | 171.7 | 3841.7 | | | | 932 | T1765 | 38'-40' | Bx | QC | Qvgp | 0.170 | 5.83 | 0.10 | 3.43 |
| | -2291 | 170.3 | 3840.3 | | | | 933 | T1766 | 40'-42' | Hw | Aout | Qvg | 0.110 | 3.77 | 0.10 | 3.43 |
| | -2291 | 168.9 | 3838.9 | | | | 934 | T1767 | 42'-44' | Hw | Aout | 0 | 0.070 | 2.40 | 0.09 | 3.09 |
| | -2291 | 167.5 | 3837.5 | | | | 935 | T1768 | 44'-46' | Hw | Aout | 0 | 0.060 | 2.06 | 0.07 | 2.40 |
| | -2291 | 166.1 | 3836.1 | | | | 936 | T1769 | 46'-48' | Hw | Aout | Qvg | 0.100 | 3.43 | 0.06 | 2.06 |
| | -2291 | 164.7 | 3834.6 | | | | 937 | T1770 | 48'-50' | Hw | Pout | Qvg | 0.270 | 9.26 | 0.08 | 2.74 |
| | | | | | | | | | | | | | | | | |
| CEM 2-8 | 2305S | 150W | 3860.0 | 118 | -45 | 30' | | | | | | | | | | |
| | -2305 | 148.6 | 3858.6 | | | | 304 | T1138 | 0'-2' | Hw | Pout | 0 | | | | |
| | -2305 | 147.2 | 3857.2 | | | | 305 | T1139 | 2'-4' | Hw | Pout | 0 | 0.100 | 3.43 | 0.07 | 2.40 |
| | -2305 | 145.8 | 3855.8 | | | | 490 | T1324 | 4'-6' | Hw | Pout | 0 | | | | |
| | -2305 | 144.3 | 3854.3 | | | | 306 | T1140 | 6'-8' | Hw | Pout | 0 | | | | |
| | -2305 | 142.9 | 3852.9 | | | | 491 | T1325 | 8'-10' | Bx | QSP | Qvgp | 0.110 | 3.77 | 0.04 | 1.37 |
| | -2305 | 141.5 | 3851.5 | | | | 307 | T1141 | 10'-12' | Bx | QSP | Qvgp | 0.050 | 1.71 | 0.02 | 0.69 |
| | -2305 | 140.1 | 3850.1 | | | | 308 | T1142 | 12'-14' | Bx | QCSP | Qvg | 0.800 | 27.43 | 0.22 | 7.54 |
| | -2305 | 138.7 | 3848.7 | | | | 309 | T1143 | 14'-16' | Bx | QCP | Qvg | 0.320 | 10.97 | 0.13 | 4.46 |
| | -2305 | 137.3 | 3847.3 | | | | 492 | T1326 | 16'-18' | Bx | QC | Qvgp | 0.520 | 17.83 | 0.10 | 3.43 |
| | -2305 | 135.9 | 3845.9 | | | | 493 | T1327 | 18'-20' | Bx | QCS | Qvg | 0.130 | 4.46 | 0.11 | 3.77 |
| | -2305 | 134.4 | 3844.4 | | | | 494 | T1328 | 20'-22' | Fw | Pin | Qvg | 0.100 | 3.43 | 0.05 | 1.71 |
| | -2305 | 133.0 | 3843.0 | | | | 310 | T1144 | 22'-24' | Fw | Aout | Qvg | | | | |
| | -2305 | 131.6 | 3841.6 | | | | 311 | T1145 | 24'-26' | Fw | Aout | Qvg | 0.080 | 2.74 | 0.02 | 0.69 |
| | -2305 | 130.2 | 3840.2 | | | | 312 | T1146 | 26'-28' | Fw | Aout | FeO | 0.160 | 5.49 | 0.03 | 1.03 |
| | -2305 | 128.8 | 3838.8 | | | | 313 | T1147 | 28'-30' | Fw | Aout | Qvg | 0.110 | 3.77 | 0.03 | 1.03 |
| | | | | | | | | | | | | | | | | |
| CEM 2-13 | 2320S | 70W | 3894.0 | 118 | -45 | 50' | | | | | | | | | | |
| | -2320 | 68.6 | 3892.6 | | | | 1317 | T2150 | 0'-2' | | | | 0.030 | 1.03 | 0.01 | 0.34 |
| | -2320 | 67.2 | 3891.2 | | | | 1318 | T2151 | 2'-4' | | | | 0.010 | 0.34 | 0.03 | 1.03 |
| | -2320 | 65.8 | 3889.8 | | | | 1319 | T2152 | 4'-6' | | | | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2320 | 64.3 | 3888.3 | | | | 1320 | T2153 | 6'-8' | | | | 0.020 | 0.69 | 0.00 | 0.00 |
| | -2320 | 62.9 | 3886.9 | | | | 1321 | T2154 | 8'-10' | | | | 0.030 | 1.03 | 0.09 | 3.09 |
| | -2320 | 61.5 | 3885.5 | | | | 1.322 | T2155 | 10'-12' | | | | 0.030 | 1.03 | 0.11 | 3.77 |
| | -2320 | 60.1 | 3884.1 | | | | 1323 | T2156 | 12'-14' | | | | 0.030 | 1.03 | 0.11 | 3.77 |
| | -2320 | 58.7 | 3882.7 | | | | 1324 | T2157 | 14'-16' | | | | 0.030 | 1.03 | 0.11 | 3.77 |
| | -2320 | 57.3 | 3881.3 | | | | 1325 | T2158 | 16'-18' | | | | 0.010 | 0.34 | 0.10 | 3.43 |
| | -2320 | 55.9 | 3879.9 | | | | 1326 | T2159 | 18'-20' | | | | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2320 | 54.4 | 3878.4 | | | | 1327 | T2160 | 20'-22' | | | | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2320 | 53.0 | 3877.0 | | | | 1328 | T2161 | 22'-24' | | | | 0.060 | 2.06 | 0.13 | 4.46 |
| | -2320 | 51.6 | 3875.6 | | | | 1329 | T2162 | 24'-26' | | | | 0.120 | 4.11 | 0.12 | 4.11 |
| | -2320 | 50.2 | 3874.2 | | | | 1330 | T2163 | 26'-28' | | | | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2320 | 48.8 | 3872.8 | | | | 1331 | T2164 | 28'-30' | | | | 0.020 | 0.69 | 0.03 | 1.03 |
| | -2320 | 47.4 | 3871.4 | | | | 1332 | T2165 | 30'-32' | | | | 0.040 | 1.37 | 0.12 | 4.11 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2320 | 46.0 | 3870.0 | | | | 1333 | T2166 | 32'-34' | | | | 0.020 | 0.69 | 0.05 | 1.71 |
| | -2320 | 44.5 | 3868.5 | | | | 1334 | T2167 | 34'-36' | | | | 0.020 | 0.69 | 0.03 | 1.03 |
| | -2320 | 43.1 | 3867.1 | | | | 1335 | T2168 | 36'-38' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2320 | 41.7 | 3865.7 | | | | 1336 | T2169 | 38'-40' | | | | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2320 | 40.3 | 3864.3 | | | | 1337 | T2170 | 40'-42' | | | | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2320 | 38.9 | 3862.9 | | | | 1338 | T2171 | 42'-44' | | | | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2320 | 37.5 | 3861.5 | | | | 1339 | T2172 | 44'-46' | | | | 0.030 | 1.03 | 0.13 | 4.46 |
| | -2320 | 36.1 | 3860.1 | | | | 1340 | T2173 | 46'-48' | | | | 0.030 | 1.03 | 0.09 | 3.09 |
| | -2320 | 34.7 | 3858.6 | | | | 1341 | T2174 | 48'-50' | | | | 0.010 | 0.34 | 0.10 | 3.43 |
| | | | | | | | | | | | | | | | | |
| CEM 2-9 | 2320S | 164W | 3858.0 | 118 | -45 | 40' | | | | | | | | | | |
| | -2320 | 162.6 | 3856.6 | | | | 495 | T1329 | 0'-2' | Hw | Pout | | 0.080 | 2.74 | 0.04 | 1.37 |
| | -2320 | 161.2 | 3855.2 | | | | 496 | T1330 | 2'-4' | Hw | Pout | | 0.110 | 3.77 | 0.04 | 1.37 |
| | -2320 | 159.8 | 3853.8 | | | | 497 | T1331 | 4'-6' | Hw | Pout | | 0.040 | 1.37 | 0.05 | 1.71 |
| | -2320 | 158.3 | 3852.3 | | | | 314 | T1148 | 6'-8' | Hw | Pout | | 0.020 | 0.69 | 0.03 | 1.03 |
| | -2320 | 156.9 | 3850.9 | | | | 498 | T1'332 | 8'-10' | Hw | Pin | 0 | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2320 | 155.5 | 3849.5 | | | | 499 | T1333 | 10'-12' | Hw | Pin | Qvgp | 0.040 | 1.37 | 0.03 | 1.03 |
| | -2320 | 154.1 | 3848.1 | | | | 500 | T1334 | 12'-14' | Hw | QC | Qvg | 0.110 | 3.77 | 0.04 | 1.37 |
| | -2320 | 152.7 | 3846.7 | | | | 501 | T1335 | 14'-16' | Bx | QC | 0 | 0.130 | 4.46 | 0.04 | 1.37 |
| | -2320 | 151.3 | 3845.3 | | | | 315 | T1149 | 16'-18' | Bx | QSP | Qvg | 0.090 | 3.09 | 0.04 | 1.37 |
| | -2320 | 149.9 | 3843.9 | | | | 316 | T1150 | 18'-20' | Bx | QS | Qvgp | 0.520 | 17.83 | 0.14 | 4.80 |
| | -2320 | 148.4 | 3842.4 | | | | 502 | T1336 | 20'-22' | Bx | QSP | Qvg | 0.200 | 6.86 | 0.05 | 1.71 |
| | -2320 | 147.0 | 3841.0 | | | | 503 | T1337 | 22'-24' | Bx | QC | Qvg | 0.070 | 2.40 | 0.05 | 1.71 |
| | -2320 | 145.6 | 3839.6 | | | | 504 | T1338 | 24'-26' | Bx | QCP | Qvg | 0.110 | 3.77 | 0.04 | 1.37 |
| | -2320 | 144.2 | 3838.2 | | | | 505 | T1339 | 26'-28' | Fw | Aout | Qvg | 0.090 | 3.09 | 0.04 | 1.37 |
| | -2320 | 142.8 | 3836.8 | | | | 317 | T1151 | 28'-30' | Fw | Aout | Qvg | 0.120 | 4.11 | 0.09 | 3.09 |
| | -2320 | 141.4 | 3835.4 | | | | 506 | T1340 | 30'-32' | Fw | Aout | 0 | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2320 | 140.0 | 3834.0 | | | | 318 | T1152 | 32'-34' | Fw | Aout | 0 | 0.080 | 2.74 | 0.05 | 1.71 |
| | -2320 | 138.5 | 3832.5 | | | | 507 | T1341 | 34'-36' | Fw | Pout | 0 | 0.050 | 1.71 | 0.02 | 0.69 |
| | -2320 | 137.1 | 3831.1 | | | | 508 | T1342 | 36'-38' | Fw | Pout | 0 | 0.090 | 3.09 | 0.01 | 0.34 |
| | -2320 | 135.7 | 3829.7 | | | | 319 | T1153 | 38'-40' | Fw | Pout | 0 | 0.030 | 1.03 | 0.01 | 0.34 |
| | | | | | | | | | | | | | | | | |
| CEM 2-10 | 2340S | 170W | 3874.0 | 118 | -45 | 40' | | | | | | | | | | |
| | -2340 | 168.6 | 3872.6 | | | | 320 | T1154 | 0'-2' | Hw | Pout | 0 | 0.030 | 1.03 | 0.09 | 3.09 |
| | -2340 | 167.2 | 3871.2 | | | | 509 | T1343 | 2'-4' | Hw | Pout | Qvg | 0.010 | 0.34 | 0.09 | 3.09 |
| | -2340 | 165.8 | 3869.8 | | | | 321 | T1155 | 4'-6' | Hw | Aout | Qvg | 0.080 | 2.74 | 0.11 | 3.77 |
| | -2340 | 164.3 | 3868.3 | | | | 322 | T1156 | 6'-8' | Bx | QS | Qcmn | 0.080 | 2.74 | 0.02 | 0.69 |
| | -2340 | 162.9 | 3866.9 | | | | 510 | T1344 | 8'-10' | Bx | QSP | Qvg | 0.050 | 1.71 | 0.10 | 3.43 |
| | -2340 | 161.5 | 3865.5 | | | | 511 | T1345 | 10'-12' | Bx | QC | Qcmn | 0.100 | 3.43 | 0.13 | 4.46 |
| | -2340 | 160.1 | 3864.1 | | | | 512 | T1S46 | 12'-14' | Bx | QSP | Qvg | 0.200 | 6.86 | 0.05 | 1.71 |
| | -2340 | 158.7 | 3862.7 | | | | 323 | T1157 | 14'-16' | Fw | QS | Qvg | 0.080 | 2.74 | 0.09 | 3.09 |
| | -2340 | 157.3 | 3861.3 | | | | 513 | T1347 | 16'-18' | Fw | A in | 0 | 0.070 | 2.40 | *0.02* | 0.69 |
| | -2340 | 155.9 | 3859.9 | | | | 514 | T1348 | 18'-20' | Fw | Aout | Qvg | 0.060 | 2.06 | 0.06 | 2.06 |
| | -2340 | 154.4 | 3858.4 | | | | 515 | T1349 | 20'-22' | Fw | Aout | Qvg | 0.070 | 2.40 | 0.02 | 0.69 |
| | -2340 | 153.0 | 3857.0 | | | | 516 | T1350 | 22'-24' | Fw | Aout | Qvg | 0.090 | 3.09 | 0.02 | 0.69 |
| | -2340 | 151.6 | 3855.6 | | | | 324 | T1158 | 24'-26' | Fw | Aout | Qvg | 0.070 | 2.40 | 0.05 | 1.71 |
| | -2340 | 150.2 | 3854.2 | | | | 325 | T1159 | 26'-28' | Fw | Aout | Qvg | 0.040 | 1.37 | 0.05 | 1.71 |
| | -2340 | 148.8 | 3852.8 | | | | 517 | T1351 | 28'-30' | Fw | Aout | 0 | 0.030 | 1.03 | 0.26 | 8.91 |
| | -2340 | 147.4 | 3851.4 | | | | 518 | T1352 | 30'-32' | Fw | Aout | 0 | 0.090 | 3.09 | 0.10 | 3.43 |
| | -2340 | 146.0 | 3850.0 | | | | 326 | T1160 | 32'-34' | Fw | Aout | 0 | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2340 | 144.5 | 3848.5 | | | | 327 | T1161 | 34'-36' | Fw | Aout | 0 | 0.100 | 3.43 | 0.11 | 3.77 |
| | -2340 | 143.1 | 3847.1 | | | | 519 | T1353 | 36'-38' | Fw | Aout | 0 | 0.050 | 1.71 | 0.02 | 0.69 |
| | -2340 | 141.7 | 3845.7 | | | | 328 | T1162 | 38'-40' | Fw | Aout | 0 | 0.030 | 1.03 | 0.03 | 1.03 |
| | | | | | | | | | | | | | | | | |
| CEM 2-11 | 2384S | 210W | 3856.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2384 | 208.6 | 3854.6 | | | | 773 | T1606 | 2'-4' | Hw | | | 0.050 | 1.71 | 0.02 | 0.69 |
| | -2384 | 207.2 | 3853.2 | | | | 774 | T1607 | 4'-6' | Hw | | | 0.220 | 7.54 | 0.16 | 5.49 |
| | -2384 | 205.8 | 3851.8 | | | | 775 | T1608 | 6'-8' | Hw | Aout | Qvgp | 0.160 | 5.49 | 0.14 | 4.80 |
| | -2384 | 204.3 | 3850.3 | | | | 776 | T1609 | 8'-10' | Bx | QSP | Qvg | 0.060 | 2.06 | 0.07 | 2.40 |
| | -2384 | 202.9 | 3848.9 | | | | 777 | T1610 | 10'-12' | Bx | QSP | Qvg | 0.200 | 6.86 | 0.25 | 8.57 |
| | -2384 | 201.5 | 3847.5 | | | | 778 | T1611 | 12'-14' | Bx | QSP | Qvg | 0.040 | 1.37 | 0.05 | 1.71 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2384 | 200.1 | 3846.1 | | | | 779 | T1612 | 14'-16' | Fw | Pout | | 0.080 | 2.74 | 0.08 | 2.74 |
| | -2384 | 198.7 | 3844.7 | | | | 780 | T1613 | 16'-18' | Fw | Pout | 0 | 0.200 | 6.86 | 0.44 | 15.09 |
| | -2384 | 197.3 | 3843.3 | | | | 781 | T1614 | 18'-20' | Fw | Pout | 0 | 0.080 | 2.74 | 0.07 | 2.40 |
| | -2384 | 195.9 | 3841.9 | | | | 782 | T1615 | 20'-22' | Fw | Pout | 0 | 0.050 | 1.71 | 0.08 | 2.74 |
| | -2384 | 194.4 | 3840.4 | | | | 783 | T1616 | 22'-24' | Fw | Pout | 0 | 0.200 | 6.86 | 0.10 | 3.43 |
| | -2384 | 193.0 | 3839.0 | | | | 784 | T1617 | 24'-26' | Fw | Pout | 0 | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2384 | 191.6 | 3837.6 | | | | 785 | T1618 | 26'-28' | Fw | Pout | 0 | ns | | ns | |
| | -2384 | 190.2 | 3836.2 | | | | 786 | T1619 | 28'-30' | Fw | Pout | 0 | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2384 | 188.8 | 3834.8 | | | | 787 | T1620 | 30'-32' | Fw | Pout | 0 | 0.090 | 3.09 | 0.05 | 1.71 |
| | -2384 | 187.4 | 3833.4 | | | | 788 | T1621 | 32'-34' | Fw | Pout | 0 | 0.060 | 2.06 | 0.06 | 2.06 |
| | -2384 | 186.0 | 3832.0 | | | | 789 | T1621 | 34'-36' | Fw | Pout | 0 | 0.090 | 3.09 | 0.05 | 1.71 |
| | -2384 | 184.5 | 3830.5 | | | | 790 | T1623 | 36'-38' | Fw | Pout | 0 | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2384 | 183.1 | 3829.1 | | | | 791 | T1624 | 38'-40' | Fw | Pout | 0 | 0.030 | 1.03 | 0.02 | 0.69 |
| | -2384 | 181.7 | 3827.7 | | | | 792 | T1625 | 40'-42' | Fw | Pout | 0 | 0.060 | 2.06 | 0.03 | 1.03 |
| | -2384 | 180.3 | 3826.3 | | | | 793 | T1626 | 42'-44' | Fw | Pout | 0 | 0.070 | 2.40 | 0.03 | 1.03 |
| | -2384 | 178.9 | 3824.9 | | | | 794 | T1627 | 44'-46' | Fw | Pout | 0 | 0.060 | 2.06 | 0.05 | 1.71 |
| | -2384 | 177.5 | 3823.5 | | | | 795 | T1628 | 46'-48' | Fw | Pout | 0 | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2384 | 176.1 | 3822.1 | | | | 796 | T1629 | 48'-50' | Fw | Pout | 0 | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2384 | 174.7 | 3820.6 | | | | 797 | T1630 | 50'-52' | Fw | Pout | 0 | 0.040 | 1.37 | 0.05 | 1.71 |
| | -2384 | 173.2 | 3819.2 | | | | 798 | T1631 | 52'-54' | Fw | Pout | 0 | 0.050 | 1.71 | 0.04 | 1.37 |
| | -2384 | 171.8 | 3817.8 | | | | 799 | T1632 | 54'-56' | Fw | Pout | 0 | 0.050 | 1.71 | 0.09 | 3.09 |
| | -2384 | 170.4 | 3816.4 | | | | 800 | T1633 | 56'-58' | Fw | Pout | 0 | 0.070 | 2.40 | 0.05 | 1.71 |
| | -2384 | 169.0 | 3815.0 | | | | 801 | T1634 | 58'-60' | Fw | Pout | 0 | 0.040 | 1.37 | 0.04 | 1.37 |
| | | | | | | | | | | | | | | | | |
| CEM 2-14 | 2450S | 65W | 3865.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2450 | 63.6 | 3863.6 | | | | 1471 | T2282 | 0'-2' | | | | 0.030 | 1.03 | 0.02 | 0.69 |
| | -2450 | 62.2 | 3862.2 | | | | 1472 | T2283 | 2'-4' | | | | 0.010 | 0.34 | 0.10 | 3.43 |
| | -2450 | 60.8 | 3860.8 | | | | 1473 | T2284 | 4'-6' | | | | 0.040 | 1.37 | 0.08 | 2.74 |
| | -2450 | 59.3 | 3859.3 | | | | 1414 | T2285 | 6'-8' | | | | 0.050 | 1.71 | 0.08 | 2.74 |
| | -2450 | 57.9 | 3857.9 | | | | 1475 | T2286 | 8'-10' | | | | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2450 | 56.5 | 3856.5 | | | | 1476 | T2287 | 10'-12' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2450 | 55.1 | 3855.1 | | | | 1477 | T2288 | 12'-14' | | | | 0.040 | 1.37 | 0.11 | 3.77 |
| | -2450 | 53.7 | 3853.7 | | | | 1478 | T2289 | 14'-16' | | | | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2450 | 52.3 | 3852.3 | | | | 1479 | T2290 | 16'-18' | | | | 0.020 | 0.69 | 0.16 | 5.49 |
| | -2450 | 50.9 | 3850.9 | | | | 1480 | T2291 | 18'-20' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2450 | 49.4 | 3849.4 | | | | 1481 | T2292 | 20'-22' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2450 | 48.0 | 3848.0 | | | | 1482 | T2293 | 22'-24' | | | | 0.030 | 1.03 | 0.07 | 2.40 |
| | -2450 | 46.6 | 3846.6 | | | | 1483 | T2294 | 24'-26' | | | | 0.020 | 0.69 | 0.06 | 2.06 |
| | -2450 | 45.2 | 3845.2 | | | | 1484 | T2295 | 26'-28' | | | | 0.040 | 1.37 | 0.11 | 3.77 |
| | -2450 | 43.8 | 3843.8 | | | | 1485 | T2296 | 28'-30' | | | | 0.030 | 1.03 | 0.06 | 2.06 |
| | -2450 | 42.4 | 3842.4 | | | | 1486 | T2297 | 30'-32' | | | | 0.030 | 1.03 | 0.05 | 1.71 |
| | -2450 | 41.0 | 3841.0 | | | | 1487 | T2298 | 32'-34' | | | | 0.050 | 1.71 | 0.04 | 1.37 |
| | -2450 | 39.5 | 3839.5 | | | | 1488 | T2299 | 34'-36' | | | | 0.050 | 1.71 | 0.10 | 3.43 |
| | -2450 | 38.1 | 3838.1 | | | | 1489 | T2300 | 36'-38' | | | | 0.010 | 0.34 | 0.07 | 2.40 |
| | -2450 | 36.7 | 3836.7 | | | | 1490 | T2301 | 38'-40' | | | | 0.030 | 1.03 | 0.02 | 0.69 |
| | -2450 | 35.3 | 3835.3 | | | | 1491 | T2302 | 40'-42' | | | | 0.040 | 1.37 | 0.05 | 1.71 |
| | -2450 | 33.9 | 3833.9 | | | | 1492 | T2303 | 42'-44' | | | | 0.020 | 0.69 | 0.06 | 2.06 |
| | -2450 | 32.5 | 3832.5 | | | | 1493 | T2304 | 44'-46' | | | | 0.010 | 0.34 | 0.03 | 1.03 |
| | -2450 | 31.1 | 3831.1 | | | | 1494 | T2305 | 46'-48' | | | | 0.010 | 0.34 | 0.03 | 1.03 |
| | -2450 | 29.7 | 3829.6 | | | | 1495 | T2306 | 48'-50' | | | | 0.030 | 1.03 | 0.06 | 2.06 |
| | -2450 | 28.2 | 3828.2 | | | | 1496 | T2307 | 50'-52' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2450 | 26.8 | 3826.8 | | | | 1497 | T2308 | 52'-54' | | | | 0.020 | 0.69 | 0.05 | 1.71 |
| | -2450 | 25.4 | 3825.4 | | | | 1498 | T2309 | 54'-56' | | | | 0.040 | 1.37 | 0.02 | 0.69 |
| | -2450 | 24.0 | 3824.0 | | | | 1499 | T2310 | 56'-58' | | | | 0.030 | 1.03 | 0.09 | 3.09 |
| | -2450 | 22.6 | 3822.6 | | | | 1500 | T2311 | 58'-60' | | | | 0.010 | 0.34 | 0.09 | 3.09 |
| | | | | | | | | | | | | | | | | |
| CEM 2-18 | 2462S | 225W | 3845.0 | 118 | -45 | 62' | | | | | | | | | | |
| | -2462 | 223.6 | 3843.6 | | | | 2931 | T2721 | 6'-8' | Hw | 0 | 0 | 0.020 | 0.69 | | |
| | -2462 | 222.2 | 3842.2 | | | | 2932 | T2722 | 8'-10' | Hw | 0 | 0 | 0.020 | 0.69 | | |
| | -2462 | 220.8 | 3840.8 | | | | 2933 | T2723 | 10'-12' | Hw | 0 | 0 | 0.050 | 1.71 | | |
| | -2462 | 219.3 | 3839.3 | | | | 2934 | T2724 | 12'-14' | Hw | Pout | 0 | 0.020 | 0.69 | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2462 | 217.9 | 3837.9 | | | | 2935 | T2725 | 14'-16' | Hw | A in | 0 | 0.030 | 1.03 | | |
| | -2462 | 216.5 | 3836.5 | | | | 2936 | T2726 | 16'-18' | Bx | QS | Qvg | 0.020 | 0.69 | | |
| | -2462 | 215.1 | 3835.1 | | | | 2937 | T2727 | 18'-20' | Bx | A in | Qvg | 0.020 | 0.69 | | |
| | -2462 | 213.7 | 3833.7 | | | | 2938 | T2728 | 20'-22' | Fw | Pin | 0 | 0.030 | 1.03 | | |
| | -2462 | 212.3 | 3832.3 | | | | 2939 | T2729 | 22'-24' | Fw | Pin | 0 | 0.030 | 1.03 | | |
| | -2462 | 210.9 | 3830.9 | | | | 2940 | T2730 | 24'-26' | Fw | Pin | 0 | 0.020 | 0.69 | | |
| | -2462 | 209.4 | 3829.4 | | | | 2941 | T2731 | 26'-28' | Fw | Pin | 0 | 0.030 | 1.03 | | |
| | -2462 | 208.0 | 3828.0 | | | | 2942 | T2732 | 28'-30' | Fw | Pin | 0 | 0.010 | 0.34 | | |
| | -2462 | 206.6 | 3826.6 | | | | 2943 | T2733 | 30'-32' | Fw | Pout | 0 | 0.010 | 0.34 | | |
| | -2462 | 205.2 | 3825.2 | | | | 2944 | T2734 | 32'-34' | Fw | Pout | 0 | 0.010 | 0.34 | | |
| | -2462 | 203.8 | 3823.8 | | | | 2945 | T2735 | 34'-36' | Fw | Pout | 0 | 0.050 | 1.71 | | |
| | -2462 | 202.4 | 3822.4 | | | | 2946 | T2736 | 36'-38' | Fw | Pout | 0 | 0.030 | 1.03 | | |
| | -2462 | 201.0 | 3821.0 | | | | 2947 | T2737 | 38'-40' | Fw | Pout | 0 | 0.020 | 0.69 | | |
| | -2462 | 199.5 | 3819.5 | | | | 2948 | T2738 | 40'-42' | Fw | Pout | 0 | 0.020 | 0.69 | | |
| | -2462 | 198.1 | 3818.1 | | | | 2949 | T2739 | 42'-44' | Fw | Pout | 0 | 0.040 | 1.37 | | |
| | -2462 | 196.7 | 3816.7 | | | | 29 §0 | T2740 | 44'-46' | Fw | A in | 0 | 0.040 | 1.37 | | |
| | -2462 | 195.3 | 3815.3 | | | | 22951 | T2741 | 46'-48' | Fw | A in | 0 | 0.020 | 0.69 | | |
| | -2462 | 193.9 | 3813.9 | | | | 2952 | T2742 | 48'-50' | Fw | Pout | 0 | 0.010 | 0.34 | | |
| | -2462 | 192.5 | 3812.5 | | | | 2953 | T2743 | 50'-52' | Fw | Pout | 0 | 0.010 | 0.34 | | |
| | -2462 | 191.1 | 3811.1 | | | | 2954 | T2744 | 52'-54' | Fw | Pout | 0 | 0.010 | 0.34 | | |
| | -2462 | 189.7 | 3809.6 | | | | 2955 | T2745 | 54'-56' | Fw | Pout | 0 | 0.020 | 0.69 | | |
| | -2462 | 188.2 | 3808.2 | | | | 2956 | T2746 | 56'-58' | Fw | Pout | 0 | 0.030 | 1.03 | | |
| | -2462 | 186.8 | 3806.8 | | | | 2957 | T2747 | 58'-60' | Fw | Pout | 0 | 0.020 | 0.69 | | |
| | -2462 | 185.4 | 3805.4 | | | | 2958 | T2748 | 60'-62' | Fw | Pout | 0 | 0.020 | 0.69 | | |
| | | | | | | | | | | | | | | | | |
| CEM 2-19 | 2480S | 225W | 3849.0 | 118 | -45 | 50' | | | | | | | | | | |
| | -2480 | 223.6 | 3847.6 | | | | 2959 | T2749 | 4'-6' | | | | 0.040 | 1.37 | | |
| | -2480 | 222.2 | 3846.2 | | | | 2960 | T2750 | 6'-8' | | | | 0.030 | 1.03 | | |
| | -2480 | 220.8 | 3844.8 | | | | 2961 | T2751 | 8'-10' | | | | 0.010 | 0.34 | | |
| | -2480 | 219.3 | 3843.3 | | | | 2962 | T2752 | 10'-12' | | | | 0.010 | 0.34 | | |
| | -2480 | 217.9 | 3841.9 | | | | 2963 | T2753 | 12'-14' | | | | 0.010 | 0.34 | | |
| | -2480 | 216.5 | 3840.5 | | | | 2964 | T2754 | 14'-16' | | | | 0.010 | 0.34 | | |
| | -2480 | 215.1 | 3839.1 | | | | 2965 | T2755 | 16'-18' | | | | 0.010 | 0.34 | | |
| | -2480 | 213.7 | 3837.7 | | | | 2966 | T2756 | 18'-20' | | | | 0.010 | 0.34 | | |
| | -2480 | 212.3 | 3836.3 | | | | 2967 | T2757 | 20'-22' | | | | 0.010 | 0.34 | | |
| | -2480 | 210.9 | 3834.9 | | | | 2968 | T2758 | 22'-24' | | | | 0.010 | 0.34 | | |
| | -2480 | 209.4 | 3833.4 | | | | 2969 | T2759 | 24'-26' | | | | 0.010 | 0.34 | | |
| | -2480 | 208.0 | 3832.0 | | | | 2970 | T2760 | 26'-28' | | | | 0.010 | 0.34 | | |
| | -2480 | 206.6 | 3830.6 | | | | 22971 | T2761 | 28'-30' | | | | 0.010 | 0.34 | | |
| | -2480 | 205.2 | 3829.2 | | | | 2972 | T2762 | 30'-32' | | | | 0.010 | 0.34 | | |
| | -2480 | 203.8 | 3827.8 | | | | 2973 | T2963 | 32'-34' | | | | 0.010 | 0.34 | | |
| | -2480 | 202.4 | 3826.4 | | | | 2974 | T2964 | 34'-36' | | | | 0.010 | 0.34 | | |
| | -2480 | 201.0 | 3825.0 | | | | 2975 | T2765 | 36'-38' | | | | 0.010 | 0.34 | | |
| | -2480 | 199.5 | 3823.5 | | | | 2976 | T2766 | 38'-40' | | | | 0.010 | 0.34 | | |
| | -2480 | 198.1 | 3822.1 | | | | 2977 | T2767 | 40'-42' | | | | 0.020 | 0.69 | | |
| | -2480 | 196.7 | 3820.7 | | | | 2978 | T2768 | 42'-44' | | | | 0.020 | 0.69 | | |
| | -2480 | 195.3 | 3819.3 | | | | 2979 | T2769 | 46'-48' | | | | 0.050 | 1.71 | | |
| | -2480 | 193.9 | 3817.9 | | | | 2980 | T2770 | 48'-50' | | | | tr. | 0.00 | | |
| | | | | | | | | | | | | | | | | |
| CEM 2-15 | 2490S | 60W | 3864.0 | 118 | -45 | 80' | | | | | | | | | | |
| | -2490 | 58.6 | 3862.6 | | | | 1501 | T2312 | 0'-2' | | | | 0.090 | 3.09 | 0.12 | 4.11 |
| | -2490 | 57.2 | 3861.2 | | | | 1502 | T2313 | 2'-4' | | | | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2490 | 55.8 | 3859.8 | | | | 1503 | T2314 | 4'-6' | | | | 0.010 | 0.34 | 0.04 | 1.37 |
| | -2490 | 54.3 | 3858.3 | | | | 1504 | T2315 | 6'-8' | | | | 0.010 | 0.34 | 0.04 | 1.37 |
| | -2490 | 52.9 | 3856.9 | | | | 1505 | T2316 | 8'-10' | | | | 0.040 | 1.37 | 0.09 | 3.09 |
| | -2490 | 51.5 | 3855.5 | | | | 1506 | T2317 | 10'-12' | | | | 0.020 | 0.69 | 0.09 | 3.09 |
| | -2490 | 50.1 | 3854.1 | | | | 1507 | T2318 | 12'-14' | | | | 0.090 | 3.09 | 0.11 | 3.77 |
| | -2490 | 48.7 | 3852.7 | | | | 1508 | T2319 | 14'-16' | | | | 0.060 | 2.06 | 0.06 | 2.06 |
| | -2490 | 47.3 | 3851.3 | | | | 1509 | T2320 | 16'-18' | | | | 0.020 | 0.69 | 0.08 | 2.74 |
| | -2490 | 45.9 | 3849.9 | | | | 1510 | T2321 | 18'-20' | | | | 0.090 | 3.09 | 0.08 | 2.74 |
| | -2490 | 44.4 | 3848.4 | | | | 1511 | T2322 | 20'-22' | | | | 0.030 | 1.03 | 0.05 | 1.71 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2490 | 43.0 | 3847.0 | | | | 1512 | T2323 | 22'-24' | | | | 0.010 | 0.34 | 0.07 | 2.40 |
| | -2490 | 41.6 | 3845.6 | | | | 1513 | T2324 | 24'-26' | | | | tr. | 0.00 | 0.07 | 2.40 |
| | -2490 | 40.2 | 3844.2 | | | | 1514 | T2325 | 26'-28' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2490 | 38.8 | 3842.8 | | | | 1515 | T2326 | 28'-30' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2490 | 37.4 | 3841.4 | | | | 1516 | T2327 | 30'-32' | | | | 0.060 | 2.06 | 0.06 | 2.06 |
| | -2490 | 36.0 | 3840.0 | | | | 1517 | T2328 | 32'-34' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2490 | 34.5 | 3838.5 | | | | 1518 | T2329 | 34'-36' | | | | 0.040 | 1.37 | 0.1 | 3.43 |
| | -2490 | 33.1 | 3837.1 | | | | 1519 | T2330 | 36'-38' | | | | 0.010 | 0.34 | 0.07 | 2.40 |
| | -2490 | 31.7 | 3835.7 | | | | 1520 | T2331 | 38'-40' | | | | 0.030 | 1.03 | 0.09 | 3.09 |
| | -2490 | 30.3 | 3834.3 | | | | 1521 | T2332 | 40'-42' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2490 | 28.9 | 3832.9 | | | | 1522 | T2333 | 42'-44' | | | | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2490 | 27.5 | 3831.5 | | | | 1523 | T2334 | 44'-46' | | | | 0.020 | 0.69 | 0.09 | 3.09 |
| | -2490 | 26.1 | 3830.1 | | | | 1524 | T2335 | 46'-48' | | | | 0.010 | 0.34 | 0.03 | 1.03 |
| | -2490 | 24.7 | 3828.6 | | | | 1525 | T2336 | 48'-50' | | | | 0.020 | 0.69 | 0.09 | 3.09 |
| | -2490 | 23.2 | 3827.2 | | | | 1526 | T2337 | 50'-52' | | | | 0.020 | 0.69 | 0.03 | 1.03 |
| | -2490 | 21.8 | 3825.8 | | | | 1527 | T2338 | 52'-54' | | | | 0.010 | 0.34 | 0.06 | 2.06 |
| | -2490 | 20.4 | 3824.4 | | | | 1528 | T2339 | 54'-56' | | | | 0.040 | 1.37 | 0.05 | 1.71 |
| | -2490 | 19.0 | 3823.0 | | | | 1529 | T2340 | 56'-58' | | | | 0.010 | 0.34 | 0.08 | 2.74 |
| | -2490 | 17.6 | 3821.6 | | | | 1530 | T2341 | 58'-60' | | | | 0.020 | 0.69 | 0.06 | 2.06 |
| | -2490 | 16.2 | 3820.2 | | | | 1531 | T2342 | 60'-62' | | | | 0.010 | 0.34 | 0.07 | 2.40 |
| | -2490 | 14.8 | 3818.8 | | | | 1532 | T2343 | 62'-64' | | | | 0.040 | 1.37 | 0.03 | 1.03 |
| | -2490 | 13.3 | 3817.3 | | | | 1533 | T2344 | 64'-66' | | | | 0.030 | 1.03 | 0.05 | 1.71 |
| | -2490 | 11.9 | 3815.9 | | | | 1534 | T2345 | 66'-68' | | | | 0.030 | 1.03 | 0.1 | 3.43 |
| | -2490 | 10.5 | 3814.5 | | | | 1535 | T2346 | 68'-70' | | | | 0.040 | 1.37 | 0.06 | 2.06 |
| | -2490 | 9.1 | 3813.1 | | | | 1536 | T2347 | 70'-72' | | | | 0.010 | 0.34 | 0.06 | 2.06 |
| | -2490 | 7.7 | 3811.7 | | | | 1537 | T2348 | 72'-74' | | | | 0.010 | 0.34 | 0.07 | 2.40 |
| | -2490 | 6.3 | 3810.3 | | | | 1538 | T2349 | 74'-76' | | | | 0.030 | 1.03 | 0.07 | 2.40 |
| | -2490 | 4.9 | 3808.9 | | | | 1539 | T2350 | 76'-78' | | | | 0.040 | 1.37 | 0.09 | 3.09 |
| | -2490 | 3.4 | 3807.4 | | | | 1540 | T2351 | 78'-80' | | | | 0.020 | 0.69 | 0.01 | 0.34 |
| | | | | | | | | | | | | | | | | |
| CEM 2-16 | 2500S | 100W | 3851.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2500 | 98.6 | 3849.6 | | | | 1541 | T2352 | 0'-2' | | | | 0.010 | 0.34 | 0.05 | 1.71 |
| | -2500 | 97.2 | 3848.2 | | | | 1542 | T2353 | 2'-4' | | | | 0.020 | 0.69 | 0.06 | 2.06 |
| | -2500 | 95.8 | 3846.8 | | | | 1543 | T2354 | 4'-6' | | | | 0.030 | 1.03 | 0.06 | 2.06 |
| | -2500 | 94.3 | 3845.3 | | | | 1544 | T2355 | 6'-8' | | | | 0.020 | 0.69 | 0.09 | 3.09 |
| | -2500 | 92.9 | 3843.9 | | | | 1545 | T2356 | 8'-10' | | | | 0.030 | 1.03 | 0.05 | 1.71 |
| | -2500 | 91.5 | 3842.5 | | | | 1546 | T2357 | 10'-12' | | | | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2500 | 90.1 | 3841.1 | | | | 1547 | T2358 | 12'-14' | | | | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2500 | 88.7 | 3839.7 | | | | 1548 | T2359 | 14'-16' | | | | 0.030 | 1.03 | 0.06 | 2.06 |
| | -2500 | 87.3 | 3838.3 | | | | 1549 | T2360 | 16'-18' | | | | 0.020 | 0.69 | 0.07 | 2.40 |
| | -2500 | 85.9 | 3836.9 | | | | 1550 | i2361 | 18'-20' | | | | 0.010 | 0.34 | 0.01 | 0.34 |
| | -2500 | 84.4 | 3835.4 | | | | 1551 | T2362 | 20'-22' | | | | 0.020 | 0.69 | 0.10 | 3.43 |
| | -2500 | 83.0 | 3834.0 | | | | 1552 | T2363 | 22'-24' | | | | 0.080 | 2.74 | 0.05 | 1.71 |
| | -2500 | 81.6 | 3832.6 | | | | 1553 | T2364 | 24'-26' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2500 | 80.2 | 3831.2 | | | | 1554 | T2365 | 26'-28' | | | | 0.090 | 3.09 | 0.05 | 1.71 |
| | -2500 | 78.8 | 3829.8 | | | | 1555 | T2366 | 28'-30' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2500 | 77.4 | 3828.4 | | | | 1556 | T2367 | 30'-32' | | | | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2500 | 76.0 | 3827.0 | | | | 1557 | T2368 | 32'-34' | | | | 0.010 | 0.34 | 0.06 | 2.06 |
| | -2500 | 74.5 | 3825.5 | | | | 1558 | T2369 | 34'-36' | | | | 0.020 | 0.69 | 0.05 | 1.71 |
| | -2500 | 73.1 | 3824.1 | | | | 1559 | T2370 | 36'-38' | | | | 0.010 | 0.34 | 0.06 | 2.06 |
| | -2500 | 71.7 | 3822.7 | | | | 1560 | T2371 | 38'-40' | | | | 0.010 | 0.34 | 0.04 | 1.37 |
| | -2500 | 70.3 | 3821.3 | | | | 1561 | T2372 | 40'-42' | | | | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2500 | 68.9 | 3819.9 | | | | 1562 | T2373 | 42'-44' | | | | 0.050 | 1.71 | 0.03 | 1.03 |
| | -2500 | 67.5 | 3818.5 | | | | 1563 | T2374 | 44'-46' | | | | 0.040 | 1.37 | 0.06 | 2.06 |
| | -2500 | 66.1 | 3817.1 | | | | 1564 | T2375 | 46'-48' | | | | 0.010 | 0.34 | 0.09 | 3.09 |
| | -2500 | 64.7 | 3815.6 | | | | 1565 | T2376 | 48'-50' | | | | 0.030 | 1.03 | 0.08 | 2.74 |
| | -2500 | 63.2 | 3814.2 | | | | 1566 | T2377 | 50'-52' | | | | 0.010 | 0.34 | 0.08 | 2.74 |
| | -2500 | 61.8 | 3812.8 | | | | 1567 | T2378 | 52'-54' | | | | 0.010 | 0.34 | 0.05 | 1.71 |
| | -2500 | 60.4 | 3811.4 | | | | 1568 | T2379 | 54'-56' | | | | 0.030 | 1.03 | 0.06 | 2.06 |
| | -2500 | 59.0 | 3810.0 | | | | 1569 | T2380 | 56'-58' | | | | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2500 | 57.6 | 3808.6 | | | | 1570 | T2381 | 58'-60' | | | | 0.010 | 0.34 | 0.09 | 3.09 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | | | | | | | | | | | | | | | | |
| CEM 2-17 | 2500S | 150W | 3847.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2500 | 148.6 | 3845.6 | | | | 1571 | T2382 | 0'-2' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2500 | 147.2 | 3844.2 | | | | 1572 | T2383 | 2'-4' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2500 | 145.8 | 3842.8 | | | | 1573 | T2384 | 4'-6' | | | | 0.020 | 0.69 | 0.07 | 2.40 |
| | -2500 | 144.3 | 3841.3 | | | | 1574 | T2385 | 6'-8' | | | | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2500 | 142.9 | 3839.9 | | | | 1575 | T2386 | 8'-10' | | | | 0.060 | 2.06 | 0.04 | 1.37 |
| | -2500 | 141.5 | 3838.5 | | | | 1576 | T2387 | 10'-12' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | -2500 | 140.1 | 3837.1 | | | | 1577 | T2388 | 12'-14' | | | | 0.030 | 1.03 | 0.05 | 1.71 |
| | -2500 | 138.7 | 3835.7 | | | | 1578 | T2389 | 14'-16' | | | | 0.030 | 1.03 | 0.05 | 1.71 |
| | -2500 | 137.3 | 3834.3 | | | | 1579 | T2390 | 16'-18' | | | | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2500 | 135.9 | 3832.9 | | | | 1580 | T2391 | 18'-20' | | | | 0.040 | 1.37 | 0.04 | 1.37 |
| | -2500 | 134.4 | 3831.4 | | | | 1581 | T2392 | 20'-22' | | | | 0.010 | 0.34 | 0.04 | 1.37 |
| | -2500 | 133.0 | 3830.0 | | | | 1582 | T2393 | 22'-24' | | | | 0.010 | 0.34 | 0.07 | 2.40 |
| | -2500 | 131.6 | 3828.6 | | | | 1583 | T2394 | 24'-26' | | | | 0.030 | 1.03 | 0.04 | 1.37 |
| | -2500 | 130.2 | 3827.2 | | | | 1584 | T2395 | 26'-28' | | | | 0.020 | 0.69 | 0.03 | 1.03 |
| | -2500 | 128.8 | 3825.8 | | | | 1585 | T2396 | 28'-30' | | | | 0.030 | 1.03 | 0.03 | 1.03 |
| | -2500 | 127.4 | 3824.4 | | | | 1586 | T2397 | 30'-32' | | | | 0.050 | 1.71 | 0.05 | 1.71 |
| | -2500 | 126.0 | 3823.0 | | | | 1587 | T2398 | 32'-34' | | | | 0.020 | 0.69 | 0.05 | 1.71 |
| | -2500 | 124.5 | 3821.5 | | | | 1588 | T2399 | 34'-36' | | | | 0.010 | 0.34 | 0.06 | 2.06 |
| | -2500 | 123.1 | 3820.1 | | | | 1589 | T2400 | 36'-38' | | | | 0.020 | 0.69 | 0.05 | 1.71 |
| | -2500 | 121.7 | 3818.7 | | | | 1590 | T2401 | 38'-40' | | | | 0.030 | 1.03 | 0.02 | 0.69 |
| | -2500 | 120.3 | 3817.3 | | | | 1591 | T2402 | 40'-42' | | | | 0.040 | 1.37 | 0.03 | 1.03 |
| | -2500 | 118.9 | 3815.9 | | | | 1592 | T2403 | 42'-44' | | | | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2500 | 117.5 | 3814.5 | | | | 1593 | T2404 | 44'-46' | | | | 0.030 | 1.03 | 0.02 | 0.69 |
| | -2500 | 116.1 | 3813.1 | | | | 1594 | T2405 | 46'-48' | | | | 0.020 | 0.69 | 0.06 | 2.06 |
| | -2500 | 114.7 | 3811.6 | | | | 1595 | T2406 | 48'-50' | | | | 0.050 | 1.71 | 0.02 | 0.69 |
| | -2500 | 113.2 | 3810.2 | | | | 1596 | T2407 | 50'-52' | | | | 0.010 | 0.34 | 0.02 | 0.69 |
| | -2500 | 111.8 | 3808.8 | | | | 1597 | T2408 | 52'-54' | | | | 0.010 | 0.34 | 0.03 | 1.03 |
| | -2500 | 110.4 | 3807.4 | | | | 1598 | T2409 | 54'-56' | | | | 0.020 | 0.69 | 0.02 | 0.69 |
| | -2500 | 109.0 | 3806.0 | | | | 1599 | T2410 | 56'-58' | | | | 0.010 | 0.34 | 0.03 | 1.03 |
| | -2500 | 107.6 | 3804.6 | | | | 1600 | T2411 | 58'-60' | | | | 0.020 | 0.69 | 0.04 | 1.37 |
| | | | | | | | | | | | | | | | | |
| CEM 2-20 | 2510S | 225W | 3845.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2510 | 223.6 | 3843.6 | | | | 2981 | T2771 | 0'-2' | | | | 0.010 | 0.34 | | |
| | -2510 | 222.2 | 3842.2 | | | | 2982 | T2772 | 2'-4' | | | | 0.010 | 0.34 | | |
| | -2510 | 220.8 | 3840.8 | | | | 2983 | T2773 | 4'-6' | | | | 0.010 | 0.34 | | |
| | -2510 | 219.3 | 3839.3 | | | | 2984 | T2774 | 6'-8' | | | | tr. | 0.00 | | |
| | -2510 | 217.9 | 3837.9 | | | | 2985 | T2775 | 8'-10' | | | | 0.010 | 0.34 | | |
| | -2510 | 216.5 | 3836.5 | | | | 2986 | T2776 | 10'-12' | | | | 0.010 | 0.34 | | |
| | -2510 | 215.1 | 3835.1 | | | | 2987 | T2777 | 12'-14' | | | | 0.020 | 0.69 | | |
| | -2510 | 213.7 | 3833.7 | | | | 2988 | T2778 | 14'-16' | | | | 0.010 | 0.34 | | |
| | -2510 | 212.3 | 3832.3 | | | | 2989 | T2779 | 16'-18' | | | | 0.010 | 0.34 | | |
| | -2510 | 210.9 | 3830.9 | | | | 2990 | T2780 | 18'-20' | | | | 0.010 | 0.34 | | |
| | -2510 | 209.4 | 3829.4 | | | | 2991 | T2781 | 20'-22' | | | | 0.020 | 0.69 | | |
| | -2510 | 208.0 | 3828.0 | | | | 2992 | T2782 | 22'-24' | | | | 0.010 | 0.34 | | |
| | -2510 | 206.6 | 3826.6 | | | | 2993 | T2783 | 24'-26' | | | | 0.010 | 0.34 | | |
| | -2510 | 205.2 | 3825.2 | | | | 2994 | T2784 | 26'-28' | | | | 0.030 | 1.03 | | |
| | -2510 | 203.8 | 3823.8 | | | | 2995 | T2785 | 28'-30' | | | | 0.020 | 0.69 | | |
| | -2510 | 202.4 | 3822.4 | | | | 2996 | T2786 | 30'-32' | | | | 0.010 | 0.34 | | |
| | -2510 | 201.0 | 3821.0 | | | | 2997 | T2787 | 32'-34' | | | | 0.010 | 0.34 | | |
| | -2510 | 199.5 | 3819.5 | | | | 2998 | T2788 | 34'-36' | | | | 0.008 | 0.27 | | |
| | -2510 | 198.1 | 3818.1 | | | | 2999 | T2789 | 36'-38' | | | | 0.012 | 0.41 | | |
| | -2510 | 196.7 | 3816.7 | | | | 3000 | T2790 | 38'-40' | | | | 0.010 | 0.34 | | |
| | -2510 | 195.3 | 3815.3 | | | | 3001 | T2791 | 40'-42' | | | | 0.005 | 0.17 | | |
| | -2510 | 193.9 | 3813.9 | | | | 3002 | T2792 | 42'-44' | | | | 0.010 | 0.34 | | |
| | -2510 | 192.5 | 3812.5 | | | | 3003 | T2793 | 44'-46' | | | | 0.007 | 0.24 | | |
| | -2510 | 191.1 | 3811.1 | | | | 3004 | T2794 | 46'-48' | | | | 0.010 | 0.34 | | |
| | -2510 | 189.7 | 3809.6 | | | | 3005 | T2795 | 48'-50' | | | | 0.007 | 0.24 | | |
| | -2510 | 188.2 | 3808.2 | | | | 3006 | T2796 | 50'-52' | | | | 0.008 | 0.27 | | |
| | -2510 | 186.8 | 3806.8 | | | | 3007 | T2797 | 52'-54' | | | | 0.010 | 0.34 | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | Lab No. | FieldNo. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2510 | 185.4 | 3805.4 | | | | 3008 | T2798 | 54'-56' | | | | 0.010 | 0.34 | | |
| | -2510 | 184.0 | 3804.0 | | | | 3009 | T2799 | 56'-58' | | | | 0.010 | 0.34 | | |
| | -2510 | 182.6 | 3802.6 | | | | 3010 | T2800 | 58'-60' | | | | 0.010 | 0.34 | | |
| | -2510 | 181.2 | 3801.2 | | | | 3011 | T2801 | 60'-66' | | | | 0.010 | 0.34 | | |

Color coding:

| | |
|---|---|
| 0.50 to 0.99 g/T Au | **yellow** |
| 1.00 to 2.99 g/T Au | **orange** |
| 3.00 g/T Au or greater | **red** |

## Geologic Explanation for Appendices B, C, D & E

**Type (Rock Type).**

BX – Breccia (Stage II through Stage IV breccias (commonly with overprinting of later re-brecciation or Stage V & VI veins)

FW – Footwall (adamellite)

HW – Hanging wall (adamellite)

VN – Fissure Vein, including Stage V & VI

**Alt (Hydrothermal Alteration): (A) dominant breccia matrix mineralogy or (B) alteration zone represented in sample.**

| | | |
|---|---|---|
| (A) | QC – quartz-chlorite | Stage III matrix (with adularia) |
| | OCP – quartz-chlorite-pyrite | Stage III matrix |
| | QS – quartz-sericite | Stage IV matrix (with illite) |
| | QSP – quartz-sericite-pyrite | Stage IV matrix |
| | QCS – quartz-chlorite-sericite | Stage III & IV with overprint |
| | QCSP – quartz-chlorite-sericite-pyrite | Stage III & IV + pyrite |
| (B) | Ain – argillic (inner) | montmorillinite-sericite±kaolinite |
| | Aout – argillic (outer) | montmorillinite-illite-chlorite |
| | Pin – propylitic (inner) | chlorite-montmorillinite zone |
| | Pout – propylitic (outer) | chlorite-epidote zone |

**Min (Mineralogy): Fissure vein mineralogy as logged in drill cuttings in (A) Telegraph-type veins and (B) other veins or supergene byproducts in fractures.**

| | | |
|---|---|---|
| (A) | Qcmn – quartz-manganese oxide-calcite | Stage IV vein |
| | Qfn – quartz fine grained | Stage V vein (with adularia) |
| | Qfnp – quartz fine grained + pyrite | Stage V vein |
| | Qs – quartz stockwork | Stage V "crackle breccia" cement |
| | Qvg – quartz, vuggy texture | Stage V, coarse-grained phase |
| (B) | CuO – Copper oxides | includes all supergene Cu minerals |
| | FeO – iron oxides | all conspicuous oxides & hydroxides |
| | Goss – gossan | oxidized high-sulfide vein (±quartz) |
| | QFe – quartz iron oxides | veinlets of unknown origin |
| | Qmp – quartz-massive + pyrite | early "Bull" quartz veins |
| | 0 – no vein material | |

# Appendix C

**Telegraph Hill No. 1 Area Drill Data**

Appendix C. Telegraph Hill No. 1 Area Drill Data.

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM 1-6 | 2960S | 110W | 3863.0 | 298 | -30 | 34' | | | | | | | | | | |
| | -2960 | 111.7 | 3862.0 | | | | T1579 | 746 | 0'-2' | Hw | Pout | 0 | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2960 | 113.5 | 3861.0 | | | | T1580 | 747 | 2'-4' | Hw | Pout | 0 | 0.040 | 1.371 | 0.05 | 1.714 |
| | -2960 | 115.2 | 3860.0 | | | | T1581 | 748 | 4'-6' | Hw | Pout | 0 | 0.010 | 0.343 | 0.04 | 1.371 |
| | -2960 | 116.9 | 3859.0 | | | | T1582 | 749 | 6'-8' | Hw | Pin | 0 | 0.020 | 0.686 | 0.08 | 2.743 |
| | -2960 | 118.7 | 3858.0 | | | | T1583 | 750 | 8'-10' | Hw | Aout | 0 | 0.030 | 1.029 | 0.04 | 1.371 |
| | -2960 | 120.4 | 3857.0 | | | | T1584 | 751 | 10'-12' | Hw | Aout | Qvg | 0.170 | 5.829 | 0.07 | 2.400 |
| | -2960 | 122.1 | 3856.0 | | | | T1585 | 752 | 12'-14' | Hw | Aout | 0 | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2960 | 123.9 | 3855.0 | | | | T1586 | 753 | 14'-16' | Hw | Pin | FeO | 0.010 | 0.343 | 0.03 | 1.029 |
| | -2960 | 125.6 | 3854.0 | | | | T1584 | 754 | 16'-18' | Hw | 0 | 0 | 0.010 | 0.343 | 0.03 | 1.029 |
| | -2960 | 127.3 | 3853.0 | | | | T1588 | 755 | 18'-20' | Hw | 0 | 0 | 0.090 | 3.086 | 0.08 | 2.743 |
| | -2960 | 129.1 | 3852.0 | | | | T1589 | 756 | 20'-22' | Hw | 0 | 0 | 0.030 | 1.029 | 0.04 | 1.371 |
| | -2960 | 130.8 | 3851.0 | | | | T1590 | 757 | 22'-24' | Hw | 0 | 0 | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2960 | 132.5 | 3850.0 | | | | T1591 | 758 | 24'-26' | Hw | Aout | Qfnp | 0.130 | 4.457 | 0.07 | 2.400 |
| | -2960 | 134.2 | 3849.0 | | | | T1592 | 759 | 26'-28' | Bx | QSP | Qfnp | 0.120 | 4.114 | 0.09 | 3.086 |
| | -2960 | 136.0 | 3848.0 | | | | T1593 | 760 | 28'-30' | Vn | 0 | Qfn | 0.430 | 14.743 | 0.15 | 5.143 |
| | -2960 | 137.7 | 3847.0 | | | | T1594 | 761 | 30'-32' | Vn | 0 | Qfn | 1.070 | 36.686 | 0.25 | 8.571 |
| | -2960 | 139.4 | 3846.0 | | | | T1595 | 762 | 32'-34' | Bx | QSP | Qvg | 0.790 | 27.086 | 0.28 | 9.600 |
| | | | | | | | | | | | | | | | | |
| CEM 1-3 | 2960S | 190W | 3861.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -2960 | 188.6 | 3859.6 | | | | T1514 | 681 | 0'-2' | Hw | Pin | 0 | 0.030 | 1.029 | 0.06 | 2.057 |
| | -2960 | 187.2 | 3858.2 | | | | T1515 | 682 | 2'-4' | Bx | QSP | 0 | 0.530 | 18.171 | 0.08 | 2.743 |
| | -2960 | 185.8 | 3856.8 | | | | T1516 | 683 | 4'-6' | Hw | Ain | Qvg | 0.080 | 2.743 | 0.22 | 7.543 |
| | -2960 | 184.3 | 3855.3 | | | | T1517 | 684 | 6'-8' | Hw | | | 0.040 | 1.371 | 0.04 | 1.371 |
| | -2960 | 182.9 | 3853.9 | | | | T1518 | 685 | 8'-10' | Vn | 0 | Qfn | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2960 | 181.5 | 3852.5 | | | | T1519 | 686 | 10'-12' | Vn | 0 | Qfn | 0.030 | 1.029 | 0.01 | 0.343 |
| | -2960 | 180.1 | 3851.1 | | | | T1520 | 687 | 12'-14' | Vn | 0 | Qfn | 0.010 | 0.343 | 0.02 | 0.686 |
| | -2960 | 178.7 | 3849.7 | | | | T1521 | 688 | 14'-16' | | | | 0.020 | 0.686 | 0.02 | 0.686 |
| | -2960 | 177.3 | 3848.3 | | | | T1522. | 689 | 16'-18' | Vn | 0 | Qfn | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2960 | 175.9 | 3846.9 | | | | T1523 | 690 | 18'-20' | Vn | 0 | Qfn | 0.040 | 1.371 | 0.02 | 0.686 |
| | -2960 | 174.4 | 3845.4 | | | | T1524 | 691 | 20'-22' | Vn | 0 | Qfn | 0.030 | 1.029 | 0.21 | 7.200 |
| | -2960 | 173.0 | 3844.0 | | | | T1525 | 692 | 22'-24' | vn | 0 | Qfn | 0.090 | 3.086 | 0.02 | 0.686 |
| | -2960 | 171.6 | 3842.6 | | | | T1526 | 693 | 24'-26' | Vn | 0 | Qfn | 0.040 | 1.371 | 0.07 | 2.400 |
| | -2960 | 170.2 | 3841.2 | | | | T1527 | 694 | 26'-28' | Vn | 0 | Qfn | 0.020 | 0.686 | 0.02 | 0.686 |
| | -2960 | 168.8 | 3839.8 | | | | T1528 | 695 | 28'-30' | Vn | 0 | Qfn | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2960 | 167.4 | 3838.4 | | | | T1529 | 696 | 30'-32' | Vn | 0 | Qfn | 0.030 | 1.029 | 0.03 | 1.029 |
| | -2960 | 166.0 | 3837.0 | | | | T1530 | 697 | 32'-34' | Vn | 0 | Qfn | 0.140 | 4.800 | 0.17 | 5.829 |
| | -2960 | 164.5 | 3835.5 | | | | T1531 | 698 | 34'-36' | Hw | Aout | Qfn | 0.260 | 8.914 | 0.54 | 18.514 |
| | -2960 | 163.1 | 3834.1 | | | | T1532 | 699 | 36'-38' | Bx | QSP | Qfnp | 0.150 | 5.143 | 0.27 | 9.257 |
| | -2960 | 161.7 | 3832.7 | | | | T1533 | 700 | 38'-40' | Bx | QSP | Qvg | 0.060 | 2.057 | 0.40 | 13.714 |
| | -2960 | 160.3 | 3831.3 | | | | T1534 | 701 | 40'-42' | Bx | QC | Qfn | 0.190 | 6.514 | 0.42 | 14.400 |
| | -2960 | 158.9 | 3829.9 | | | | T1535 | 702 | 42'-44' | Fw | Pin | Qvg | 0.150 | 5.143 | 0.32 | 10.971 |
| | -2960 | 157.5 | 3828.5 | | | | T1536 | 703 | 44'-46' | Fw | Pin | Qvg | 0.150 | 5.143 | 0.37 | 12.686 |
| | -2960 | 156.1 | 3827.1 | | | | 1'1537 | 704 | 46'-48' | Fw | Aout | Qvg | 0.130 | 4.457 | 0.26 | 8.914 |
| | -2960 | 154.7 | 3825.6 | | | | T1538 | 705 | 48'-50' | Bx | QSP | Qfn | 0.100 | 3.429 | 0.12 | 4.114 |
| | -2960 | 153.2 | 3824.2 | | | | T1539 | 706 | 50'-52' | Fw | Aout | Qvg | 0.120 | 4.114 | 0.16 | 5.486 |
| | -2960 | 151.8 | 3822.8 | | | | T1540 | 707 | 52'-54' | Fw | Aout | Qvg | 0.040 | 1.371 | 0.09 | 3.086 |
| | -2960 | 150.4 | 3821.4 | | | | T1541 | 708 | 54'-56' | Vn | 0 | Qfn | 0.060 | 2.057 | 0.09 | 3.086 |
| | -2960 | 149.0 | 3820.0 | | | | T1542 | 709 | 56'-58' | | | | 0.060 | 2.057 | 0.09 | 3.086 |
| | -2960 | 147.6 | 3818.6 | | | | T1543 | 710 | 58'-60' | | | | 0.050 | 1.714 | 0.08 | 2.743 |
| | | | | | | | | | | | | | | | | |
| CEM 1-5 | 2970S | 110W | 3865.0 | 298 | -30 | 30' | | | | | | | | | | |
| | -2970 | 111.7 | 3864.0 | | | | T1564 | 731 | 0'-2' | | | | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2970 | 113.5 | 3863.0 | | | | T1565 | 732 | 2'-4' | | | | 0.020 | 0.686 | 0.01 | 0.343 |
| | -2970 | 115.2 | 3862.0 | | | | T1566 | 733 | 4'-6' | | | | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2970 | 116.9 | 3861.0 | | | | T1567 | 734 | 6'-8' | | | | 0.010 | 0.343 | 0.02 | 0.686 |
| | -2970 | 118.7 | 3860.0 | | | | T1568 | 735 | 8'-10' | | | | tr. | 0.000 | 0.02 | 0.686 |
| | -2970 | 120.4 | 3859.0 | | | | T1569 | 736 | 10'-12' | | | | 0.470 | 16.114 | 0.12 | 4.114 |
| | -2970 | 122.1 | 3858.0 | | | | T1570 | 737 | 12'-14' | | | | 0.160 | 5.486 | 0.04 | 1.371 |
| | -2970 | 123.9 | 3857.0 | | | | T1571 | 738 | 14'-16' | | | | 0.040 | 1.371 | 0.04 | 1.371 |
| | -2970 | 125.6 | 3856.0 | | | | T1572 | 739 | 16'-18' | | | | 0.090 | 3.086 | 0.04 | 1.371 |
| | -2970 | 127.3 | 3855.0 | | | | T1573 | 740 | 18'-20' | | | | 0.010 | 0.343 | 0.03 | 1.029 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2970 | 129.1 | 3854.0 | | | | T1574 | 741 | 20'-22' | | | | 0.060 | 2.057 | 0.06 | 2.057 |
| | -2970 | 130.8 | 3853.0 | | | | T1575 | 742 | 22'-24' | | | | 0.090 | 3.086 | 0.05 | 1.714 |
| | -2970 | 132.5 | 3852.0 | | | | T1576 | 743 | 24'-26' | | | | 0.070 | 2.400 | 0.04 | 1.371 |
| | -2970 | 134.2 | 3851.0 | | | | T1577 | 744 | 26'-28' | | | | 0.060 | 2.057 | 0.1 | 3.429 |
| | -2970 | 136.0 | 3850.0 | | | | T1578 | 745 | 28'-30' | | | | 0.160 | 5.486 | 0.13 | 4.457 |
| | | | | | | | | | | | | | | | | |
| CEM 1-2 | 2970S | 190W | 3861.0 | 118 | -45 | 38' | | | | | | | | | | |
| | -2970 | 188.6 | 3859.6 | | | | T1495 | 662 | 0'-2' | | | | 0.210 | 7.200 | 0.35 | 12.000 |
| | -2970 | 187.2 | 3858.2 | | | | T1496 | 663 | 2'-4' | | | | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2970 | 185.8 | 3856.8 | | | | T1497 | 664 | 4'-6' | | | | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2970 | 184.3 | 3855.3 | | | | T1498 | 665 | 6'-8' | | | | 0.020 | 0.686 | 0.01 | 0.343 |
| | -2970 | 182.9 | 3853.9 | | | | T1499 | 666 | 8'-10' | | | | 0.010 | 0.343 | 0.02 | 0.686 |
| | -2970 | 181.5 | 3852.5 | | | | T1500 | 667 | 10'-12' | | | | 0.020 | 0.686 | 0.01 | 0.343 |
| | -2970 | 180.1 | 3851.1 | | | | T1501 | 668 | 12'-14' | | | | 0.040 | 1.371 | 0.03 | 1.029 |
| | -2970 | 178.7 | 3849.7 | | | | T1502 | 669 | 14'-16' | | | | 0.020 | 0.686 | 0.02 | 0.686 |
| | -2970 | 177.3 | 3848.3 | | | | T1503 | 670 | 16'-18' | | | | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2970 | 175.9 | 3846.9 | | | | T1504 | 671 | 18'-20' | | | | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2970 | 174.4 | 3845.4 | | | | T1505 | 672 | 20'-22' | | | | 0.030 | 1.029 | 0.04 | 1.371 |
| | -2970 | 173.0 | 3844.0 | | | | T1506 | 673 | 22'-24' | | | | 0.030 | 1.029 | 0.02 | 0.686 |
| | -2970 | 171.6 | 3842.6 | | | | T1507 | 674 | 24'-26' | | | | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2970 | 170.2 | 3841.2 | | | | T1508 | 675 | 26'-28' | | | | 0.010 | 0.343 | 0.02 | 0.686 |
| | -2970 | 168.8 | 3839.8 | | | | T1509 | 676 | 28'-30' | | | | 0.030 | 1.029 | 0.02 | 0.686 |
| | -2970 | 167.4 | 3838.4 | | | | T1510 | 677 | 30'-32' | | | | 0.040 | 1.371 | 0.07 | 2.400 |
| | -2970 | 166.0 | 3837.0 | | | | T1511 | 678 | 32'-34' | | | | 0.040 | 1.371 | 0.06 | 2.057 |
| | -2970 | 164.5 | 3835.5 | | | | T1512 | 679 | 34'-36' | | | | 0.050 | 1.714 | 0.12 | 4.114 |
| | -2970 | 163.1 | 3834.1 | | | | T1513 | 680 | 36'-38' | | | | 0.150 | 5.143 | 0.40 | 13.714 |
| | | | | | | | | | | | | | | | | |
| CEM 1-4 | 2980S | 110W | 3867.0 | 298 | -30 | 40' | | | | | | | | | | |
| | -2980 | 111.7 | 3866.0 | | | | T1544 | 711 | 0'-2' | | | | 0.070 | 2.400 | 0.05 | 1.714 |
| | -2980 | 113.5 | 3865.0 | | | | T1545 | 712 | 2'-4' | | | | 0.070 | 2.400 | 0.07 | 2.400 |
| | -2980 | 115.2 | 3864.0 | | | | T1546 | 713 | 4'-6' | | | | 0.050 | 1.714 | 0.1 | 3.429 |
| | -2980 | 116.9 | 3863.0 | | | | T1547 | 714 | 6'-8' | | | | 0.020 | 0.686 | 0.07 | 2.400 |
| | -2980 | 118.7 | 3862.0 | | | | T1548 | 715 | 8'-10' | | | | 0.020 | 0.686 | 0.04 | 1.371 |
| | -2980 | 120.4 | 3861.0 | | | | T1549 | 716 | 10'-12' | | | | 0.010 | 0.343 | 0.04 | 1.371 |
| | -2980 | 122.1 | 3860.0 | | | | T1550 | 717 | 12'-14' | | | | 0.070 | 2.400 | 0.04 | 1.371 |
| | -2980 | 123.9 | 3859.0 | | | | T1551 | 718 | 14'-16' | | | | 0.030 | 1.029 | 0.02 | 0.686 |
| | -2980 | 125.6 | 3858.0 | | | | T1552 | 719 | 16'-18' | | | | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2980 | 127.3 | 3857.0 | | | | T1553 | 720 | 18'-20' | | | | 0.020 | 0.686 | 0.01 | 0.343 |
| | -2980 | 129.1 | 3856.0 | | | | T1554 | 721 | 20'-22' | | | | 0.020 | 0.686 | 0.06 | 2.057 |
| | -2980 | 130.8 | 3855.0 | | | | T1555 | 722 | 22'-24' | | | | 0.020 | 0.686 | 0.04 | 1.371 |
| | -2980 | 132.5 | 3854.0 | | | | T1556 | 723 | 24'-26' | | | | 0.020 | 0.686 | 0.05 | 1.714 |
| | -2980 | 134.2 | 3853.0 | | | | T1557 | 724 | 26'-28' | | | | 0.040 | 1.371 | 0.03 | 1.029 |
| | -2980 | 136.0 | 3852.0 | | | | T1558 | 725 | 28'-30' | | | | 0.080 | 2.743 | 0.04 | 1.371 |
| | -2980 | 137.7 | 3851.0 | | | | T1559 | 726 | 30'-32' | | | | 0.030 | 1.029 | 0.06 | 2.057 |
| | -2980 | 139.4 | 3850.0 | | | | T1560 | 727 | 32'-34' | | | | 0.040 | 1.371 | 0.06 | 2.057 |
| | -2980 | 141.2 | 3849.0 | | | | T1561 | 728 | 34'-36' | | | | 0.020 | 0.686 | 0.08 | 2.743 |
| | -2980 | 142.9 | 3848.0 | | | | T1562 | 729 | 36'-38' | | | | 0.060 | 2.057 | 0.05 | 1.714 |
| | -2980 | 144.6 | 3847.0 | | | | T1563 | 730 | 38'-40' | | | | 0.340 | 11.657 | 0.12 | 4.114 |
| | | | | | | | | | | | | | | | | |
| CEM 1-1 | 2980S | 190W | 3860.0 | 118 | -45 | 36' | | | | | | | | | | |
| | -2980 | 188.6 | 3858.6 | | | | T1476 | 643 | 0'-2' | | | | 0.040 | 1.371 | 0.02 | 0.686 |
| | -2980 | 187.2 | 3857.2 | | | | T1477 | 644 | 2'-4' | | | | 0.010 | 0.343 | 0.01 | 0.343 |
| | -2980 | 185.8 | 3855.8 | | | | T1478 | 645 | 4'-6' | | | | 0.060 | 2.057 | 0.02 | 0.686 |
| | -2980 | 184.3 | 3854.3 | | | | T1479 | 646 | 6'-8' | | | | 0.030 | 1.029 | 0.01 | 0.343 |
| | -2980 | 182.9 | 3852.9 | | | | T1480 | 647 | 8'-10' | | | | 0.030 | 1.029 | 0.04 | 1.371 |
| | -2980 | 181.5 | 3851.5 | | | | T1482 | 648 | 10'-12' | | | | 0.030 | 1.029 | 0.04 | 1.371 |
| | -2980 | 180.1 | 3850.1 | | | | T1482 | 649 | 12'-14' | | | | 0.010 | 0.343 | 0.03 | 1.029 |
| | -2980 | 178.7 | 3848.7 | | | | T1483 | 650 | 14'-16' | | | | 0.020 | 0.686 | 0.02 | 0.686 |
| | -2980 | 177.3 | 3847.3 | | | | T1484 | 651 | 16'-18' | | | | 0.020 | 0.686 | 0.03 | 1.029 |
| | -2980 | 175.9 | 3845.9 | | | | T1485 | 652 | 18'-20' | | | | 0.020 | 0.686 | 0.02 | 0.686 |
| | -2980 | 174.4 | 3844.4 | | | | T1486 | 653 | 20'-22' | | | | 0.020 | 0.686 | 0.04 | 1.371 |
| | -2980 | 173.0 | 3843.0 | | | | T1487 | 654 | 22'-24' | | | | 0.010 | 0.343 | 0.03 | 1.029 |
| | -2980 | 171.6 | 3841.6 | | | | T1488 | 655 | 24'-26' | | | | 0.040 | 1.371 | 0.03 | 1.029 |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -2980 | 170.2 | 3840.2 | | | | T1489 | 656 | 26'-28' | | | | 0.100 | **3.429** | 0.03 | 1.029 |
| | -2980 | 168.8 | 3838.8 | | | | T1491 | 658 | 28'-30' | | | | 0.020 | **0.686** | 0.02 | 0.686 |
| | -2980 | 167.4 | 3837.4 | | | | T1492 | 659 | 30'-32' | | | | 0.090 | **3.086** | 0.04 | 1.371 |
| | -2980 | 166.0 | 3836.0 | | | | T1493 | 660 | 32'-34' | | | | 0.050 | **1.714** | 0.04 | 1.371 |
| | -2980 | 164.5 | 3834.5 | | | | T1494 | 661 | 34'-36' | | | | 0.100 | **3.429** | 0.06 | 2.057 |
| | | | | | | | | | | | | | | | | |
| CEM 1-16 | 3000S | 135W | 3770.0 | 0 | -90 | 10' | | | | | | | | | | |
| | -3000 | 135.0 | 3875.0 | | | | T2891 | 3391 | 0'-5' | | | | 0.640 | **21.943** | | |
| | -3000 | 135.0 | 3880.0 | | | | T2890 | 3390 | 5'-10' | | | | 0.410 | **14.057** | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-23 | 3004S | 161W | 3876.0 | 163 | -45 | 60' | | | | | | | | | | |
| | -3005.0 | 160.0 | 3874.6 | | | | T2902 | 3402 | 0'-2' | | | | 0.020 | **0.686** | | |
| | -3006.0 | 159.0 | 3873.2 | | | | T2903 | 3403 | 2'-4' | | | | 0.010 | 0.343 | | |
| | -3007.0 | 158.0 | 3871.8 | | | | T2904 | 3404 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3008.0 | 157.0 | 3870.3 | | | | T2905 | 3405 | 6'-8' | | | | 0.010 | 0.343 | | |
| | -3009.0 | 156.0 | 3868.9 | | | | T2906 | 3406 | 8'-10' | | | | 0.010 | 0.343 | | |
| | -3010.0 | 155.0 | 3867.5 | | | | T2907 | 3407 | 10'-12' | | | | 0.010 | 0.343 | | |
| | -3011.0 | 154.0 | 3866.1 | | | | T2908 | 3408 | 12'-14' | | | | 0.020 | **0.686** | | |
| | -3012.0 | 153.0 | 3864.7 | | | | T2909 | 3409 | 14'-16' | | | | 0.010 | 0.343 | | |
| | -3013.0 | 152.0 | 3863.3 | | | | T2910 | 3410 | 16'-18' | | | | 0.010 | 0.343 | | |
| | -3014.0 | 151.0 | 3861.9 | | | | T2911 | 3411 | 18'-20' | | | | 0.010 | 0.343 | | |
| | -3015.0 | 150.0 | 3860.4 | | | | T2912 | 3412 | 20'-22' | | | | 0.010 | 0.343 | | |
| | -3016.0 | 149.0 | 3859.0 | | | | T2913 | 3413 | 22'-24' | | | | 0.020 | **0.686** | | |
| | -3017.0 | 148.0 | 3857.6 | | | | T2914 | 3414 | 24'-26' | | | | 0.010 | 0.343 | | |
| | -3018.0 | 147.0 | 3856.2 | | | | T2915 | 3415 | 26'-28' | | | | 0.010 | 0.343 | | |
| | -3019.0 | 146.0 | 3854.8 | | | | T2916 | 3416 | 28'-30' | | | | 0.010 | 0.343 | | |
| | -3020.0 | 145.0 | 3853.4 | | | | T2917 | 3417 | 30'-32' | | | | 0.140 | **4.800** | | |
| | -3021.0 | 144.0 | 3852.0 | | | | T2918 | 3418 | 32'-34' | | | | 0.590 | **20.229** | | |
| | -3022.0 | 143.0 | 3850.5 | | | | T2919 | 3419 | 34'-36' | | | | 0.030 | **1.029** | | |
| | -3023.0 | 142.0 | 3849.1 | | | | T2920 | 3420 | 36'-38' | | | | 0.030 | **1.029** | | |
| | -3024.0 | 141.0 | 3847.7 | | | | T2921 | 3421 | 38'-40' | | | | 0.020 | **0.686** | | |
| | -3025.0 | 140.0 | 3846.3 | | | | T2812 | 3422 | 40'-42' | | | | 0.030 | **1.029** | | |
| | -3026.0 | 139.0 | 3844.9 | | | | T2923 | 3423 | 42'-44' | | | | 0.010 | 0.343 | | |
| | -3027.0 | 138.0 | 3843.5 | | | | T2924 | 3424 | 44'-46' | | | | 0.140 | **4.800** | | |
| | -3028.0 | 137.0 | 3842.1 | | | | T2925 | 3425 | 46'-48' | | | | 0.050 | **1.714** | | |
| | -3029.0 | 136.0 | 3840.6 | | | | T2926 | 3426 | 48'-50' | | | | 0.020 | **0.686** | | |
| | -3030.0 | 135.0 | 3839.2 | | | | T2927 | 3427 | 50'-52' | | | | 0.020 | **0.686** | | |
| | -3031.0 | 134.0 | 3837.8 | | | | T2928 | 3428 | 52'-54' | | | | 0.010 | 0.343 | | |
| | -3032.0 | 133.0 | 3836.4 | | | | T2929 | 3429 | 54'-56' | | | | 0.020 | **0.686** | | |
| | -3033.0 | 132.0 | 3835.0 | | | | T2930 | 3430 | 56'-58' | | | | 0.020 | **0.686** | | |
| | -3034.0 | 131.0 | 3833.6 | | | | T2931 | 3431 | 58'-60' | | | | 0.030 | **1.029** | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-26 | 3020S | 220W | 3850.0 | 118 | -45 | 62' | | | | | | | | | | |
| | -3020 | 218.6 | 3848.6 | | | | T3142 | 3653 | 2'-4' | | | | 0.010 | 0.343 | | |
| | -3020 | 217.2 | 3847.2 | | | | T3143 | 3654 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3020 | 215.8 | 3845.8 | | | | T3144 | 3655 | 6'-8' | | | | 0.010 | 0.343 | | |
| | -3020 | 214.3 | 3844.3 | | | | T3145 | 3656 | 8'-10' | | | | tr. | 0.000 | | |
| | -3020 | 212.9 | 3842.9 | | | | T3146 | 3657 | 10'-12' | | | | 0.010 | 0.343 | | |
| | -3020 | 211.5 | 3841.5 | | | | T3147 | 3658 | 12'-14' | | | | 0.020 | **0.686** | | |
| | -3020 | 210.1 | 3840.1 | | | | T3148 | 3659 | 14'-16' | | | | 0.020 | **0.686** | | |
| | -3020 | 208.7 | 3838.7 | | | | T3149 | 3660 | 16'-18' | | | | 0.010 | 0.343 | | |
| | -3020 | 207.3 | 3837.3 | | | | T3150 | 3661 | 18'-20' | | | | 0.010 | 0.343 | | |
| | -3020 | 205.9 | 3835.9 | | | | T3151 | 3662 | 20'-22' | | | | 0.010 | 0.343 | | |
| | -3020 | 204.4 | 3834.4 | | | | T3152 | 3663 | 22'-24' | | | | 0.020 | **0.686** | | |
| | -3020 | 203.0 | 3833.0 | | | | T3153 | 3664 | 24'-26' | | | | 0.020 | **0.686** | | |
| | -3020 | 201.6 | 3831.6 | | | | T3154 | 3665 | 26'-28' | | | | 0.010 | 0.343 | | |
| | -3020 | 200.2 | 3830.2 | | | | T3155 | 3666 | 28'-30' | | | | 0.030 | **1.029** | | |
| | -3020 | 198.8 | 3828.8 | | | | T3156 | 3667 | 30'-32' | | | | 0.030 | **1.029** | | |
| | -3020 | 197.4 | 3827.4 | | | | T3157 | 3668 | 32'-34' | | | | 0.020 | **0.686** | | |
| | -3020 | 196.0 | 3826.0 | | | | T3158 | 3669 | 34'-36' | | | | 0.010 | 0.343 | | |
| | -3020 | 194.5 | 3824.5 | | | | T3159 | 3670 | 36'-38' | | | | 0.010 | 0.343 | | |
| | -3020 | 193.1 | 3823.1 | | | | T3160 | 3671 | 38'-40' | | | | 0.020 | **0.686** | | |
| | -3020 | 191.7 | 3821.7 | | | | T3161 | 3672 | 40'-42' | | | | 0.010 | 0.343 | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -3020 | 190.3 | 3820.3 | | | | T3162 | 3673 | 42'-44' | | | | 0.020 | 0.686 | | |
| | -3020 | 188.9 | 3818.9 | | | | T3613 | 3674 | 44'-46' | | | | 0.020 | 0.686 | | |
| | -3020 | 187.5 | 3817.5 | | | | T3164 | 3675 | 46'-48' | | | | 0.010 | 0.343 | | |
| | -3020 | 186.1 | 3816.1 | | | | T3165 | 3676 | 48'-50' | | | | 0.010 | 0.343 | | |
| | -3020 | 184.7 | 3814.6 | | | | T3166 | 3677 | 50'-52' | | | | 0.010 | 0.343 | | |
| | -3020 | 183.2 | 3813.2 | | | | T3167 | 3678 | 52'-54' | | | | 0.010 | 0.343 | | |
| | -3020 | 181.8 | 3811.8 | | | | T3168 | 3679 | 54'-56' | | | | 0.020 | 0.686 | | |
| | -3020 | 180.4 | 3810.4 | | | | T3169 | 3680 | 56'-58' | | | | 0.020 | 0.686 | | |
| | -3020 | 179.0 | 3809.0 | | | | T3170 | 3681 | 58'-60' | | | | 0.010 | 0.343 | | |
| | -3020 | 177.6 | 3807.6 | | | | T3171 | 3682 | 60'-62' | | | | 0.010 | 0.343 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-24 | 3021S | 178W | 3857.0 | 163 | -45 | 60' | | | | | | | | | | |
| | -3022.0 | 177.0 | 3855.6 | | | | T2962 | 3462 | 0'-2' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3023.0 | 176.0 | 3854.2 | | | | T2963 | 3463 | 2'-4' | Hw | 0 | 0 | 0.040 | 1.371 | | |
| | -3024.0 | 175.0 | 3852.8 | | | | T2964 | 3464 | 4'-6' | Hw | 0 | 0 | 0.020 | 0.686 | | |
| | -3025.0 | 174.0 | 3851.3 | | | | T2965 | 3465 | 6'-8' | Hw | 0 | 0 | 0.020 | 0.686 | | |
| | -3026.0 | 173.0 | 3849.9 | | | | T2966 | 3466 | 8'-10' | Hw | 0 | 0 | 0.020 | 0.686 | | |
| | -3027.0 | 172.0 | 3848.5 | | | | T2967 | 3467 | 10'-12' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3028.0 | 171.0 | 3847.1 | | | | T2968 | 3468 | 12'-14' | Hw | 0 | 0 | 0.020 | 0.686 | | |
| | -3029.0 | 170.0 | 3845.7 | | | | T2969 | 3469 | 14'-16' | Hw | 0 | 0 | tr. | 0.000 | | |
| | -3030.0 | 169.0 | 3844.3 | | | | T2970 | 3470 | 16'-18' | Hw | 0 | 0 | 0.040 | 1.371 | | |
| | -3031.0 | 168.0 | 3842.9 | | | | T2971 | 3471 | 18'-20' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3032.0 | 167.0 | 3841.4 | | | | T2972 | 3472 | 20'-22' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3033.0 | 166.0 | 3840.0 | | | | T2974 | 3473 | 22'-24' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3034.0 | 165.0 | 3838.6 | | | | T2974 | 3474 | 24'-26' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3035.0 | 164.0 | 3837.2 | | | | T2975 | 3475 | 26'-28' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3036.0 | 163.0 | 3835.8 | | | | T2976 | 3479 | 28'-30' | Hw | 0 | 0 | 0.010 | 0.343 | | |
| | -3037.0 | 162.0 | 3834.4 | | | | T2977 | 3477 | 30'-32' | Bx | QSP | 0 | 0.020 | 0.686 | | |
| | -3038.0 | 161.0 | 3833.0 | | | | T2978 | 3478 | 32'-34' | Vn | 0 | Qfn | 0.300 | 10.286 | | |
| | -3039.0 | 160.0 | 3831.5 | | | | T2979 | 3479 | 34'-36' | vn | QSP | Qfnp | 0.620 | 21.257 | | |
| | -3040.0 | 159.0 | 3830.1 | | | | T2980 | 3480 | 36'-38' | Fw | 0 | Qfnp | 0.430 | 14.743 | | |
| | -3041.0 | 158.0 | 3828.7 | | | | T2981 | 3481 | 38'-40' | Vn | QC | Qfn | 0.290 | 9.943 | | |
| | -3042.0 | 157.0 | 3827.3 | | | | T2982 | 3482 | 40'-42' | Bx | Ain | Qfn | 0.130 | 4.457 | | |
| | -3043.0 | 156.0 | 3825.9 | | | | T2983 | 3483 | 42'-44' | Fw | Pin | Qvg | 0.080 | 2.743 | | |
| | -3044.0 | 155.0 | 3824.5 | | | | T2984 | 3484 | 44'-46' | Fw | Pout | Qvg | 0.060 | 2.057 | | |
| | -3045.0 | 154.0 | 3823.1 | | | | T2985 | 3485 | 46'-48' | Fw | Pout | 0 | 0.070 | 2.400 | | |
| | -3046.0 | 153.0 | 3821.6 | | | | T2986 | 3486 | 48'-50' | Fw | Pout | 0 | 0.020 | 0.686 | | |
| | -3047.0 | 152.0 | 3820.2 | | | | T2987 | 3487 | 50'-52' | Fw | Pout | 0 | 0.010 | 0.343 | | |
| | -3048.0 | 151.0 | 3818.8 | | | | T2988 | 3488 | 52'-54' | Fw | Pout | 0 | 0.070 | 2.400 | | |
| | -3049.0 | 150.0 | 3817.4 | | | | T2989 | 3489 | 54'-56' | Fw | Pout | 0 | 0.020 | 0.686 | | |
| | -3050.0 | 149.0 | 3816.0 | | | | T2990 | 3490 | 56'-58' | Fw | Pout | 0 | 0.010 | 0.343 | | |
| | -3051.0 | 148.0 | 3814.6 | | | | T2991 | 3491 | 58'-60' | Fw | Pout | 0 | 0.010 | 0.343 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-17 | 3024S | 136W | 3885.0 | 0 | -90 | 10' | | | | | | | | | | |
| | -3024 | 136 | 3880.0 | | | | T2892 | 3392 | 0'-5' | | | | 0.480 | 16.457 | | |
| | -3024 | 136 | 3875.0 | | | | T2893 | 3393 | 5'-10' | | | | 0.490 | 16.800 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-18 | 3033S | 136W | 3888.0 | 0 | -90 | 10' | | | | | | | | | | |
| | -3033 | 136.0 | 3883.0 | | | | T2894 | 3394 | 0'-5' | | | | 0.010 | 0.343 | | |
| | -3033 | 136.0 | 3878.0 | | | | T2895 | 3395 | 5'-10' | | | | 0.010 | 0.343 | | |
| | | | | | | | | | | | | | | | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM 1-25 | 3038S | 195W | 3852.0 | 163 | -45 | 60' | | | | | | | | | | |
| | -3039.0 | 194.0 | 3850.6 | | | | T2932 | 3432 | 0'-2' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3040.0 | 193.0 | 3849.2 | | | | T2933 | 3433 | 2'-4' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3041.0 | 192.0 | 3847.8 | | | | T2934 | 3434 | 4'-6' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3042.0 | 191.0 | 3846.3 | | | | T2935 | 3435 | 6'-8' | Hw | Pout | 0 | tr. | 0.000 | | |
| | -3043.0 | 190.0 | 3844.9 | | | | T2936 | 3436 | 8'-10' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3044.0 | 189.0 | 3843.5 | | | | T2937 | 3437 | 10'-12' | Hw | Pout | 0 | 0.020 | 0.686 | | |
| | -3045.0 | 188.0 | 3842.1 | | | | T2938 | 3438 | 12'-14' | Hw | Pout | 0 | 0.030 | 1.029 | | |
| | -3046.0 | 187.0 | 3840.7 | | | | T2939 | 3439 | 14'-16' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3047.0 | 186.0 | 3839.3 | | | | T2940 | 3440 | 16'-18' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3048.0 | 185.0 | 3837.9 | | | | T2941 | 3441 | 18'-20' | Hw | Pout | 0 | 0.010 | 0.343 | | |
| | -3049.0 | 184.0 | 3836.4 | | | | T2942 | 3442 | 20'-22' | Bx | QSP | Qvg | 0.180 | 6.171 | | |
| | -3050.0 | 183.0 | 3835.0 | | | | T2943 | 3443 | 22'-24' | Fw | Aout | Qvgp | 0.020 | 0.686 | | |
| | -3051.0 | 182.0 | 3833.6 | | | | T2944 | 3444 | 24'-26' | Fw | QSP | Qvg | 0.030 | 1.029 | | |
| | -3052.0 | 181.0 | 3832.2 | | | | T2945 | 3445 | 26'-28' | Fw | 0 | Qfn | 0.130 | 4.457 | | |
| | -3053.0 | 180.0 | 3830.8 | | | | T2946 | 3446 | 28'-30' | Vn | 0 | Qfnp | 0.070 | 2.400 | | |
| | -3054.0 | 179.0 | 3829.4 | | | | T2947 | 3447 | 30'-32' | Vn | 0 | Qfn | 0.290 | 9.943 | | |
| | -3055.0 | 178.0 | 3828.0 | | | | T2948 | 3448 | 32'-34' | Fw | Aout | Qfnp | 0.130 | 4.457 | | |
| | -3056.0 | 177.0 | 3826.5 | | | | T2949 | 3449 | 34'-36' | Fw | Aout | Qfn | 0.070 | 2.400 | | |
| | -3057.0 | 176.0 | 3825.1 | | | | T2950 | 3450 | 36'-38' | Fw | 0 | 0 | 0.100 | 3.429 | | |
| | -3058.0 | 175.0 | 3823.7 | | | | T2951 | 3451 | 38'-40' | Fw | 0 | 0 | 0.080 | 2.743 | | |
| | -3059.0 | 174.0 | 3822.3 | | | | T2952 | 3452 | 40'-42' | Fw | 0 | 0 | 0.030 | 1.029 | | |
| | -3060.0 | 173.0 | 3820.9 | | | | T2953 | 3453 | 42'-44' | Fw | 0 | 0 | 0.020 | 0.686 | | |
| | -3061.0 | 172.0 | 3819.5 | | | | T2954 | 3454 | 44'-46' | Fw | 0 | 0 | 0.030 | 1.029 | | |
| | -3062.0 | 171.0 | 3818.1 | | | | T2955 | 3455 | 46'-48' | Fw | .o | 0 | 0.060 | 2.057 | | |
| | -3063.0 | 170.0 | 3816.6 | | | | T2956 | 3456 | 48'-50' | Fw | 0 | 0 . | 0.080 | 2.743 | | |
| | -3064.0 | 169.0 | 3815.2 | | | | T2957 | 3457 | 50'-52' | Fw | 0 | 0 | 0.090 | 3.086 | | |
| | -3065.0 | 168.0 | 3813.8 | | | | T2958 | 3458 | 52'-54' | Fw | 0 | 0 | 0.070 | 2.400 | | |
| | -3066.0 | 167.0 | 3812.4 | | | | T2959 | 3459 | 54'-56' | Fw | 0 | 0 | 0.030 | 1.029 | | |
| | -3067.0 | 166.0 | 3811.0 | | | | T2960 | 3460 | 56'-58' | Fw | 0 | 0 | 0.020 | 0.686 | | |
| | -3068.0 | 165.0 | 3809.6 | | | | T2961 | 3461 | 58'-60' | Fw | 0 | 0 | 0.050 | 1.714 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-32 | 3045S | 255W | 3851.0 | 118 | -45 | 64' | | | | | | | | | | |
| | -3045 | 253.6 | 3849.6 | | | | T3051 | 3562 | 0'-2' | | | | 0.020 | 0.686 | | |
| | -3045 | 252.2 | 3848.2 | | | | T3052 | 3563 | 2'-4' | | | | 0.010 | 0.343 | | |
| | -3045 | 250.8 | 3846.8 | | | | T3053 | 3564 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3045 | 249.3 | 3845.3 | | | | T3054 | 3565 | 6'-8' | | | | 0.010 | 0.343 | | |
| | -3045 | 247.9 | 3843.9 | | | | T3055 | 3566 | 8'-10' | | | | 0.010 | 0.343 | | |
| | -3045 | 246.5 | 3842.5 | | | | T3056 | 3567 | 10'-12' | | | | 0.010 | 0.343 | | |
| | -3045 | 245.1 | 3841.1 | | | | T3057 | 3568 | 12'-14' | | | | 0.010 | 0.343 | | |
| | -3045 | 243.7 | 3839.7 | | | | T3058 | 3569 | 14'-16' | | | | 0.010 | 0.343 | | |
| | -3045 | 242.3 | 3838.3 | | | | T3059 | 3570 | 16'-18' | | | | 0.010 | 0.343 | | |
| | -3045 | 240.9 | 3836.9 | | | | T3060 | 3571 | 18'-20' | | | | 0.010 | 0.343 | | |
| | -3045 | 239.4 | 3835.4 | | | | T3061 | 3572 | 20'-22' | | | | 0.010 | 0.343 | | |
| | -3045 | 238.0 | 3834.0 | | | | T3062 | 3573 | 22'-24' | | | | 0.020 | 0.686 | | |
| | -3045 | 236.6 | 3832.6 | | | | T3063 | 3574 | 24'-26' | | | | 0.050 | 1.714 | | |
| | -3045 | 235.2 | 3831.2 | | | | T3064 | 3575 | 26'-28' | | | | 0.010 | 0.343 | | |
| | -3045 | 233.8 | 3829.8 | | | | T3065 | 3576 | 28'-30' | | | | 0.020 | 0.686 | | |
| | -3045 | 232.4 | 3828.4 | | | | T3066 | 3577 | 30'-32' | | | | 0.010 | 0.343 | | |
| | -3045 | 231.0 | 3827.0 | | | | T3067 | 3578 | 32'-34' | | | | 0.020 | 0.686 | | |
| | -3045 | 229.5 | 3825.5 | | | | T3068 | 3579 | 34'-36' | | | | 0.030 | 1.029 | | |
| | -3045 | 228.1 | 3824.1 | | | | T3069 | 3580 | 36'-38' | | | | 0.010 | 0.343 | | |
| | -3045 | 226.7 | 3822.7 | | | | T3070 | 3581 | 38'-40' | | | | 0.010 | 0.343 | | |
| | -3045 | 225.3 | 3821.3 | | | | T3071 | 3582 | 40'-42' | | | | 0.010 | 0.343 | | |
| | -3045 | 223.9 | 3819.9 | | | | T3072 | 3583 | 42'-44' | | | | 0.010 | 0.343 | | |
| | -3045 | 222.5 | 3818.5 | | | | T3073 | 3584 | 44'-46' | | | | 0.010 | 0.343 | | |
| | -3045 | 221.1 | 3817.1 | | | | T3074 | 3585 | 46'-48' | | | | 0.010 | 0.343 | | |
| | -3045 | 219.7 | 3815.6 | | | | T3075 | 3586 | 48'-50' | | | | 0.010 | 0.343 | | |
| | -3045 | 218.2 | 3814.2 | | | | T3076 | 3587 | 50'-52' | | | | 0.010 | 0.343 | | |
| | -3045 | 216.8 | 3812.8 | | | | T3077 | 3588 | 52'-54' | | | | 0.010 | 0.343 | | |
| | -3045 | 215.4 | 3811.4 | | | | T3078 | 3589 | 54'-56' | | | | 0.010 | 0.343 | | |
| | -3045 | 214.0 | 3810.0 | | | | T3079 | 3590 | 56'-58' | | | | 0.020 | 0.686 | | |
| | -3045 | 212.6 | 3808.6 | | | | T3080 | 3591 | 58'-60' | | | | 0.010 | 0.343 | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -3045 | 211.2 | 3807.2 | | | | T3081 | 3592 | 60'-62' | | | | 0.010 | 0.343 | | |
| | -3045 | 209.8 | 3805.8 | | | | T3082 | 3593 | 62'-64' | | | | 0.010 | 0.343 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-31 | 3050S | 90W | 3877.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -3050 | 88.6 | 3875.6 | | | | T3022 | 3528 | 0'-2' | | | | 0.020 | 0.686 | | |
| | -3050 | 87.2 | 3874.2 | | | | T3023 | 3529 | 2'-4' | | | | tr. | 0.000 | | |
| | -3050 | 85.8 | 3872.8 | | | | T3024 | 3530 | 4'-6' | | | | tr. | 0.000 | | |
| | -3050 | 84.3 | 3871.3 | | | | T3025 | 3531 | 6'-8' | | | | tr. | 0.000 | | |
| | -3050 | 82.9 | 3869.9 | | | | T3026 | 3532 | 8'-10' | | | | 0.010 | 0.343 | | |
| | -3050 | 81.5 | 3868.5 | | | | T3027 | 3533 | 10'-12' | | | | 0.010 | 0.343 | | |
| | -3050 | 80.1 | 3867.1 | | | | T302B | 3534 | 12'-14' | | | | 0.010 | 0.343 | | |
| | -3050 | 78.7 | 3865.7 | | | | T3029 | 3535 | 14'-16' | | | | 0.010 | 0.343 | | |
| | -3050 | 77.3 | 3864.3 | | | | T3030 | 3536 | 16'-18' | | | | 0.010 | 0.343 | | |
| | -3050 | 75.9 | 3862.9 | | | | T3031 | 3537 | 18'-20' | | | | 0.010 | 0.343 | | |
| | -3050 | 74.4 | 3861.4 | | | | T3032 | 3538 | 20'-22' | | | | 0.010 | 0.343 | | |
| | -3050 | 73.0 | 3860.0 | | | | T3033 | 3539 | 22'-24' | | | | tr. | 0.000 | | |
| | -3050 | 71.6 | 3858.6 | | | | T3034 | 3540 | 24'-26' | | | | tr. | 0.000 | | |
| | -3050 | 70.2 | 3857.2 | | | | T3035 | 3541 | 26'-28' | | | | 0.010 | 0.343 | | |
| | 3050 | 68.8 | 3855.8 | | | | T3036 | 3542 | 28'-30' | | | | 0.010 | 0.343 | | |
| | -3050 | 67.4 | 3854.4 | | | | T3037 | 3543 | 30'-32' | | | | 0.040 | 1.371 | | |
| | -3050 | 66.0 | 3853.0 | | | | T3038 | 3544 | 32'-34' | | | | 0.570 | 19.543 | | |
| | -3050 | 64.5 | 3851.5 | | | | T3039 | 3545 | 34'-36' | | | | 0.020 | 0.686 | | |
| | -3050 | 63.1 | 3850.1 | | | | T3040 | 3546 | 36'-38' | | | | 0.020 | 0.686 | | |
| | -3050 | 61.7 | 3848.7 | | | | T3041 | 3547 | 38'-40' | | | | 0.010 | 0.343 | | |
| | -3050 | 60.3 | 3847.3 | | | | T3042 | 3548 | 40'-42' | | | | tr. | 0.000 | | |
| | -3050 | 58.9 | 3845.9 | | | | T304;; | 3549 | 42'-44' | | | | 0.010 | 0.343 | | |
| | -3050 | 57.5 | 3844.5 | | | | T3044 | 3550 | 44'-46' | | | | 0.010 | 0.343 | | |
| | -3050 | 56.1 | 3843.1 | | | | T3045 | 3551 | 46'-48' | | | | 0.010 | 0.343 | | |
| | -3050 | 54.7 | 3841.6 | | | | T3046 | 3552 | 48'-50' | | | | 0.010 | 0.343 | | |
| | -3050 | 53.2 | 3840.2 | | | | T3047 | 3553 | 50'-52' | | | | 0.010 | 0.343 | | |
| | -3050 | 51.8 | 3838.8 | | | | T3048 | 3554 | 52'-54' | | | | 0.040 | 1.371 | | |
| | -3050 | 50.4 | 3837.4 | | | | T3049 | 3555 | 54'-56' | | | | 0.010 | 0.343 | | |
| | -3050 | 49.0 | 3836.0 | | | | T3050 | 3556 | 56'-58' | | | | 0.220 | 7.543 | | |
| | -3050 | 47.6 | 3834.6 | | | | T3051 | 3557 | 58'-60' | | | | 0.010 | 0.343 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-19 | 3070S | 190W | 3870.0 | 0 | -90 | 10' | | | | | | | | | | |
| | -3070 | 190 | 3865.0 | | | | T2896 | 3396 | 0'-5' | | | | 0.030 | 1.029 | | |
| | -3070 | 190 | 3860.0 | | | | T2897 | 3397 | 5'-10' | | | | 0.180 | 6.171 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-27 | 3070S | 220W | 3854.0 | 118 | -45 | 36' | | | | | | | | | | |
| | -3070 | 218.6 | 3852.6 | | | | T3124 | 3635 | 0'-2' | | | | 0.010 | 0.343 | | |
| | -3070 | 217.2 | 3851.2 | | | | T3125 | 3636 | 2'-4' | | | | 0.010 | 0.343 | | |
| | -3070 | 215.8 | 3849.8 | | | | T3126 | 3637 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3070 | 214.3 | 3848.3 | | | | T3127 | 3638 | 6'-8' | | | | 0.010 | 0.343 | | |
| | -3070 | 212.9 | 3846.9 | | | | T3128 | 3639 | 8'-10' | | | | 0.010 | 0.343 | | |
| | -3070 | 211.5 | 3845.5 | | | | T3129 | 3640 | 10'-12' | | | | 0.010 | 0.343 | | |
| | -3070 | 210.1 | 3844.1 | | | | T3130 | 3641 | 12'-14' | | | | 0.010 | 0.343 | | |
| | -3070 | 208.7 | 3842.7 | | | | T3131 | 3642 | 14'-16' | | | | 0.010 | 0.343 | | |
| | -3070 | 207.3 | 3841.3 | | | | T3132 | 3043 | 16'-18' | | | | 0.010 | 0.343 | | |
| | -3070 | 205.9 | 3839.9 | | | | T3133 | 3644 | 18'-20' | | | | 0.010 | 0.343 | | |
| | -3070 | 204.4 | 3838.4 | | | | T3134 | 3645 | 20'-22' | | | | 0.010 | 0.343 | | |
| | -3070 | 203.0 | 3837.0 | | | | T3135 | 3646 | 22'-24' | | | | 0.010 | 0.343 | | |
| | -3070 | 201.6 | 3835.6 | | | | T3136 | 3647 | 24'-26' | | | | 0.010 | 0.343 | | |
| | -3070 | 200.2 | 3834.2 | | | | T3137 | 3648 | 26'-28' | | | | 0.010 | 0.343 | | |
| | -3070 | 198.8 | 3832.8 | | | | T3138 | 3649 | 28'-30' | | | | 0.070 | 2.400 | | |
| | -3070 | 197.4 | 3831.4 | | | | T3139 | 3650 | 30'-32' | | | | 0.040 | 1.371 | | |
| | -3070 | 196.0 | 3830.0 | | | | T3140 | 3651 | 32'-34' | | | | 0.050 | 1.714 | | |
| | -3070 | 194.5 | 3828.5 | | | | T3141 | 3652 | 34'-36' | | | | 0.040 | 1.371 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-20 | 3100S | 200W | 3868.0 | 0 | -90 | 10' | | | | | | | | | | |
| | -3100 | 200.0 | | | | | T2898 | 3398 | 0'-5' | | | | 0.020 | 0.686 | | |
| | -3100 | 200.0 | | | | | T2899 | 3399 | 5'-10' | | | | 0.010 | 0.343 | | |
| | | | | | | | | | | | | | | | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM 1-28 | 3100S | 220W | 3858.0 | 118 | -45 | 12' | | | | | | | | | | |
| | -3100 | 218.6 | 3856.6 | | | | T3172 | 3683 | 0'-2' | | | | 0.030 | 1.029 | | |
| | -3100 | 217.2 | 3855.2 | | | | T3173 | 3684 | 2'-4' | | | | 0.030 | 1.029 | | |
| | -3100 | 215.8 | 3853.8 | | | | T3174 | 3685 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3100 | 214.3 | 3852.3 | | | | T3175 | 3686 | 6'-8' | | | | 0.020 | 0.686 | | |
| | -3100 | 212.9 | 3850.9 | | | | T3176 | 3687 | 8'-10' | | | | 0.020 | 0.686 | | |
| | -3100 | 211.5 | 3849.5 | | | | T3177 | 3688 | 10'-12' | | | | 0.040 | 1.371 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-29 | 3135S | 170W | 3866.0 | 332 | -45 | 60' | | | | | | | | | | |
| | -3135 | 168.6 | 3864.6 | | | | T2992 | 3492 | 0'-2' | | | | 0.010 | 0.343 | | |
| | -3135 | 167.2 | 3863.2 | | | | T2993 | 3493 | 2'-4' | | | | 0.010 | 0.343 | | |
| | -3135 | 165.8 | 3861.8 | | | | T2994 | 3494 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3135 | 164.3 | 3860.3 | | | | T2995 | 3495 | 6'-8' | | | | 0.010 | 0.343 | | |
| | -3135 | 162.9 | 3858.9 | | | | T2996 | 3496 | 8'-10' | | | | 0.010 | 0.343 | | |
| | -3135 | 161.5 | 3857.5 | | | | T2997 | 3497 | 10'-12' | | | | 0.010 | 0.343 | | |
| | -3135 | 160.1 | 3856.1 | | | | T2998 | 3498 | 12'-14' | | | | 0.010 | 0.343 | | |
| | -3135 | 158.7 | 3854.7 | | | | .T2999 | 3499 | 14'-16' | | | | 0.010 | 0.343 | | |
| | -3135 | 157.3 | 3853.3 | | | | T3000 | 3500 | 16'-18' | | | | 0.010 | 0.343 | | |
| | -3135 | 155.9 | 3851.9 | | | | T3001 | 3501 | 18'-20' | | | | 0.010 | 0.343 | | |
| | -3135 | 154.4 | 3850.4 | | | | T3002 | 3502 | 20'-22' | | | | 0.010 | 0.343 | | |
| | -3135 | 153.0 | 3849.0 | | | | T3003 | 3503 | 22'-24' | | | | 0.010 | 0.343 | | |
| | -3135 | 151.6 | 3847.6 | | | | T3004 | 3504 | 24'-26' | | | | 0.010 | 0.343 | | |
| | -3135 | 150.2 | 3846.2 | | | | T3005 | 3505 | 26'-28' | | | | 0.020 | 0.686 | | |
| | -3135 | 148.8 | 3844.8 | | | | T3006 | 3506 | 28'-30' | | | | 0.010 | 0.343 | | |
| | -3135 | 147.4 | 3843.4 | | | | T3007 | 3507 | 30'-32' | | | | tr. | 0.000 | | |
| | -3135 | 146.0 | 3842.0 | | | | T3008 | 3508 | 32'-34' | | | | 0.010 | 0.343 | | |
| | -3135 | 144.5 | 3840.5 | | | | T3009 | 3509 | 34'-36' | | | | 0.010 | 0.343 | | |
| | -3135 | 143.1 | 3839.1 | | | | T3010 | 3510 | 36'-38' | | | | 0.010 | 0.343 | | |
| | -3135 | 141.7 | 3837.7 | | | | T3011 | 3511 | 38'-40' | | | | 0.010 | 0.343 | | |
| | -3135 | 140.3 | 3836.3 | | | | T3012 | 3512 | 40'-42' | | | | 0.010 | 0.343 | | |
| | -3135 | 138.9 | 3834.9 | | | | T3013 | 3513 | 42'-44' | | | | 0.010 | 0.343 | | |
| | -3135 | 137.5 | 3833.5 | | | | T3014 | 3514 | 44'-46' | | | | tr. | 0.000 | | |
| | -3135 | 136.1 | 3832.1 | | | | T3015 | 3515 | 46'-48' | | | | 0.010 | 0.343 | | |
| | -3135 | 134.7 | 3830.6 | | | | T3016 | 3516 | 48'-50' | | | | 0.010 | 0.343 | | |
| | -3135 | 133.2 | 3829.2 | | | | T3017 | 3517 | 50'-52' | | | | 0.010 | 0.343 | | |
| | -3135 | 131.8 | 3827.8 | | | | T3018 | 3518 | 52'-54' | | | | 0.010 | 0.343 | | |
| | -3135 | 130.4 | 3826.4 | | | | T3019 | 3519 | 54'-56' | | | | 0.010 | 0.343 | | |
| | -3135 | 129.0 | 3825.0 | | | | T3020 | 3520 | 56'-58' | | | | tr. | 0.000 | | |
| | -3135 | 127.6 | 3820.6 | | | | T3021 | 3521 | 58'-60' | | | | tr. | 0.000 | | |
| | | | | | | | | | | | | | | | | |
| CEM 1-30 | 3169S | 220W | 3850.0 | 118 | -45 | 66' | | | | | | | | | | |
| | -3169 | 218.6 | 3848.6 | | | | T3093 | 3604 | 0'-2' | | | | 0.040 | 1.371 | | |
| | -3169 | 217.2 | 3847.2 | | | | T3094 | 3605 | 2'-4' | | | | 0.010 | 0.343 | | |
| | -3169 | 215.8 | 3845.8 | | | | T3095 | 3606 | 4'-6' | | | | 0.010 | 0.343 | | |
| | -3169 | 214.3 | 3844.3 | | | | T3096 | 3607 | 6'-8' | | | | 0.010 | 0.343 | | |
| | -3169 | 212.9 | 3842.9 | | | | T3097 | 3608 | 8'-10' | | | | 0.380 | 13.029 | | |
| | -3169 | 211.5 | 3841.5 | | | | T3098 | 3609 | 10'-12' | | | | 0.240 | 8.229 | | |
| | -3169 | 210.1 | 3840.1 | | | | T3099 | 3610 | 12'-14' | | | | 0.070 | 2.400 | | |
| | -3169 | 208.7 | 3838.7 | | | | T3100 | 3611 | 14'-16' | | | | 0.020 | 0.686 | | |
| | -3169 | 207.3 | 3837.3 | | | | T3101 | 3612 | 16'-18' | | | | 0.060 | 2.057 | | |
| | -3169 | 205.9 | 3835.9 | | | | T3102 | 3613 | 18'-20' | | | | 0.020 | 0.686 | | |
| | -3169 | 204.4 | 3834.4 | | | | T3103 | 3614 | 20'-22' | | | | 0.020 | 0.686 | | |
| | -3169 | 203.0 | 3833.0 | | | | T3104 | 3615 | 22'-24' | | | | 0.020 | 0.686 | | |
| | -3169 | 201.6 | 3831.6 | | | | T3105 | 3616 | 24'-26' | | | | 0.020 | 0.686 | | |
| | -3169 | 200.2 | 3830.2 | | | | T3106 | 3617 | 26'-28' | | | | 0.010 | 0.343 | | |
| | -3169 | 198.8 | 3828.8 | | | | T3107 | 3618 | 28'-30' | | | | 0.020 | 0.686 | | |
| | -3169 | 197.4 | 3827.4 | | | | T3108 | 3619 | 30'-32' | | | | 0.010 | 0.343 | | |
| | -3169 | 196.0 | 3826.0 | | | | T3109 | 3620 | 32'-34' | | | | 0.010 | 0.343 | | |
| | -3169 | 194.5 | 3824.5 | | | | T3110 | 3621 | 34'-36' | | | | 0.010 | 0.343 | | |
| | -3169 | 193.1 | 3823.1 | | | | T3111 | 3622 | 36'-38' | | | | 0.010 | 0.343 | | |
| | -3169 | 191.7 | 3821.7 | | | | T3112 | 3623 | 38'-40' | | | | 0.010 | 0.343 | | |
| | -3169 | 190.3 | 3820.3 | | | | T3113 | 3624 | 40'-42' | | | | tr. | 0.000 | | |
| | -3169 | 188.9 | 3818.9 | | | | T3114 | 3625 | 42'-44' | | | | tr. | 0.000 | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| | -3169 | 187.5 | 3817.5 | | | | T3115 | 3626 | 44'-46' | | | | 0.110 | **3.771** | | |
| | -3169 | 186.1 | 3816.1 | | | | T3116 | 3627 | 46'-48' | | | | tr. | 0.000 | | |
| | -3169 | 184.7 | 3814.6 | | | | T3117 | 3628 | 48'-50' | | | | 0.010 | 0.343 | | |
| | -3169 | 183.2 | 3813.2 | | | | T3118 | 3629 | 50'-52' | | | | 0.010 | 0.343 | | |
| | -3169 | 181.8 | 3811.8 | | | | T3119 | 3630 | 52'-54' | | | | 0.010 | 0.343 | | |
| | -3169 | 180.4 | 3810.4 | | | | T3120 | 3631 | 54'-56' | | | | 0.020 | **0.686** | | |
| | -3169 | 179.0 | 3809.0 | | | | T3121 | 3632 | 56'-58' | | | | 0.010 | 0.343 | | |
| | -3169 | 177.6 | 3807.6 | | | | T3122 | 3633 | 58'-60' | | | | 0.030 | **1.029** | | |
| | -3169 | 173.4 | 3803.4 | | | | T3123 | 3634 | 60'-66' | | | | | | | |

| | | |
|---|---|---|
| Color coding: | 0.50 to 0.99 g/T Au | **yellow** |
| | 1.00 to 2.99 g/T Au | **orange** |
| | 3.00 g/T Au or greater | **red** |

## Geologic Explanation for Appendices B, C, D & E

**Type (Rock Type).**

BX – Breccia (Stage II through Stage IV breccias (commonly with overprinting of later re-brecciation or Stage V & VI veins)

FW – Footwall (adamellite)

HW – Hanging wall (adamellite)

VN – Fissure Vein, including Stage V & VI

**Alt (Hydrothermal Alteration): (A) dominant breccia matrix mineralogy or (B) alteration zone represented in sample.**

| | | |
|---|---|---|
| (A) | QC – quartz-chlorite | Stage III matrix (with adularia) |
| | OCP – quartz-chlorite-pyrite | Stage III matrix |
| | QS – quartz-sericite | Stage IV matrix (with illite) |
| | QSP – quartz-sericite-pyrite | Stage IV matrix |
| | QCS – quartz-chlorite-sericite | Stage III & IV with overprint |
| | QCSP – quartz-chlorite-sericite-pyrite | Stage III & IV + pyrite |
| (B) | Ain – argillic (inner) | montmorillinite-sericite±kaolinite |
| | Aout – argillic (outer) | montmorillinite-illite-chlorite |
| | Pin – propylitic (inner) | chlorite-montmorillinite zone |
| | Pout – propylitic (outer) | chlorite-epidote zone |

**Min (Mineralogy): Fissure vein mineralogy as logged in drill cuttings in (A) Telegraph-type veins and (B) other veins or supergene byproducts in fractures.**

| | | |
|---|---|---|
| (A) | Qcmn – quartz-manganese oxide-calcite | Stage IV vein |
| | Qfn – quartz fine grained | Stage V vein (with adularia) |
| | Qfnp – quartz fine grained + pyrite | Stage V vein |
| | Qs – quartz stockwork | Stage V "crackle breccia" cement |
| | Qvg – quartz, vuggy texture | Stage V, coarse-grained phase |
| (B) | CuO – Copper oxides | includes all supergene Cu minerals |
| | FeO – iron oxides | all conspicuous oxides & hydroxides |
| | Goss – gossan | oxidized high-sulfide vein (±quartz) |
| | QFe – quartz iron oxides | veinlets of unknown origin |
| | Qmp – quartz-massive + pyrite | early "Bull" quartz veins |
| | 0 – no vein material | |

# Appendix D

**Northern Extension (Telegraph Extension Claim) Area Drill Data**

| Appendix D. Northern Extension (Telegraph Extension Claim) Area Drill Data. | | | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM N-10 | 270N | 390W | 3827.0 | 68 | -45 | 60' | | | | | | | | | | |
| | 273.3 | 387.4 | 3822.8 | | | | 10-0 | T107 | 0'-6' | | | | | | | |
| | 276.6 | 384.7 | 3818.5 | | | | 10-6 | T108 | 6'-12' | | | | | | | |
| | 279.9 | 382.1 | 3814.3 | | | | 10-12 | T109 | 12'-18' | | | | | | | |
| | 283.2 | 379.4 | 3810.0 | | | | 10-18 | T110 | 18'-24' | | | | | | | |
| | 286.5 | 376.8 | 3805.8 | | | | 10-24 | T111 | 24'-30' | | | | | | | |
| | 289.8 | 374.1 | 3801.5 | | | | 10-30 | T112 | 30'-36' | | | | | | | |
| | 293.0 | 371.5 | 3797.3 | | | | 10-36 | T113 | 36'-42' | | | | 0.034 | 1.166 | 0.05 | 1.714 |
| | 296.3 | 368.8 | 3793.1 | | | | 10-42 | T114 | 42'-48' | | | | 0.034 | 1.166 | 0.05 | 1.714 |
| | 299.6 | 366.2 | 3788.8 | | | | 10-48 | T115 | 48'-54' | | | | 0.015 | 0.514 | 0.05 | 1.714 |
| | 302.9 | 363.5 | 3784.6 | | | | 10-54 | T116 | 54'-60' | | | | 0.005 | 0.171 | 0.05 | 1.714 |
| | | | | | | | | | | | | | | | | |
| CEM N-9 | 202N | 285W | 3835.0 | 31 | -45 | 12' | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| CEM N-8 | 202N | 285W | 3835.0 | 78 | -45 | 60' | | | | | | | | | | |
| | 204.6 | 281.7 | 3830.8 | | | | 8-0 | T97 | 0'-6' | | | | | | | |
| | 207.3 | 278.4 | 3826.5 | | | | 8-6 | T98 | 6'-12' | Hw | Pout | 0 | | | | |
| | 209.9 | 275.1 | 3822.3 | | | | 8-12 | T99 | 12'-18' | Hw | Pout | 0 | | | | |
| | 212.6 | 271.8 | 3818.0 | | | | 8-18 | T100 | 18'-24' | Hw | Pout | 0 | | | | |
| | 215.2 | 268.5 | 3813.8 | | | | 8-24 | T101 | 24'-30' | Hw | Pout | 0 | 0.020 | 0.686 | tr. | 0.000 |
| | 217.9 | 265.2 | 3809.5 | | | | 8-30 | T102 | 30'-36' | Vn | Pout | Qvgp | 0.033 | 1.131 | 0.05 | 1.714 |
| | 220.5 | 262.0 | 3805.3 | | | | 8-36 | T103 | 36'-42' | vn | Pout | Qvgp | 0.032 | 1.097 | 0.05 | 1.714 |
| | 223.2 | 258.7 | 3801.1 | | | | 8-42 | T104 | 42'-48' | Hw | Pout | 0 | 0.034 | 1.166 | 0.05 | 1.714 |
| | 225.8 | 255.4 | 3796.8 | | | | 8-48 | T105 | 48'-54' | Bw | Pout | 0 | 0.030 | 1.029 | 0.05 | 1.714 |
| | 228.5 | 252.1 | 3792.6 | | | | 8-54 | T106 | 54'-60' | Hw | Pout | Qvgp | 0.044 | 1.509 | 0.05 | 1.714 |
| | | | | | | | | | | | | | | | | |
| CEM N-11 | 102N | 120W | 3847.0 | 105 | -45 | 60' | | | | | | | | | | |
| | 103.0 | 115.9 | 3842.8 | | | | 11-0 | T117 | 0'-6' | | | | | | | |
| | 103.9 | 111.7 | 3838.5 | | | | 11-12 | T118 | 12'-18' | | | | | | | |
| | 104.9 | 107.6 | 3834.3 | | | | 11-18 | T119 | 18'-24' | | | | | | | |
| | 105.8 | 103.5 | 3830.0 | | | | 11-24 | T120 | 24'-30' | | | | | | | |
| | 106.8 | 99.3 | 3825.8 | | | | 11-30 | T121 | 30'-36' | | | | 0.005 | 0.171 | 0.05 | 1.714 |
| | 107.7 | 95.2 | 3821.5 | | | | 11-36 | T122 | 36'-42' | | | | 0.016 | 0.549 | 0.05 | 1.714 |
| | 108.7 | 91.1 | 3817.3 | | | | 11-42 | T123 | 42'-48' | | | | | | | |
| | 109.6 | 86.9 | 3813.1 | | | | 11-48 | T124 | 48'-54' | | | | | | | |
| | 110.6 | 82.7 | 3808.9 | | | | 11-54 | T125 | 54'-60' | | | | | | | |
| | | | | | | | | | | | | | | | | |
| CEM N-7 | 25N | 155W | 3842.0 | 133 | -45 | 60' | | | | | | | | | | |
| | 21.7 | 142.7 | 3829.3 | | | | 7-12 | T89 | 12'-18' | | | | | | | |
| | 20.6 | 138.6 | 3825.0 | | | | 7-18 | T90 | 18'-24' | | | | | | | |
| | 19.5 | 134.5 | 3820.8 | | | | 7-24 | T91 | 24'-30' | | | | | | | |
| | 18.4 | 130.4 | 3816.5 | | | | 7-30 | T92 | 30'-36' | | | | 0.038 | 1.303 | tr. | 0.000 |
| | 17.3 | 126.3 | 3812.3 | | | | 7-36 | T93 | 36'-42' | | | | 0.018 | 0.617 | tr. | 0.000 |
| | 16.2 | 122.2 | 3808.1 | | | | 7-42 | T94 | 42'-48' | | | | 0.012 | 0.411 | 0.05 | 1.714 |
| | 15.1 | 118.1 | 3803.8 | | | | 7-48 | T95 | 48'-54' | | | | 0.008 | 0.274 | 0.05 | 1.714 |
| | 14.0 | 114.0 | 3799.6 | | | | 7-54 | T96 | 54'-60' | | | | 0.006 | 0.206 | 0.05 | 1.714 |
| | | | | | | | | | | | | | | | | |
| CEM N-6 | 75S | 175W | 3843.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -75 | 153.8 | 3821.8 | | | | | T83 | 24'-30' | | | | | | | |
| | -75 | 149.5 | 3817.5 | | | | | T84 | 30'-36' | | | | | | | |
| | -75 | 145.3 | 3813.3 | | | | | T85 | 36'-42' | | | | 0.012 | 0.411 | 0.05 | 1.714 |
| | -75 | 141.1 | 3809.1 | | | | | T86 | 42'-48' | | | | 0.020 | 0.686 | 0.05 | 1.714 |
| | -75 | 136.8 | 3804.8 | | | | 6-48 | T87 | 48'-54' | | | | | | | |
| | -75 | 132.6 | 3800.6 | | | | 6-54 | T88 | 54'-60' | | | | | | | |
| | | | | | | | | | | | | | | | | |
| CEM N-4 | 200S | 234W | 3837.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -200 | 212.8 | 3815.8 | | | | 4-24 | T72 | 24'-30' | | | | tr. | 0.000 | 0.14 | 4.800 |
| | -200 | 204.3 | 3807.3 | | | | 4-36 | T73 | 36'-42' | | | | 0.015 | 0.514 | tr. | 0.000 |
| | -200 | 200.1 | 3803.1 | | | | 4-42 | T74 | 42'-48' | | | | 0.025 | 0.857 | tr. | 0.000 |
| | -200 | 195.8 | 3798.8 | | | | 4-48 | T75 | 48'-54' | | | | 0.045 | 1.543 | tr. | 0.000 |
| | -200 | 191.6 | 3794.6 | | | | 4-54 | T76 | 54'-60' | | | | 0.013 | 0.446 | tr. | 0.000 |
| | | | | | | | | | | | | | | | | |

| CEM Drill Hole No. | Collar | | | | | | Sample | | | Geo. Log (Lange) | | | Analyses | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Depth (ft) | FieldNo. | Lab No. | Length (feet) | Type | Alt | Min | Au (opt) | Au (g/T) (calc.) | Ag (opt) | Ag (g/T) (calc.) |
| CEM N-5 | 200S | 225W | 3838.0 | 118 | -60 | 60 | | | | | | | | | | |
| | -200 | 210.0 | 3823.0 | | | | 5-24 | T77 | 24'-30' | | | | tr. | 0.000 | 0.17 | 5.829 |
| | -200 | 207.0 | 3820.0 | | | | 5-30 | T78 | 30'-36' | | | | 0.017 | 0.583 | tr. | 0.000 |
| | -200 | 204.0 | 3817.0 | | | | 5-36 | T79 | 36'-42' | | | | 0.005 | 0.171 | tr. | 0.000 |
| | -200 | 201.0 | 3814.0 | | | | 5-42 | T80 | 42'-48' | | | | tr. | 0.000 | 0.05 | 1.714 |
| | -200 | 198.0 | 3811.0 | | | | 5-48 | T81 | 48'-54' | | | | 0.028 | 0.960 | 0.13 | 4.457 |
| | -200 | 195.0 | 3808.0 | | | | 5-54 | T82 | 54'-60' | | | | 0.036 | 1.234 | 0.10 | 3.429 |
| | | | | | | | | | | | | | | | | |
| CEM N-3 | 300S | 332W | 3836.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -300 | 315.0 | 3819.0 | | | | 3-12 | T67 | 12'-24' | Hw | Aout | 0 | tr. | 0.000 | tr. | 0.000 |
| | -300 | 310.8 | 3814.8 | | | | 3-24 | T68 | 24'-30' | Hw | Aout | Qfn | tr. | 0.000 | tr. | 0.000 |
| | -300 | 306.5 | 3810.5 | | | | 3-30 | T69 | 30'-36' | Bx | QSP | Qfn | 0.065 | 2.229 | 0.53 | 18.171 |
| | -300 | 302.3 | 3806.3 | | | | 3-36 | T70 | 36'-42' | Fw | Aout | Qfn | 0.014 | 0.480 | 0.66 | 22.629 |
| | -300 | 298.1 | 3802.1 | | | | 3-42 | T71 | 42'-48' | Fw | Pout | Qfn | | | | |
| | | | | | | | | | | | | | | | | |
| CEM N-1 | 350S | 225W | 3837.0 | 118 | -45 | 60' | | | | | | | | | | |
| | -350 | 215.1 | 3827.1 | | | | | T135 | 12'-14' | Hw | Pin | 0 | 0.030 | 1.029 | 0.05 | 1.714 |
| | -350 | 213.7 | 3825.7 | | | | | T136 | 14'-16' | Bx | QC | Qvg | 0.104 | 3.566 | 0.05 | 1.714 |
| | -350 | 212.3 | 3824.3 | | | | | T137 | 16'-18' | Bx | QSP | Qfn | 0.020 | 0.686 | 0.05 | 1.714 |
| | -350 | 210.9 | 3822.9 | | | | | T138 | 18'-20' | Bx | QSP | Qfn | 0.028 | 0.960 | 0.05 | 1.714 |
| | -350 | 209.4 | 3821.4 | | | | | T139 | 20'-22' | Vn | 0 | Qfn | 0.060 | 2.057 | 0.05 | 1.714 |
| | -350 | 208.0 | 3820.0 | | | | | T140 | 22'-24' | Vn | QSP | Qfn | 0.294 | 10.080 | 0.19 | 6.514 |
| | -350 | 206.6 | 3818.6 | | | | | T141 | 24'-26' | Fw | Pin | 0 | 0.100 | 3.429 | 0.05 | 1.714 |
| | -350 | 205.2 | 3817.2 | | | | | T142 | 26'-28' | Vn | QSP | Qfn | 0.044 | 1.509 | 0.05 | 1.714 |
| | -350 | 203.8 | 3815.8 | | | | | T143 | 32'-36' | Fw | Pout | 0 | 0.005 | 0.171 | 0.05 | 1.714 |
| | -350 | 186.8 | 3798.8 | | | | | T145H | 52'-54' | | | | 0.060 | 2.057 | 0.29 | 9.943 |
| | -350 | 185.4 | 3797.4 | | | | | T145I | 54'-56' | | | | 0.030 | 1.029 | 0.05 | 1.714 |
| | -350 | 184.0 | 3796.0 | | | | | T145J | 56'-58' | | | | 0.055 | 1.886 | 0.10 | 3.429 |
| | -350 | 182.6 | 3794.6 | | | | | T145K | 58'-60' | | | | 0.040 | 1.371 | 0.05 | 1.714 |
| | | | | | | | | | | | | | | | | |
| CEM N-13 | 350S | 216W | 3839.0 | 118 | -45 | 30' | | | | | | | | | | |
| | -350 | 214.6 | 3837.6 | | | | T2517 | 2042 | 0'-2' | | | | 0.050 | 1.714 | 0.49 | 16.800 |
| | -350 | 213.2 | 3836.2 | | | | T2518 | 2043 | 2'-4' | | | | 0.090 | 3.086 | 0.59 | 20.229 |
| | -350 | 211.8 | 3834.8 | | | | T2519 | 2044 | 4'-6' | | | | 0.030 | 1.029 | 0.05 | 1.714 |
| | -350 | 210.3 | 3833.3 | | | | T2520 | 2045 | 6'-8' | | | | 0.050 | 1.714 | 0.23 | 7.886 |
| | -350 | 208.9 | 3831.9 | | | | T2521 | 2046 | 8'-10' | | | | 0.080 | 2.743 | 0.13 | 4.457 |
| | -350 | 207.5 | 3830.5 | | | | T2522 | 2047 | 10'-12' | | | | 0.040 | 1.371 | 0.22 | 7.543 |
| | -350 | 206.1 | 3829.1 | | | | T2523 | 2048 | 12'-14' | | | | 0.020 | 0.686 | 0.20 | 6.857 |
| | -350 | 204.7 | 3827.7 | | | | T2524 | 2049 | 14'-16' | | | | 0.050 | 1.714 | 0.30 | 10.286 |
| | -350 | 203.3 | 3826.3 | | | | T2525 | 2050 | 16'-18' | | | | 0.030 | 1.029 | 0.27 | 9.257 |
| | -350 | 201.9 | 3824.9 | | | | T2526 | 2051 | 18'-20' | | | | 0.030 | 1.029 | 0.39 | 13.371 |
| | -350 | 200.4 | 3823.4 | | | | T2527 | 2052 | 20'-22' | | | | 0.110 | 3.771 | 0.66 | 22.629 |
| | -350 | 199.0 | 3822.0 | | | | T2528 | 2053 | 22'-24' | | | | 0.070 | 2.400 | 0.23 | 7.886 |
| | -350 | 197.6 | 3820.6 | | | | T2529 | 2054 | 24'-26' | | | | 0.070 | 2.400 | 0.16 | 5.486 |
| | -350 | 196.2 | 3819.2 | | | | T2530 | 2055 | 26'-28' | | | | 0.020 | 0.686 | 0.09 | 3.086 |
| | -350 | 194.8 | 3817.8 | | | | T2531 | 2056 | 28'-30' | | | | 0.020 | 0.686 | 0.05 | 1.714 |
| | | | | | | | | | | | | | | | | |
| CEM N-12 | 500S | 225W | 3835.0 | 118 | -45 | 66' | | | | | | | | | | |
| | -500 | 216.5 | 3826.5 | | | | 12-12 | T126 | 12'-18' | | | | | | | |
| | -500 | 212.3 | 3822.3 | | | | 12-18 | T127 | 18'-24' | | | | | | | |
| | -500 | 208.0 | 3818.0 | | | | 12-24 | T128 | 24'-30' | | | | | | | |
| | -500 | 203.8 | 3813.8 | | | | 12-30 | T129 | 30'-36' | | | | 0.078 | 2.674 | 0.05 | 1.714 |
| | -500 | 199.5 | 3809.5 | | | | 12-36 | T130 | 36'-42' | | | | 0.014 | 0.480 | 0.05 | 1.714 |
| | -500 | 195.3 | 3805.3 | | | | 12-42 | T131 | 42'-48' | | | | 0.042 | 1.440 | 0.05 | 1.714 |
| | -500 | 191.1 | 3801.1 | | | | 12-48 | T132 | 48'-54' | | | | | | | |
| | -500 | 186.8 | 3796.8 | | | | 12-54 | T133 | 54'-60' | | | | | | | |
| | -500 | 182.6 | 3792.6 | | | | 12-60 | T134 | 60'-66' | | | | | | | |

Color coding:

| | | |
|---|---|---|
| 0.50 to 0.99 g/T Au | **yellow** |
| 1.00 to 2.99 g/T Au | **orange** |
| 3.00 g/T Au or greater | **red** |

# Geologic Explanation for Appendices B, C, D & E

**Type (Rock Type).**

BX – Breccia (Stage II through Stage IV breccias (commonly with overprinting of later re-brecciation or Stage V & VI veins)

FW – Footwall (adamellite)

HW – Hanging wall (adamellite)

VN – Fissure Vein, including Stage V & VI

**Alt (Hydrothermal Alteration): (A) dominant breccia matrix mineralogy or (B) alteration zone represented in sample.**

| | | |
|---|---|---|
| (A) | QC – quartz-chlorite | Stage III matrix (with adularia) |
| | OCP – quartz-chlorite-pyrite | Stage III matrix |
| | QS – quartz-sericite | Stage IV matrix (with illite) |
| | QSP – quartz-sericite-pyrite | Stage IV matrix |
| | QCS – quartz-chlorite-sericite | Stage III & IV with overprint |
| | QCSP – quartz-chlorite-sericite-pyrite | Stage III & IV + pyrite |
| (B) | Ain – argillic (inner) | montmorillinite-sericite±kaolinite |
| | Aout – argillic (outer) | montmorillinite-illite-chlorite |
| | Pin – propylitic (inner) | chlorite-montmorillinite zone |
| | Pout – propylitic (outer) | chlorite-epidote zone |

**Min (Mineralogy): Fissure vein mineralogy as logged in drill cuttings in (A) Telegraph-type veins and (B) other veins or supergene byproducts in fractures.**

| | | |
|---|---|---|
| (A) | Qcmn – quartz-manganese oxide-calcite | Stage IV vein |
| | Qfn – quartz fine grained | Stage V vein (with adularia) |
| | Qfnp – quartz fine grained + pyrite | Stage V vein |
| | Qs – quartz stockwork | Stage V “crackle breccia” cement |
| | Qvg – quartz, vuggy texture | Stage V, coarse-grained phase |
| (B) | CuO – Copper oxides | includes all supergene Cu minerals |
| | FeO – iron oxides | all conspicuous oxides & hydroxides |
| | Goss – gossan | oxidized high-sulfide vein (±quartz) |
| | QFe – quartz iron oxides | veinlets of unknown origin |
| | Qmp – quartz-massive + pyrite | early “Bull” quartz veins |
| | 0 – no vein material | |

# Geologic Explanation for Appendices B, C, D & E

**Type (Rock Type).**

BX – Breccia (Stage II through Stage IV breccias (commonly with overprinting of later re-brecciation or Stage V & VI veins)

FW – Footwall (adamellite)

HW – Hanging wall (adamellite)

VN – Fissure Vein, including Stage V & VI

**Alt (Hydrothermal Alteration): (A) dominant breccia matrix mineralogy or (B) alteration zone represented in sample.**

| | | |
|---|---|---|
| (A) | QC – quartz-chlorite | Stage III matrix (with adularia) |
| | OCP – quartz-chlorite-pyrite | Stage III matrix |
| | QS – quartz-sericite | Stage IV matrix (with illite) |
| | QSP – quartz-sericite-pyrite | Stage IV matrix |
| | QCS – quartz-chlorite-sericite | Stage III & IV with overprint |
| | QCSP – quartz-chlorite-sericite-pyrite | Stage III & IV + pyrite |
| (B) | Ain – argillic (inner) | montmorillinite-sericite±kaolinite |
| | Aout – argillic (outer) | montmorillinite-illite-chlorite |
| | Pin – propylitic (inner) | chlorite-montmorillinite zone |
| | Pout – propylitic (outer) | chlorite-epidote zone |

**Min (Mineralogy): Fissure vein mineralogy as logged in drill cuttings in (A) Telegraph-type veins and (B) other veins or supergene byproducts in fractures.**

| | | |
|---|---|---|
| (A) | Qcmn – quartz-manganese oxide-calcite | Stage IV vein |
| | Qfn – quartz fine grained | Stage V vein (with adularia) |
| | Qfnp – quartz fine grained + pyrite | Stage V vein |
| | Qs – quartz stockwork | Stage V “crackle breccia” cement |
| | Qvg – quartz, vuggy texture | Stage V, coarse-grained phase |
| (B) | CuO – Copper oxides | includes all supergene Cu minerals |
| | FeO – iron oxides | all conspicuous oxides & hydroxides |
| | Goss – gossan | oxidized high-sulfide vein (±quartz) |
| | QFe – quartz iron oxides | veinlets of unknown origin |
| | Qmp – quartz-massive + pyrite | early “Bull” quartz veins |
| | 0 – no vein material | |

# Appendix F

**OME 1986 Drill Data**

Appendix F OME 1968 Drilling

| Drill Hole No. | Collar | | | | | | | Sample | | Analysis | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | N-S | E-W | Elev. | Az. | Incl. | Drill Stem Depth | Vertical Depth (ft) | Field Note | Length (feet) | Au (opt) | Au (g/T) (calc) |
| OME-1 | -1085 | 465 | 3826 | 118 | -55 | | 182 | | | | |
| | -1085 | 427.3 | 3721 | | | | 103 | 129 | 1.4 | 0 | |
| | -1085 | 426 | 3720 | | | | 105 | | | | |
| | -1085 | 375 | 3701 | | | | 125 | 130 | 4.5 | 0 | |
| | -1085 | 371 | 3796 | | | | 129 | | | | |
| | -1085 | 359 | 2679 | | | | 148 | 130 | 3.1 | 0 | |
| | -1085 | 354 | 3674 | | | | 152 | | | | |
| | | | | | | | | | | | |
| OME-2 | -1320 | 487 | 3825 | 118 | -55 | 200 | 163 | | | | |
| | -1320 | 417 | 3727 | | | | 98 | 118 | 5 | 0.28 | 8.71 |
| | -1320 | 413 | 3722 | | | | 104 | 119 | | | |
| | -1320 | 383 | 3680 | | | | 150' | 120 | 4 | 0.08 | 2.49 |
| | | 381 | 3678 | | | | 154 | 121 | | | |
| | | 379 | 3675 | | | | | | | | |
| | | 376 | 3671 | | | | | | | | |
| | | | | | | | | | | | |
| OME-3 | -2273 | 494 | 3822 | 118 | -55 | 189 | 155 | | | | |
| | -2273 | 421 | 3717 | | | | 105 | 122 | 5 | 0 | |
| | -2273 | 416 | 3712 | | | | 110 | 2714 | | | |
| | | | | | | | | | | | |
| OME-4 | -2474 | 493 | 3826 | 118 | -55 | 192 | 158 | | | | |
| | -2474 | 412 | 3709 | | | | 116 | 123 | 3 | 0.2 | 6.22 |
| | -2474 | 410 | 3706 | | | | 120 | 125 | | | |
| | -2474 | 395 | 3684 | | | | 142 | 2715 | 5 | 0.18 | 5.6 |
| | -2474 | 392 | 3680 | | | | 146 | | | | |
| | | | | | | | | | | | |
| OME-5 | -2675 | 496 | 3830 | 118 | 55 | 192 | 157 | | | | |
| | -2675 | 396 | 3688 | | | | 142 | 127 | 6.7 | 0 | |
| | -2675 | 389 | 3679 | | | | 151 | 128 | | 0 | |
| | | | | | | | | | | | |
| OME-6 | -2980 | 480 | 3827 | 118 | 60 | 200 | 173 | | | | |
| | -2980 | 415 | 3703 | | | | 114.8 | 131 | 1.6 | 0 | |
| | -2980 | 414 | 3700 | | | | 117 | 132 | | 0 | |
| | -2980 | 402 | 3683 | | | | 139 | 133 | 5 | 0 | |
| | -2980 | 398 | 3777 | | | | 144.5 | | | | |
| | | | | | | | | | | | |
| OME-9 | -2362 | 336 | 3834 | 118 | 90 | 100 | 100 | | | | |
| | -2362 | 336 | 3776 | | | | 58.5 | 134-6 | 12 | 0.21 | 6.53 |
| | -2362 | 336 | 3757 | | | | 71.5 | | | | |
| | | | | | | | | | | | |
| OME-10 | -2560 | 343 | 3839 | 118 | 90 | 107.5 | 107.5 | | | | |
| | -2569 | 343 | 3744 | | | | 95 | 140-4 | 8 | 0.15 | |
| | -2560 | 343 | 3733 | | | | 106 | | | | |
| | | | | | | | | | | | |
| OME-12 | -3025 | 323 | 3841 | 118 | 75 | 91.5 | 88 | | | | |
| | -3025 | 314 | 3768 | | | | 72.6 | 2709-12 | 6 | 0.2 | |
| | -3025 | 301.5 | 3760 | | | | 81 | | | | |
| | | | | | | | | | | | |
| OME-14 | -1893 | 306 | 3841 | 118 | 60 | 80 | 69.5 | 2713 | 6 | 0 | |
| | -1893 | 269 | 3777 | | | | 63 | | | | |
| | -1893 | 265 | 3772 | | | | 69.5 | | | | |

Note: "0" sample result as shown in the assay column means the drill sample was incompetent and any assay result were not reliable. Tomo Ito, the supervising geologist made the following observation on page 7 of his Final Report to the OME,: "In most cases, drilling results were good, but the writer strongly feels that true information as to values contained is not obtainable in certain types of formation such as encountered at Telegraph. This is especially true when highly fractured vein material with powdered oxides of manganese and iron, together with soft, light carbonates (calcite and siderite) are encountered. This is the type of material most likely to carry high values.... Sludge samples submitted where core loss was especially high also may not indicate true values due to heavy dilution." Given the drilling technology that existed in 1968, the drilling process mechanically destroyed the bonding of the rock fragments that made up the brecciated vein sample exposing the surface of the original rock particles. Intense water or air pressure was required to lift the drill cuttings to the surface. In this process the gold deposited on the surface of the brecciated pieces was washed or blown away. The resulting sample was unrepresentative of the original values contained in the vein intercept.

# Appendix H

**Analytical Data from Truck Loads of Ore during the 1981-1982 Mining**

| Appendix H. Truck Load Sample Data | | | | | | |
|---|---|---|---|---|---|---|
| | Sample | | | | Analysis | |
| Truck Load No. | Lab No | Sample No | Tons | Pad Loc. | Au(oz) | Au(grams) |
| 1,3,5,7,9,11 | 2067 | 1 | 60 | | 0.14 | 4.80 |
| 2,4,6,8,10,12 | 2068 | 2 | 60 | | 0.57 | 19.54 |
| 13,17 | 2069 | 3 | 20 | 22 E | 0.10 | 3.43 |
| 18-23 | 2070 | 4 | 60 | 22 C | 0.15 | 5.14 |
| 36-48 | 2071 | 5 | 130 | 23 A & B | 0.16 | 5.49 |
| 49-53 | 2072 | 6 | 50 | 22,23 A | 0.11 | 3.77 |
| 54-60 | 2073 | 7 | 76 | 23 A | 0.06 | 2.06 |
| 61-75 | 2074 | 8 | 153.5 | 23 A | 0.16 | 5.49 |
| 76-91 | 2075 | 9 | 170 | | 0.33 | 11.31 |
| 92-101 | 2125 | 59 | 108 | 23 A & B | 0.12 | 4.11 |
| 102-111 | 2126 | 60 | 108 | 23 B | 0.10 | 3.43 |
| 112-121 | 2127 | 61 | 106 | 23 B & C | 0.18 | 6.17 |
| 122-133 | 2128 | 62 | 129 | 23 B & C | 0.17 | 5.83 |
| 133-142 | 2129 | 63 | 109 | 23 C | 0.24 | 8.23 |
| 143-158 | 2134 | 64 | 160 | 23 C | 0.06 | 2.06 |
| 159-175 | 2135 | 65 | 170 | 23 C & D | 0.58 | 19.89 |
| 176-197 | 2136 | 66 | 220 | 23 D & E | 0.63 | 21.60 |
| 198-222 | 2137 | 67 | 253 | 23 C, D,E | 0.32 | 10.97 |
| 223-238 | 2138 | 68 | 160 | 23 A,B,C | 0.30 | 10.29 |
| 239-244 | 2139 | 69 | | | 0.06 | 2.06 |
| 245-255 | 2154 | 70 | 110 | 23 A | 0.36 | 12.34 |
| 256-267 | 2155 | 71 | 120 | 22 B,C,:23 B,C | 0.04 | 1.37 |
| 268-285 | 2156 | 72 | 180 | 22 C,D: 23 C | 0.08 | 2.74 |
| 286-294 | 2168 | 73 | 90 | 22 D,E,F | 0.24 | 8.23 |
| 298-301 | 2169 | 74 | 40 | 22 F | 0.41 | 14.06 |
| 302-305 | 2170 | 75 | 40 | 22 B,F | 0.11 | 3.77 |
| 353 | 2196 | 76 | 10 | 23 C | 0.15 | 5.14 |
| 319 | 2197 | 77 | 10 | 23 C | 0.08 | 2.74 |
| 325-331 | 2198 | 78 | 70 | 22 D E | 0.20 | 6.85714 |
| 333 | 2199 | 79 | 10 | 22 E | 0.10 | 3.42857 |
| 310-317 | 2206 | 80 | 80 | 22 B,C | 0.40 | 13.71428 |
| 342-369 | 2216 | 81 | 280.98 | 22 A, B C, D | 0.85 | 29.14 |
| 370-371 | 2217 | 82 | 22.44 | 3A | 1.02 | 34.97 |
| 372-377 | 2218 | 83 | 67.32 | 3A | 1.04 | 35.66 |
| 383-393 | 2219 | 84 | 123.42 | 3A | 0.56 | 19.20 |
| 394-399 | 2220 | 85 | 67.32 | 3B | 1.20 | 41.14284 |
| 378-382 | 2221 | 86 | 56.1 | 3A | 0.51 | 17.49 |
| 411-422 | 2228 | 87 | 134.64 | 3 D,E | 0.32 | 10.97 |
| 423-429 | 2229 | 88 | 78.54 | 3 D,E | 0.45 | 15.43 |
| 431-440 | 2230 | 89 | 112.2 | 3 E | 0.90 | 30.86 |
| 441-449 | 2231 | 90 | 100.98 | 3 E | 0.55 | 18.86 |
| 450-459 | 2232 | 91 | 112.2 | 3 F | 0.22 | 7.54 |
| 460-469 | 2233 | 92 | 112.2 | 3 F,G | 0.18 | 6.17 |
| 470-477 | 2234 | 93 | 89.76 | 3 G | 0.39 | 13.37 |
| 400-410 | 2236 | 94 | 123.42 | 3 C | 1.07 | 36.69 |
| 478-489 | 2237 | 95 | 134.64 | 4 E | 0.93 | 31.89 |
| 490-499 | 2238 | 96 | 112.2 | 4 E | 0.34 | 11.66 |
| 500-509 | 2239 | 97 | 112.2 | 4 F | 0.33 | 11.31 |
| 510-519 | 2265 | 98 | 112.2 | 4 D,F | 0.24 | 8.23 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 520-529 | 2266 | 99 | 112.2 | 4 C,D | 0.28 | 9.60 |
| 579-587 | 2272 | 105 | 100.98 | 5 C | 0.78 | 26.74 |
| 590-599 | 2273 | 106 | 112.2 | 5 C,D | 0.83 | 28.46 |
| 600-607 | 2274 | 107 | 89.76 | 5 D | 0.21 | 7.20 |
| 678-687 | 2275 | 108 | 112.2 | 6A | 0.77 | 26.40 |
| 688-697 | 2276 | 109 | 112.2 | 6A | 0.29 | 9.94 |
| 698-707 | 2277 | 110 | 110 | 6A,B | 0.41 | 14.06 |
| 708-717 | 2278 | 111 | 110 | 6 B | 0.95 | 32.57 |
| 630-639 | 2279 | 112 | 112.2 | 5 E | 0.21 | 7.20 |
| 620-629 | 2280 | 113 | 112.2 | 5 D | 0.21 | 7.20 |
| 610-619 | 2281 | 114 | 112.2 | 5 D | 0.23 | 7.89 |
| 638-649 | 2294 | 115 | 123.42 | 5 E | 0.24 | 8.23 |
| 650-659 | 2295 | 116 | 112.2 | 5 E,F,G | 0.32 | 10.97 |
| 660-669 | 2296 | 117 | 112.2 | 5 G | 0.14 | 4.80 |
| 670-677 | 2297 | 118 | 89.76 | 5 G | 0.22 | 7.54 |
| 720-726 | 2298 | 119 | 80.5 | 6 B | 0.30 | 10.29 |
| 727-734 | 2299 | 120 | 92 | 6 C | 0.76 | 26.06 |
| 735-743 | 2313 | 121 | 100.98 | 6 C | 0.47 | 16.11 |
| 744-752 | 2314 | 122 | 100.98 | 6 D | 0.06 | 2.06 |
| 753-760 | 2315 | 123 | 89.76 | 6 D | 0.41 | 14.06 |
| 761-767 | 2316 | 124 | 78.54 | 6 E | 0.36 | 12.34 |
| 768-777 | 2317 | 125 | 112.2 | 6 F | 0.14 | 4.80 |
| 778-787 | 2318 | 126 | 112.2 | 6 F | 0.23 | 7.89 |
| 788-796 | 2319 | 127 | 100.98 | 6 G | 0.49 | 16.80 |
| 797-804 | 2337 | 128 | 89.76 | 7 F | 0.28 | 9.60 |
| 805-814 | 2338 | 129 | 112.2 | 7 F | 0.30 | 10.29 |
| 815-823 | 2339 | 130 | 100.98 | 7 F | 0.19 | 6.51 |
| 824-833 | 2435 | 134 | 112.2 | 7 C | 0.30 | 10.29 |
| 834-843 | 2436 | 135 | 112.2 | 7 C | 0.09 | 3.09 |
| 844-851 | 2437 | 136 | 89.76 | 7 B,C | 0.35 | 12.00 |
| 869-876 | 2484 | 139 | 89.76 | 7A | 0.08 | 2.74 |
| 877-884 | 2485 | 140 | 95.04 | 7A | 0.22 | 7.54 |
| 885-892 | 2486 | 141 | 89.76 | 7A,B | 0.42 | 14.40 |
| 893-901 | 2487 | 142 | 100.98 | 8 B | 0.34 | 11.66 |
| 901-910 | 2488 | 143 | 100.98 | 8 B,C | 1.17 | 40.11 |
| 911-918 | 2489 | 144 | 89.76 | 8 C | 0.45 | 15.43 |
| 919-929 | 2490 | 145 | 123.42 | 8 D | 0.17 | 5.83 |
| 930-939 | 2536 | 146 | 112.2 | 8 D | 0.07 | 2.40 |
| 940-949 | 2537 | 147 | 112.2 | 8 D, E | 0.06 | 2.06 |
| 950-959 | 2538 | 148 | 112.2 | 7 E,F | 0.20 | 6.85714 |
| 960-969 | 2539 | 149 | 112.2 | 7 F | 0.03 | 1.03 |
| 970-977 | 2540 | 150 | 89.76 | 7 F,G | 0.05 | 1.71 |
| 978-985 | 2541 | 151 | 89.76 | 7 G | 0.07 | 2.40 |
| 986-992 | 2542 | 152 | 78.54 | 7 G | 0.04 | 1.37 |
| 993-999 | 2543 | 153 | 78.54 | 8 G | 0.11 | 3.77 |
| 1000-1006 | 2544 | 154 | 78.54 | 8 G | 0.08 | 2.74 |
| 1007-1013 | 2545 | 155 | 78.54 | 8 G | 0.05 | 1.71 |
| 1014-1020 | 2766 | 156 | 70 | 9 F,G | 0.44 | 15.09 |
| 1021-1025 | 2767 | 157 | 50 | 9 F | 0.08 | 2.74 |
| 1026-1033 | 2768 | 158 | 80 | 9 F | 0.07 | 2.40 |
| 1044-1051 | 2769 | 159 | 89.76 | 9 E,F | 0.06 | 2.06 |
| 1052-1059 | 2770 | 160 | 89.76 | 9E | 0.08 | 2.74 |

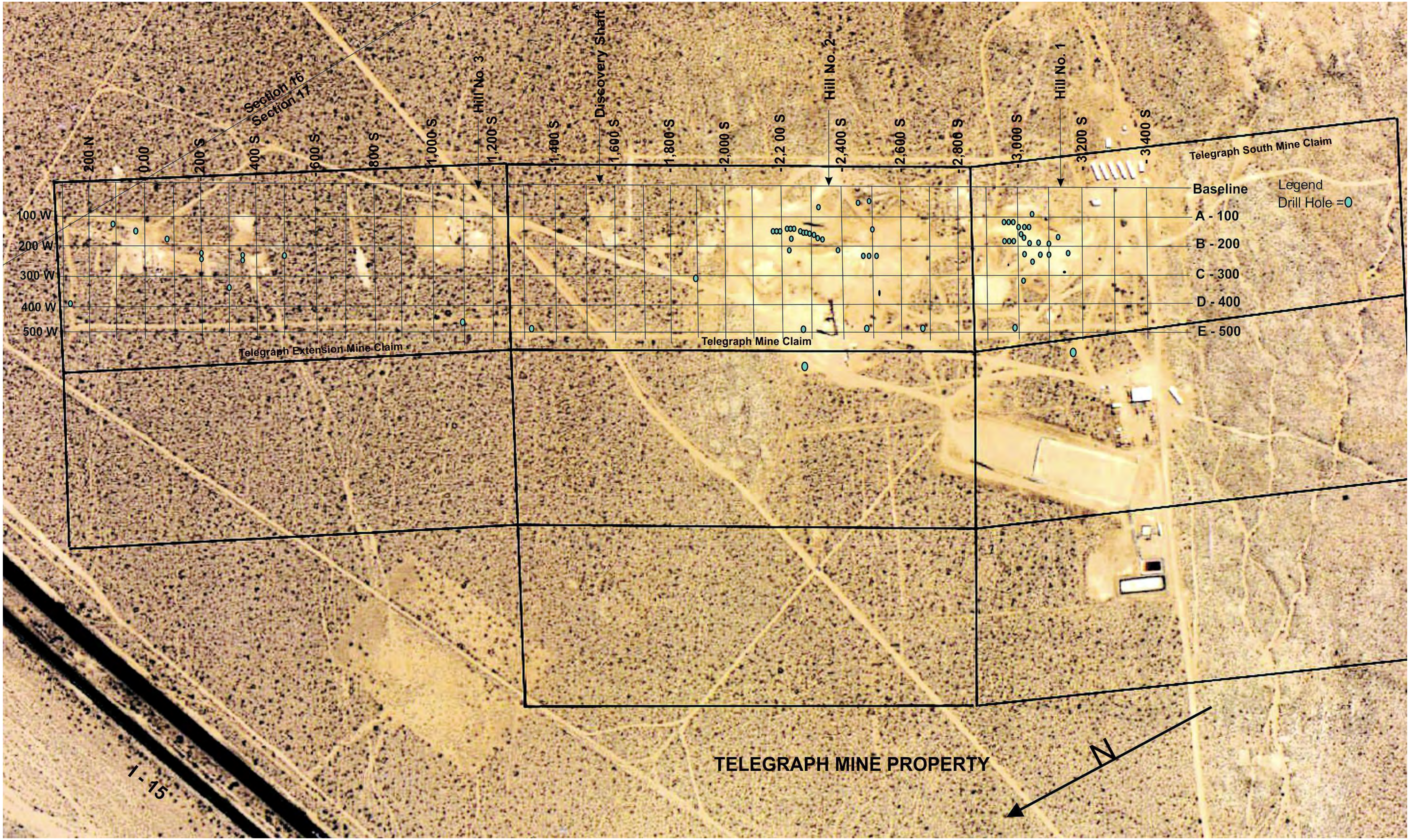
| | | | | | | |
|---|---|---|---|---|---|---|
| 1060-1066 | 2771 | 161 | 78.54 | 9 E, G | 0.08 | 2.74 |
| 1067-1073 | 2772 | 162 | 78.54 | 9 D,E | 0.05 | 1.71 |
| 1074-1080 | 2773 | 163 | 78.54 | 9 D | 0.06 | 2.06 |
| 1081-1087 | 2774 | 164 | 78.54 | 8 C | 0.09 | 3.09 |
| 1088-1094 | 2775 | 165 | 78.54 | 8 B C | 0.06 | 2.06 |
| 1095-1101 | 2776 | 166 | 78.54 | 8 A, B | 0.04 | 1.37 |
| 1102-1109 | 2777 | 167 | 89.76 | 8A | 0.06 | 2.06 |
| 1110-1117 | 2778 | 168 | 89.76 | 8 A, B | 0.07 | 2.40 |
| 1118-1125 | 2779 | 169 | 89.76 | 8 A: 9 A | 0.05 | 1.71 |
| 1126-1131 | 2795 | 174 | 67.32 | 9 A,B | 0.09 | 3.09 |
| 1132-1137 | 2796 | 175 | 67.32 | 9 B | 0.09 | 3.09 |
| 1138-1143 | 2797 | 176 | 67.32 | 9 B, C | 0.05 | 1.71 |
| 1144-1152 | 2780 | 170 | 100.98 | 9 B | 0.07 | 2.40 |
| 1153-1158 | 2781 | 171 | 67.32 | 9 B,C | 0.16 | 5.49 |
| 1159-1164 | 2782 | 172 | 67.32 | 9 C | 0.08 | 2.74 |
| 1165-1171 | 2782 | 173 | 78.54 | 9 C,D | 0.07 | 2.40 |
| 1172-1179 | 2856 | 177 | | | 0.12 | 4.11 |
| 1180-1187 | 2857 | 178 | | | 0.04 | 1.37 |
| 1188-1193 | 2858 | 179 | 67.32 | 9 F | 0.05 | 1.71 |
| 1194-1199 | 2859 | 180 | 67.32 | 9 F, G | 0.08 | 2.74 |
| 1200-1206 | 2860 | 181 | 78.54 | 9 G | 0.06 | 2.06 |
| 1207-1213 | 2861 | 182 | 78.54 | 9 G: 10 G | 0.06 | 2.06 |
| 1214-1220 | 2862 | 183 | 78.54 | 10 G | 0.02 | 0.69 |
| 1221-1227 | 2863 | 184 | 78.54 | 10 G | 0.03 | 1.03 |
| 1235-1241 | 3252 | 189 | 78.54 | 10 E, F | 0.03 | 1.03 |
| 1228-1234 | 3253 | 190 | 78.54 | 10 F | 0.07 | 2.40 |
| 1250-1257 | 3254 | 191 | 89.76 | 10 D | 0.11 | 3.77 |
| 1258-1265 | 3255 | 192 | 89.76 | 10 D, E | 0.14 | 4.80 |
| 1266-1273 | 3256 | 193 | 89.76 | 10 C,D | 0.13 | 4.46 |
| 1274-1281 | 3257 | 194 | 89.76 | 10 A, B | 0.21 | 7.20 |
| 1282-1287 | 3258 | 195 | 67.32 | 10 A, B | 0.08 | 2.74 |
| 1288-1293 | 3259 | 196 | 67.32 | 10A | 0.09 | 3.09 |
| 1294-1300 | 3260 | 197 | 78.54 | 10A | 0.05 | 1.71 |
| 1301-1307 | 3261 | 198 | 78.54 | 11A | 0.05 | 1.71 |
| 1308-1314 | 3262 | 199 | 78.54 | 11 A, B | 0.04 | 1.37 |
| 1315-1322 | 3263 | 200 | 89.76 | 11 B | 0.08 | 2.74 |
| 1323-1332 | 3264 | 201 | 112.2 | 11 B,C | 0.02 | 0.69 |
| 1333-1342 | 3265 | 202 | 112.2 | 11 C | 0.02 | 0.69 |
| 1343-1351 | 3266 | 203 | 100.98 | 11 C, D | 0.04 | 1.37 |
| 1352-1360 | 3267 | 204 | 100.98 | 11 D | 0.014 | 0.48 |
| 1361-1369 | 3268 | 205 | 100.98 | 11 D, E | 0.06 | 2.06 |
| 1370-1378 | 3269 | 206 | 100.98 | 11 E, | 0.024 | 0.82 |
| 1379-1386 | 3270 | 207 | 89.76 | 11 E, F | 0.09 | 3.09 |
| 1235-1249 | 3281 | 208 | 168.3 | 10 E, F | 0.18 | 6.17 |
| 1387-1392 | 3282 | 209 | 67.32 | 11 F | 0.04 | 1.37 |
| 1393-1398 | 3283 | 210 | 67.32 | 11 G | 0.03 | 1.03 |
| 1399-1405 | 3284 | 211 | 78.54 | 11 G | 0.02 | 0.69 |
| 1406-1412 | 3285 | 212 | 78.54 | 11 G | 0.16 | 5.49 |
| 1413-1418 | 3286 | 213 | 67.32 | 11 C, D,E,F,G | 0.06 | 2.06 |
| 1419-1424 | 3287 | 214 | 67.32 | 12 B | 0.73 | 25.03 |
| 1425-1431 | 3288 | 215 | 78.54 | 12 B | 0.11 | 3.77 |
| 1432-1440 | 3289 | 216 | 89.76 | 12 A, B | 0.08 | 2.74 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 1441-1447 | 3290 | 217 | 89.76 | 12 A,C | 0.97 | 33.26 |
| 1448-1454 | 3310 | 220 | 78.54 | 11 C | 0.88 | 30.17 |
| 1455-1461 | 3311 | 221 | 78.54 | 11 D | 0.97 | 33.26 |
| 1462-1468 | 3312 | 222 | 78.54 | 11 D,E | 1.02 | 34.97 |
| 1469-1475 | 3313 | 223 | 78.54 | 12 E,F | 1.12 | 38.40 |
| 1476-1482 | 3314 | 224 | 78.54 | 12 F | 1.07 | 36.69 |
| 1610-1616 | 3352 | 243 | 78.54 | 12 E | 0.06 | 2.06 |
| 1617-1622 | 3353 | 244 | 67.32 | 12 E,F | 0.35 | 12.00 |
| 1623-1628 | 3354 | 245 | 67.32 | 12 F | 0.51 | 17.49 |
| 1629-1634 | 3355 | 246 | 67.32 | 12 F,G | 0.74 | 25.37 |
| 1635-1640 | 3356 | 247 | 67.32 | 12 G | 0.40 | 13.71428 |
| 1641-1654 | 3522 | 249 | 157.08 | 12, 13,, G | 0.10 | 3.43 |
| 1655-1667 | 3523 | 250 | 145.86 | 13 G | 0.12 | 4.11 |
| 1668-1677 | 3524 | 251 | 100.98 | 13 F | 0.11 | 3.77 |
| 1678-1687 | 3525 | 252 | 112.2 | 13 F | 0.08 | 2.74 |
| 1688-1699 | 3526 | 253 | 134.64 | 13 D, E | 0.11 | 3.77 |
| 1700-1708 | 3527 | 254 | 100.98 | 13 D | 0.07 | 2.40 |
| 1709-1720 | 3689 | 255 | 134.64 | 13 D | 0.10 | 3.43 |
| 1739-1748 | 3692 | 258 | 112.2 | 13 A,B | 0.04 | 1.37 |
| 1750-1761 | 3693 | 259 | 123.42 | 13 A | 0.04 | 1.37 |
| 1762-1772 | 3694 | 260 | 123.42 | 13 A, B, C | 0.05 | 1.71 |
| 1773-1783 | 3695 | 261 | 123.42 | 13 G | 0.06 | 2.06 |
| 1784-1791 | 3696 | 262 | 89.76 | 13 G | 0.08 | 2.74 |
| 1792-1800 | 3697 | 263 | 100.98 | 13 E,F, G | 0.08 | 2.74 |
| 1801-1809 | 3698 | 264 | 100.98 | 13 F ,G | 0.05 | 1.71 |
| 1810-1822 | 3699 | 265 | 145.86 | 13 E | 0.05 | 1.71 |
| 1823-1832 | 3716 | 266 | 112.2 | 13 D | 0.02 | 0.69 |
| 1833-1842 | 3717 | 267 | 112.2 | 13 D | 0.02 | 0.69 |
| 1843-1852 | 3718 | 268 | 112.2 | 13 C | 0.04 | 1.37 |
| 1853-1861 | 3719 | 269 | 99 | 14 B | 0.05 | 1.71 |
| 1862-1870 | 3720 | 270 | 99 | 14 A, B | 0.05 | 1.71 |
| 1871-1880 | 3721 | 271 | 110 | 14 A | 0.06 | 2.06 |
| 1883-1891 | 3722 | 272 | 99 | 14 A | 0.04 | 1.37 |
| 1892-1900 | 3723 | 273 | 99 | 14 A | 0.02 | 0.69 |
| 1901-1907 | 3724 | 274 | 77 | 14 A, B | 0.05 | 1.71 |
| 1922-1929 | 3725 | 275 | 88 | 14 C | 0.04 | 1.37 |
| 1979-1981 | 3741 | 289 | 33 | 14 G | 0.12 | 4.11 |
| 1990-1995 | 3742 | 290 | 66 | 13 D,E,F,G | 0.08 | 2.74 |
| 1996-2005 | 3743 | 291 | 99 | 14 D,G | 0.09 | 3.09 |
| 2006-2015 | 3744 | 292 | 80 | 15 F,G | 0.05 | 1.71 |
| 2016-2025 | 3745 | 293 | 80 | 15 F | 0.07 | 2.40 |
| 2026-2035 | 3746 | 294 | 80 | 15 E,F | 0.05 | 1.71 |
| 2036-2050 | 3747 | 295 | 120 | 15 E,F | 0.06 | 2.06 |
| 2167-2176 | 3769 | 302 | 80 | 15 B,C | 0.04 | 1.37 |
| 2177-2186 | 3770 | 303 | 80 | 15 B,C | 0.19 | 6.51 |
| 2187-2196 | 3771 | 304 | 80 | 15 D,E | 0.12 | 4.11 |
| 2197-2206 | 3772 | 305 | 80 | 15 D,E | 0.05 | 1.71 |
| 2207-2216 | 3773 | 306 | 80 | 15 E | 0.07 | 2.40 |
| 2217-2225 | 3774 | 307 | 72 | 15 E | 0.06 | 2.06 |
| 2226-2235 | 3775 | 308 | 80 | 15 E,F | 0.06 | 2.06 |
| 2236-2245 | 3776 | 309 | 80 | 15 F | 0.05 | 1.71 |
| 2246-2255 | 3777 | 310 | 80 | 15 F,G | 0.06 | 2.06 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 2256-2265 | 3778 | 311 | 80 | 15 G | 0.10 | 3.43 |
| 2266-2273 | 3779 | 312 | 64 | 15 A | 0.12 | 4.11 |
| 2274-2283 | 3780 | 313 | 80 | 15 A,B; 16 A | 0.14 | 4.80 |
| 2284-2293 | 3781 | 314 | 80 | 16 A,B | 0.13 | 4.46 |
| 2294-2298 | 3782 | 315 | 40 | 16 A,B | 0.72 | 24.69 |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| 530-539 | 2267 | 100 | 112.2 | 4 C,D | No Results | |
| 540-548 | 2268 | 101 | 100.98 | 4 C | No Results | |
| 549-559 | 2269 | 102 | 123.42 | 5A | No Results | |
| 560-569 | 2270 | 103 | 112.2 | 5B | No Results | |
| 570-578 | 2271 | 104 | 100.98 | 5 B | No Results | |
| 852-859 | 2482 | 137 | 89.76 | 7 B | No Results | |
| 860-868 | 2483 | 138 | 100.98 | 7 B | No Results | |
| 1583-1589 | 3348 | 239 | 78.54 | 12 B,C | No Results | |
| 1590-1597 | 3349 | 240 | 89.76 | 12 C,D | No Results | |
| 1598-1604 | 3350 | 241 | 78.54 | 12 D | No Results | |
| 1605-1609 | 3351 | 242 | 56.1 | 12 D | No Results | |
| 1721-1730 | 3690 | 256 | 112.2 | 13 C | No Results | |
| 1731-1740 | 3691 | 257 | 112.2 | 13 B | No Results | |
| 1930-1937 | 3726 | 276 | 88 | 14 C | No Results | |
| 1938-1945 | 3727 | 277 | 88 | 14 D | No Results | |
| 1946-1953 | 3728 | 278 | 88 | 14 D, E | No Results | |
| 1955-1961 | 3729 | 279 | 77 | 14 E | No Results | |
| 1962-1970 | 3730 | 280 | 99 | 14 F | No Results | |
| 1971-1978 | 3731 | 281 | 88 | 14 F, G | No Results | |
| 2051-2060 | 3736 | 284 | 80 | 15 E | No Results | |
| 2060-2070 | 3737 | 285 | 88 | 15 D | No Results | |
| 2071-2080 | 3738 | 286 | 80 | 15 C,D | No Results | |
| 2080-2089 | 3739 | 287 | 80 | 15 C | No Results | |
| 2090-2099 | 3740 | 288 | 80 | 15 B,C | No Results | |
| 2100-2103 | 3734 | 282 | 24 | 15 B | No Results | |
| 2104-2113 | 3735 | 283 | 80 | 14 A,B | No Results | |
| 2114-2123 | 3763 | 296 | 80 | 15 A | No Results | |
| 2124-2133 | 3764 | 297 | 80 | 15 A | No Results | |
| 2134-2143 | 3765 | 298 | 80 | 15 B | No Results | |
| 2144-2153 | 3766 | 299 | 80 | 15 B | No Results | |
| 2154-2156 | 3767 | 300 | 24 | 15 B | No Results | |
| 2157-2166 | 3768 | 301 | 80 | 15 B,C | No Results | |

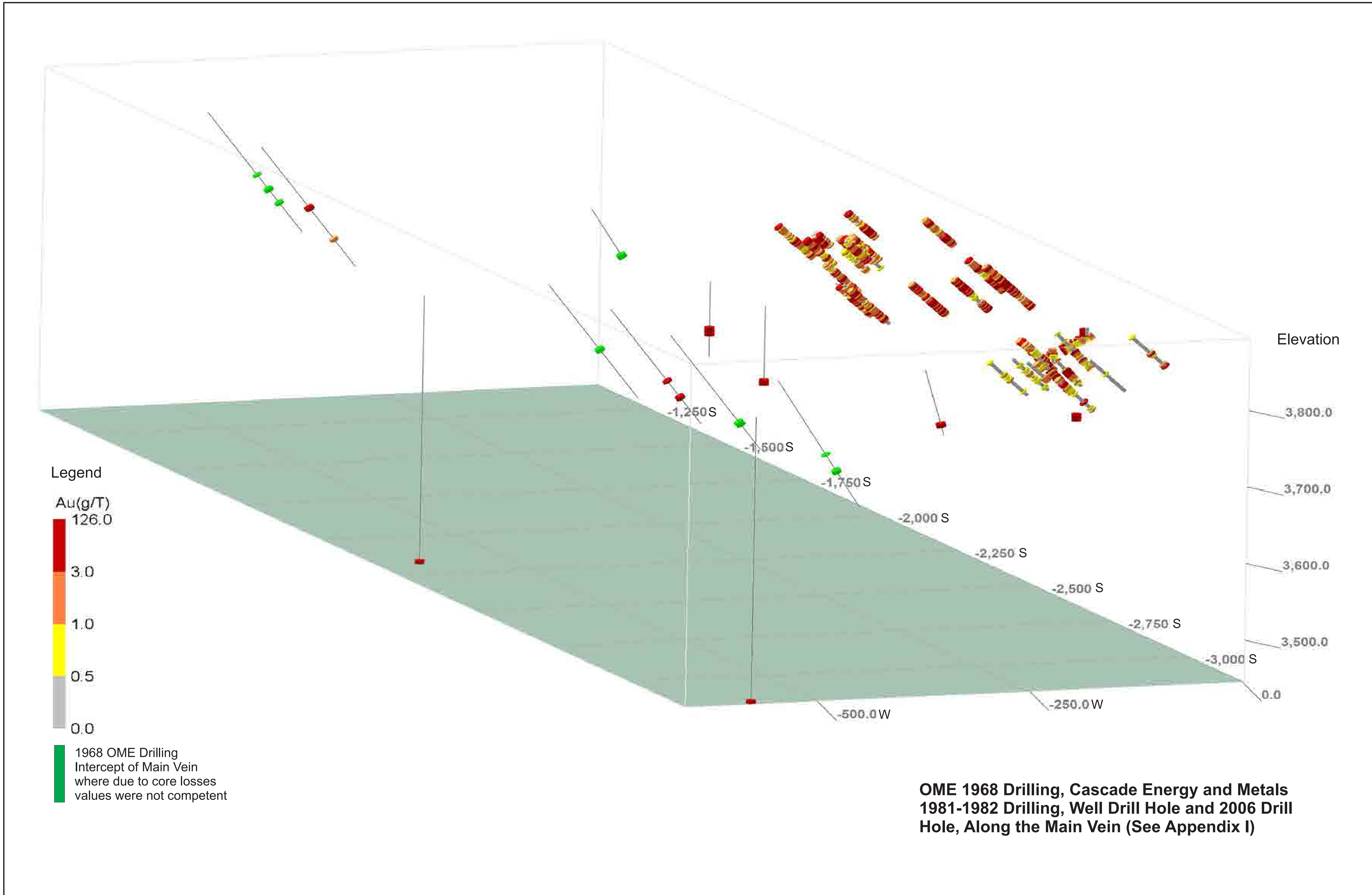
# Appendix I

**Aerial Photo Showing Claim Boundaries**
**the Telegraph Grid**
**and Drill Hole Locations**

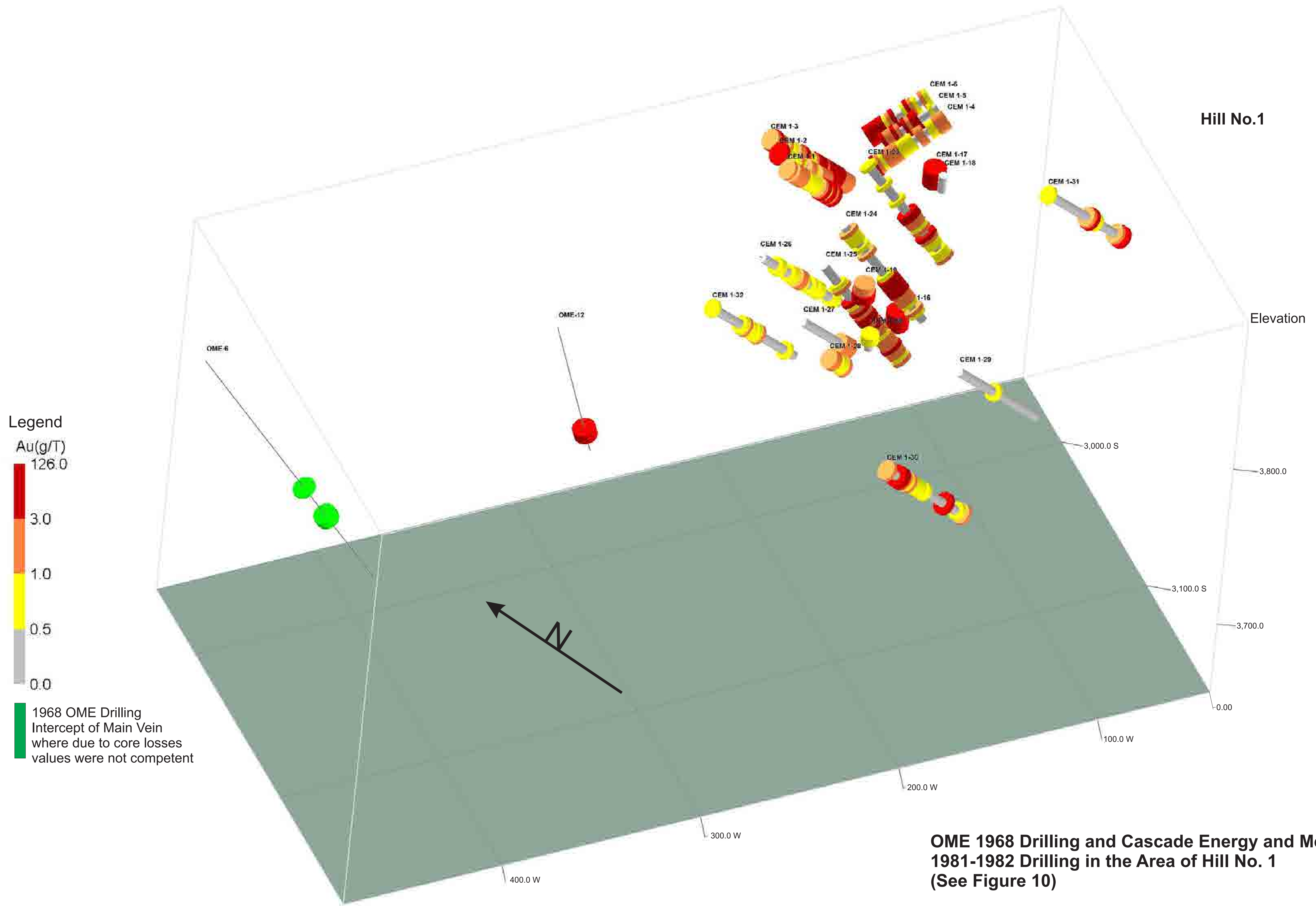

Section 16
Section 17
200 N
0.00
200 S
400 S
600 S
800 S
1,000 S
Hill No 3
1,200 S
1,400 S
Discovery Shaft
1,600 S
1,800 S
2,000 S
2,2 00 S
Hill No. 2
2,400 S
2,600 S
2,800 S
3,000 S
Hill No. 1
3,200 S
3,400 S
Telegraph South Mine Claim
Baseline
A - 100
B - 200
C - 300
D - 400
E - 500
Legend
Drill Hole =
100 W
200 W
300 W
400 W
500 W
Telegraph Extension Mine Claim
Telegraph Mine Claim
TELEGRAPH MINE PROPERTY
N
I - 15

# Appendix J

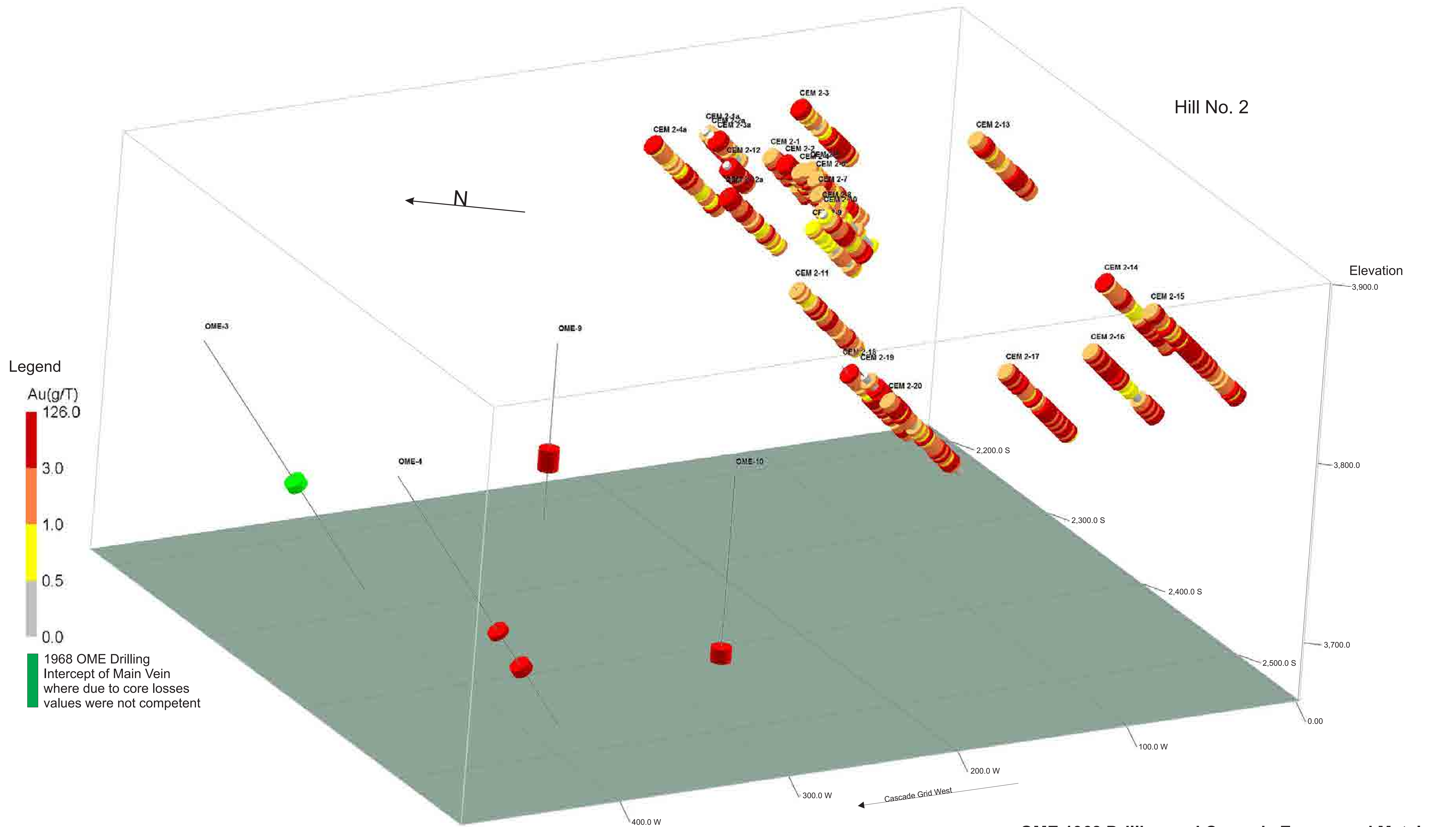
**3-D Plots of Telegraph Mine Historic Drilling**




**OME 1968 Drilling, Cascade Energy and Metals 1981-1982 Drilling, Well Drill Hole and 2006 Drill Hole, Along the Main Vein (See Appendix I)**




**OME 1968 Drilling and Cascade Energy and Metals 1981-1982 Drilling in the Area of Hill No. 1 (See Figure 10)**




**OME 1968 Drilling and Cascade Energy and Metals 1981-1982 Drilling in the Area of Hill No. 2 (See Figure 9)**